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PROGRAM MANAGER RMA CONTAMINATION CLEANUP

U.S. ARMY
MATERIEL COMMAND

— COMMITTED TO PROTECTION OF THE ENVIRONMENT —

COMPREHENSIVE MONITORING PROGRAM

Contract Number DAAA15-87-0095

FINAL SURFACE WATER DATA ASSESSMENT REPORT FOR 1989

JUNE 1990

Version 2.0

Volume III

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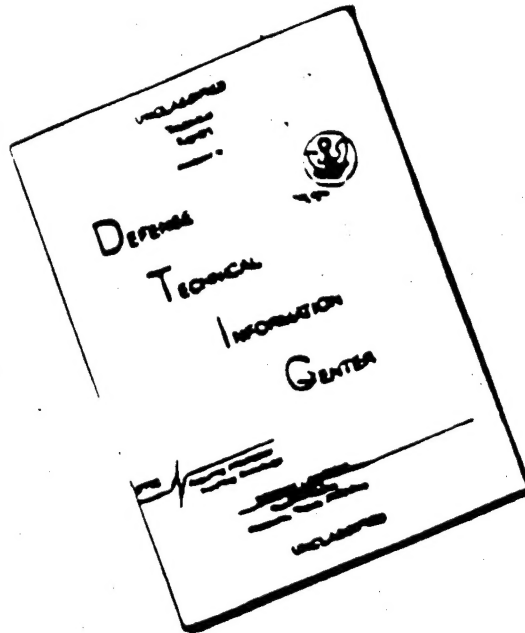
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**FINAL SURFACE WATER DATA ASSESSMENT
REPORT FOR 1989**

JUNE 1990

Version 2.0

Volume III

APPENDIX A

(Appendices A-1 to A-6)

Prepared by:

**R. L. STOLLAR & ASSOCIATES INC.
HARDING LAWSON ASSOCIATES
EBASCO SERVICES INC.
DATACHEM, INC.
ENVIRONMENTAL SCIENCE & ENGINEERING, INC.
RIVERSIDE TECHNOLOGY, INC.**

Prepared for:

**U. S. ARMY PROGRAM MANAGER FOR
ROCKY MOUNTAIN ARSENAL**

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APPENDIX A

Surface-Water Quantity Data for Water Year 1989

APPENDIX A-1

Surface-Water Station Survey Information

APPENDIX A-1.1

Monitoring Station Survey Information

| Station # | Location | Northing | Easting | Elevation/GH |
|-----------|---------------------------|------------|--------------|--|
| SW01001 | N. Uvalda Interceptor | 175,588.02 | 2,187,896.41 | 5,260.55 = TBM 5,258.92 = 3.33 on SG |
| SW01003 | South Plants Ditch | 177,784.84 | 2,185,793.81 | 5,255.61 = TBM 5,248.78 = 0.00 on SG 5,253.13 = PZF on SW Weir 5,252.21 = PZF on S Weir |
| SW01004 | Upper Derby Lake | 176,932.23 | 2,187,034.25 | 5,247.77 = 0.00 on SG |
| SW01005 | Lower Derby Lake | 176,414.44 | 2,183,945.48 | 5,230.17 = 0.00 on SG |
| SW02001 | Ladora Weir | 176,311.48 | 2,183,662.77 | 5,235.49 = TBM 5,228.84 = 0.00 on SG |
| SW02003 | Ladora Lake | 177,726.61 | 2,179,691.86 | 5,222.11 = 15.00 on SG |
| SW02004 | Lake Mary | 177,378.84 | 2,178,434.27 | 5,202.39 = 0.00 on SG |
| SW05001 | South First Creek (old) | 175,590.08 | 2,197,131.85 | 5,281.87 = TBM 5,278.58 = 0.00 on SG 5,278.91 = PZF |
| SW08003 | South First Creek (new) | 173,686.65 | 2,198,520.22 | 5,293.84 = TBM A 5,293.94 = TBM B 5,290.83 = PZF 5,290.82 = 0.00 on SG |
| SW11001 | Peoria Interceptor | 170,287.71 | 2,179,583.49 | 5,252.48 = TBM 5,250.28 = 3.33 on SG |
| SW11002 | Havana Interceptor | 170,992.86 | 2,178,854.75 | 5,261.49 = TBM 5,252.09 = 0.00 on SG |
| SW11003 | Havana Pond | 172,696.42 | 2,180,121.78 | 5,253.97 = TBM 5,244.08 = 0.00 on SG |
| SW12005 | South Uvalda Interceptor | 170,445.36 | 2,186,746.06 | 5,272.37 = TBM 5,274.40 = 3.33 on SG |
| SW12007 | Highline Lateral | 175,292.77 | 2,188,725.83 | 5,275.15 = TBM 5,275.10 = 3.33 on SG 5,272.63 = PZF |
| SW24001 | Sewage Treatment Effluent | 194,147.34 | 2,186,376.17 | 5,154.56 = PVC |

Appendix A-1.1 Table A-1.1-1 (cont'd.)

| Station # | Location | Northing | Easting | Elevation/GH |
|-----------|----------------------|------------|--------------|---|
| SW24002 | N. First Creek (new) | 195,311.93 | 2,187,575.26 | 5,146.52 = TBM A 5,146.01 = TBM B 5,141.75 = PZF 5,144.51 = 3.33 on SG |
| SW36001 | Basin A | 180,985.85 | 2,184,525.97 | 5,253.51 = TBM A 5,253.50 = TBM B 5,252.11 = 0.00 on SG 5,252.19 = PZF |
| SW37001 | First Creek Off-post | 199,013.30 | 2,180,816.71 | 5,108.99 = TBM 5,110.24 = 3.33 on SG 5107.43 = PZF Weir |

SG = Staff Gage
TBM = Temporary Bench Mark
PZF = Point of Zero Flow

APPENDIX A-1.2

Station Survey Information

APPENDIX A-1.2

Cross-Section Survey Plots

Cross Sections were surveyed at the following stations:

- North Uvalda (SW01001)
- Peoria Interceptor (SW11001)
- Havana Interceptor (SW11002)
- South Uvalda (SW12005)
- North First Creek (SW24002)

Two channel cross sections were surveyed below the structure, one cross section through the center of the structure, one cross section upstream of the structure through the existing staff gage and two additional cross sections were surveyed upstream of the staff gage. The maximum distance between adjacent cross sections was five channel widths.

One cross section was surveyed at Havana Interceptor along with upstream and downstream thalweg elevations for bed slope calculations. Four cross sections were surveyed at North Uvalda. Six cross sections were surveyed at Peoria Interceptor and South Uvalda. A total of five cross sections were surveyed at North First Creek.

Each cross section elevation is in feet mean sea level (MSL) and is tied to a vertical control (temporary bench mark - TBM) near each gage. All cross sections were surveyed from left bank to right bank looking in a downstream direction. Horizontal and vertical scales for plotting were selected independently for each station reach based on best visual representation of plots to actual site conditions. Cross-section plot number three and four for each station includes the staff gage elevations on the cross-section plot.

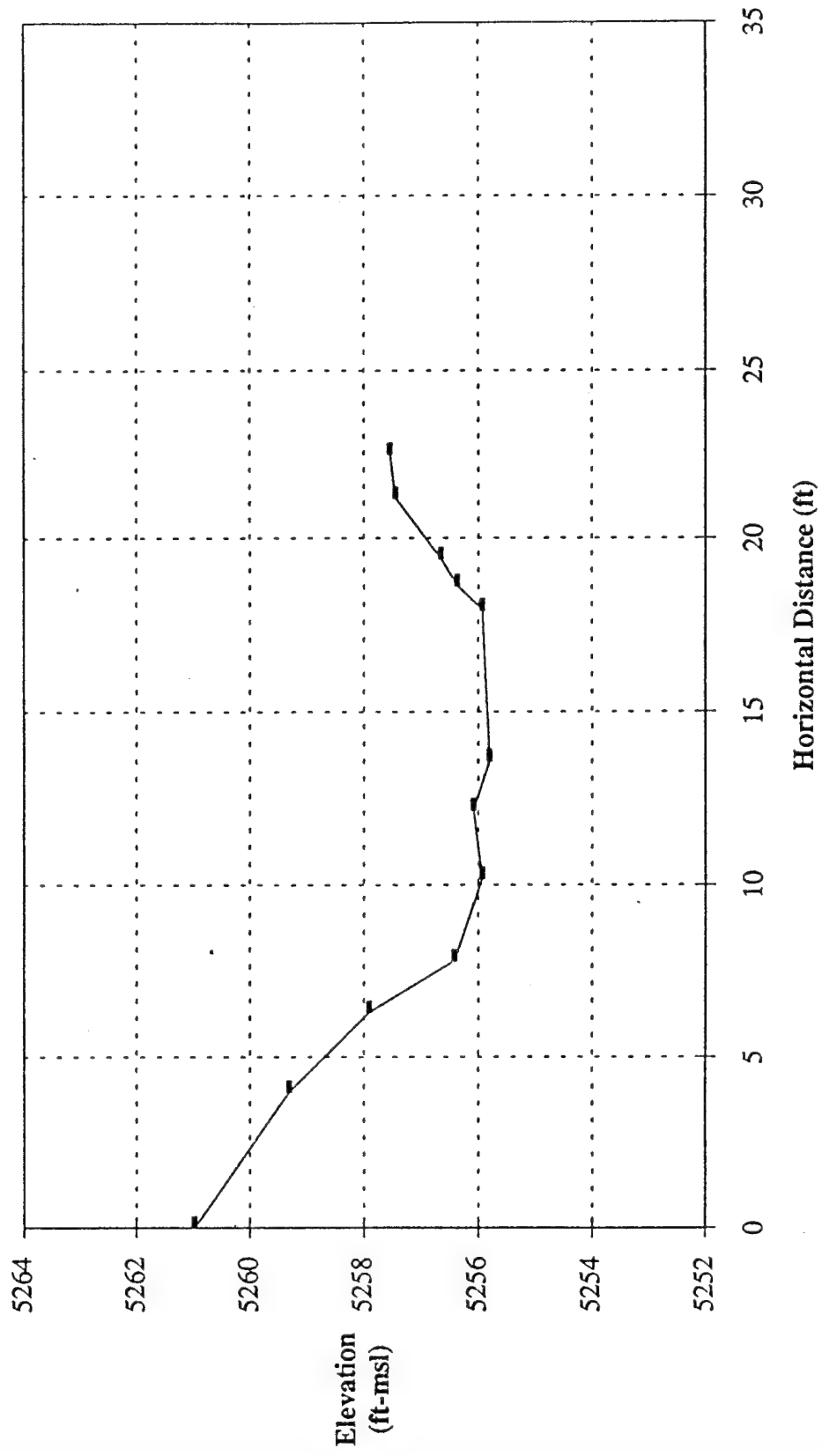
Plan view drawings were produced for each surveyed station. The plan views contain the following information:

- Distance between cross sections.
- Location of the control structure.
- Location of the stilling well.
- Location of the staff gage.
- Location of the TBM.
- Direction of flow.
- Average width of the channel.

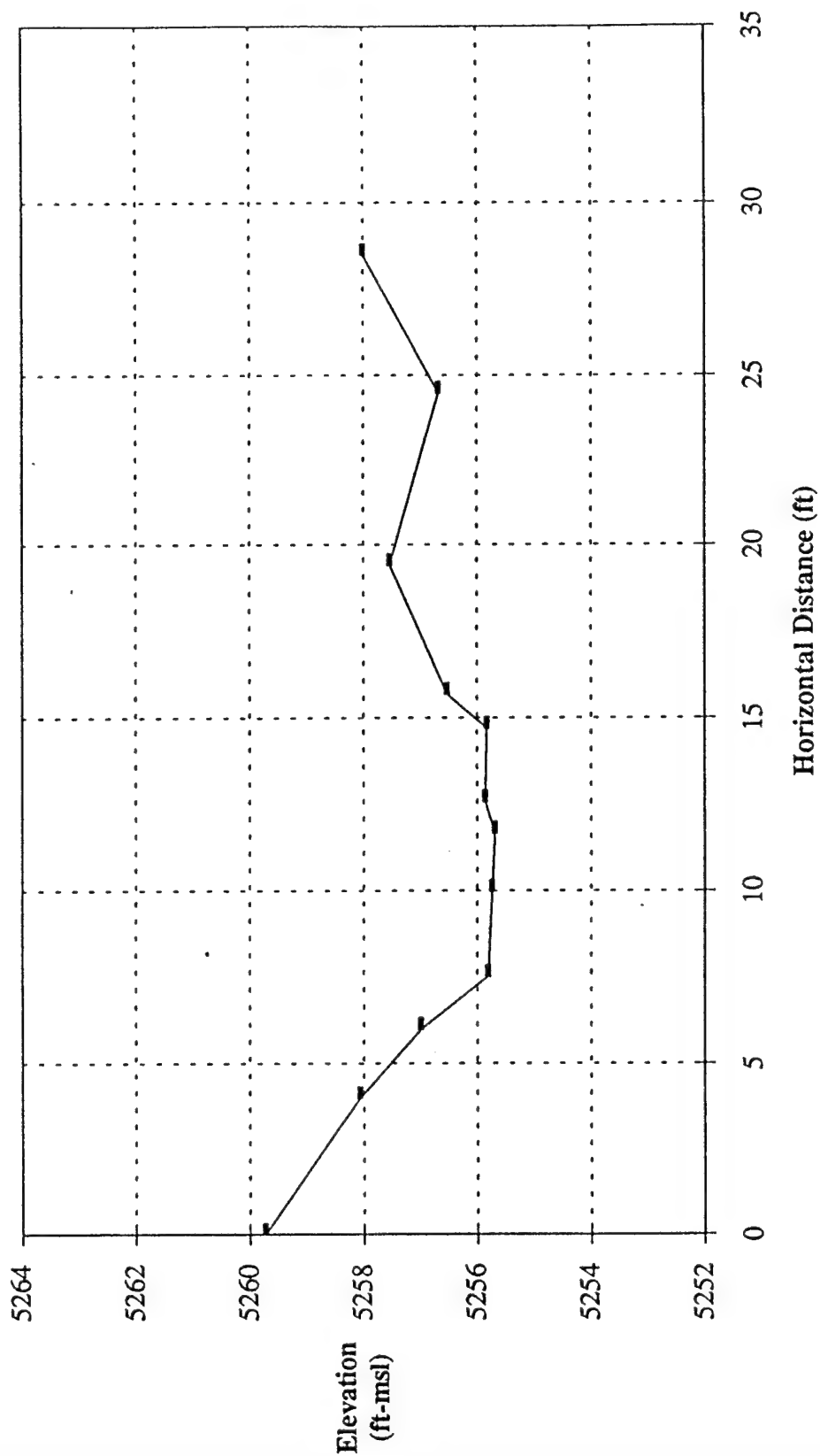
APPENDIX A-1.2.1

Cross Section Survey Plots

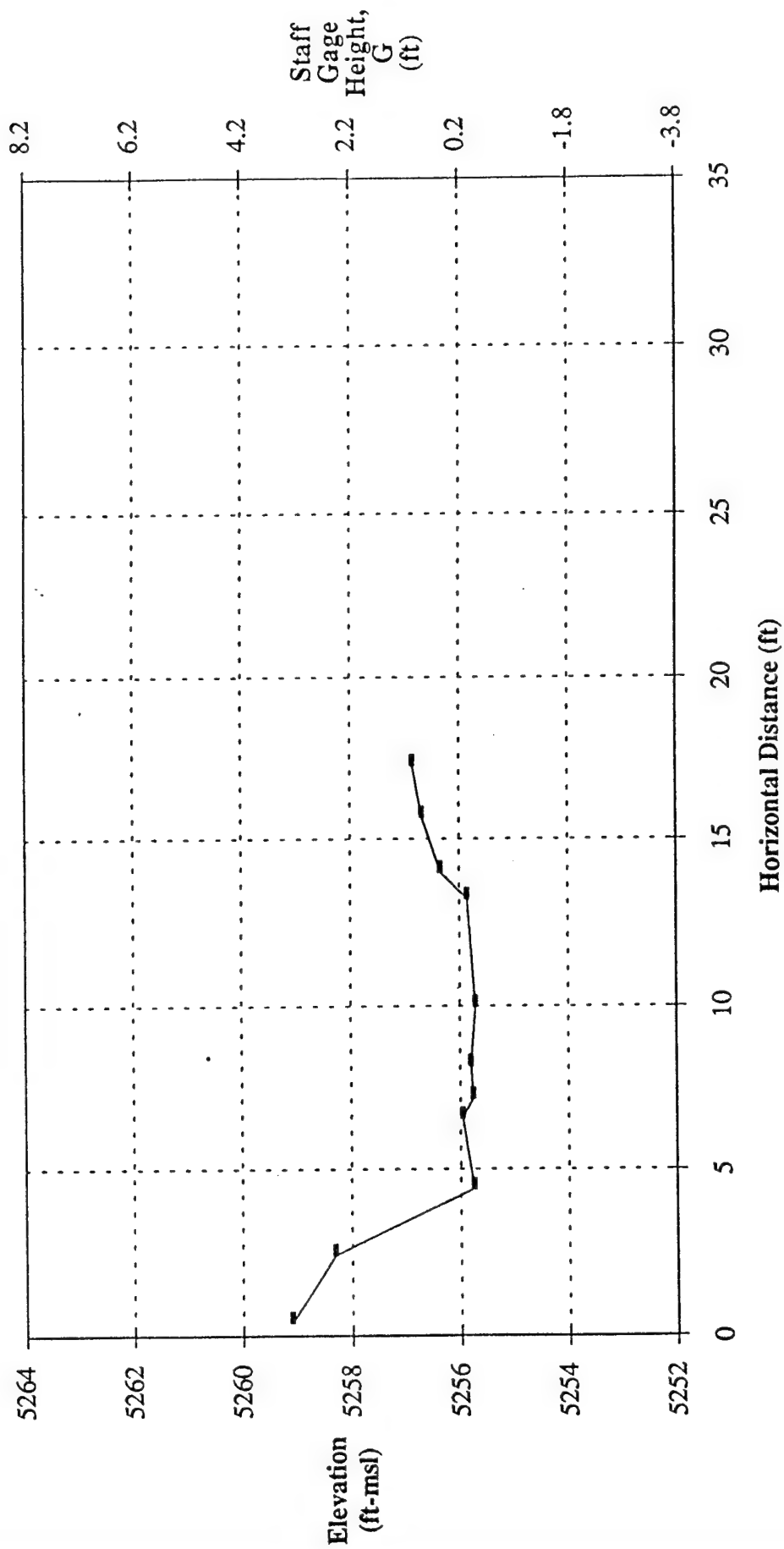
NORTH UVALDA (STATION SW01001)
CROSS SECTION 1



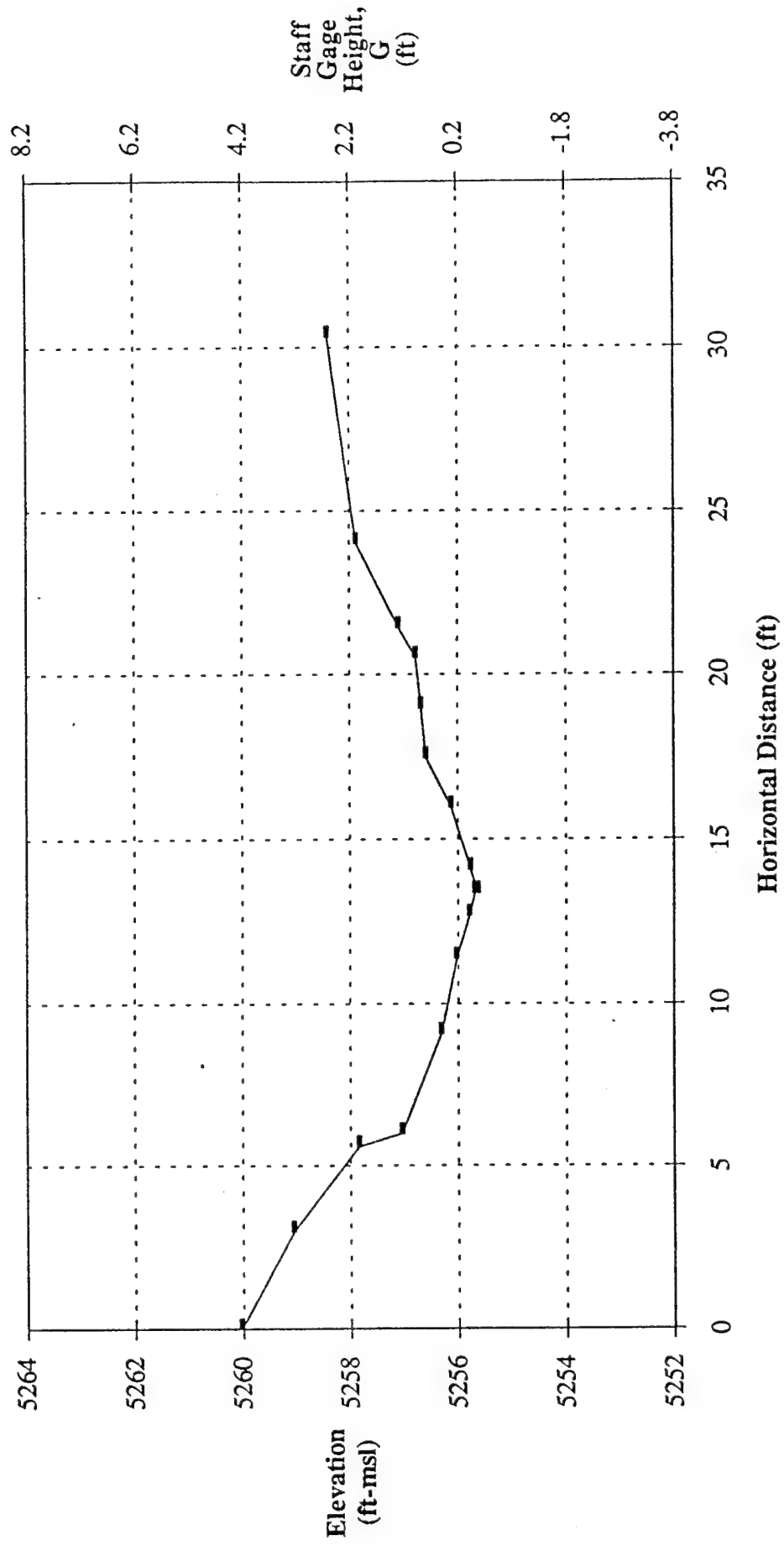
NORTH UVALDA (STATION SW01001)
CROSS SECTION 2



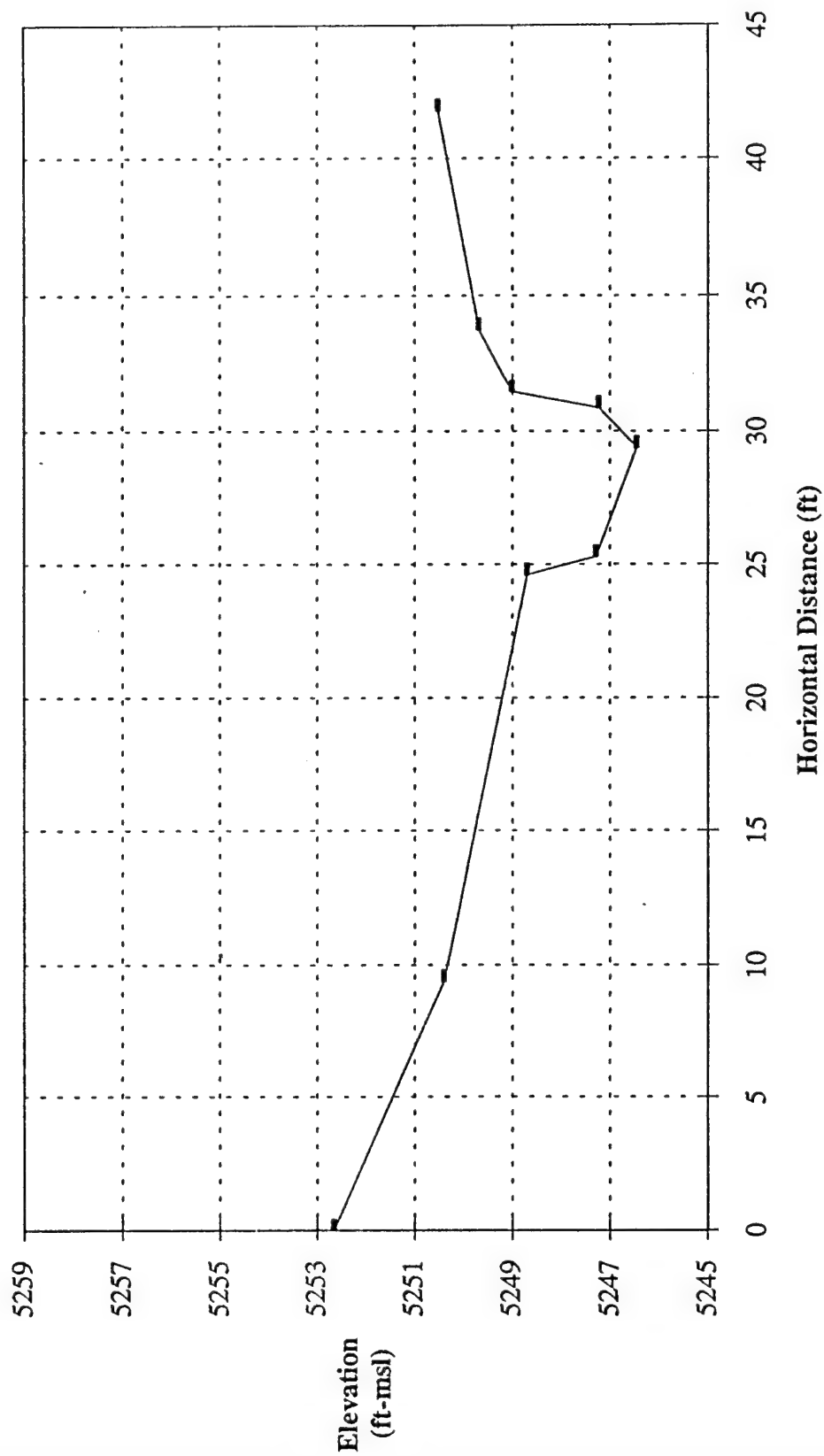
NORTH UVALDA (STATION SW01001)
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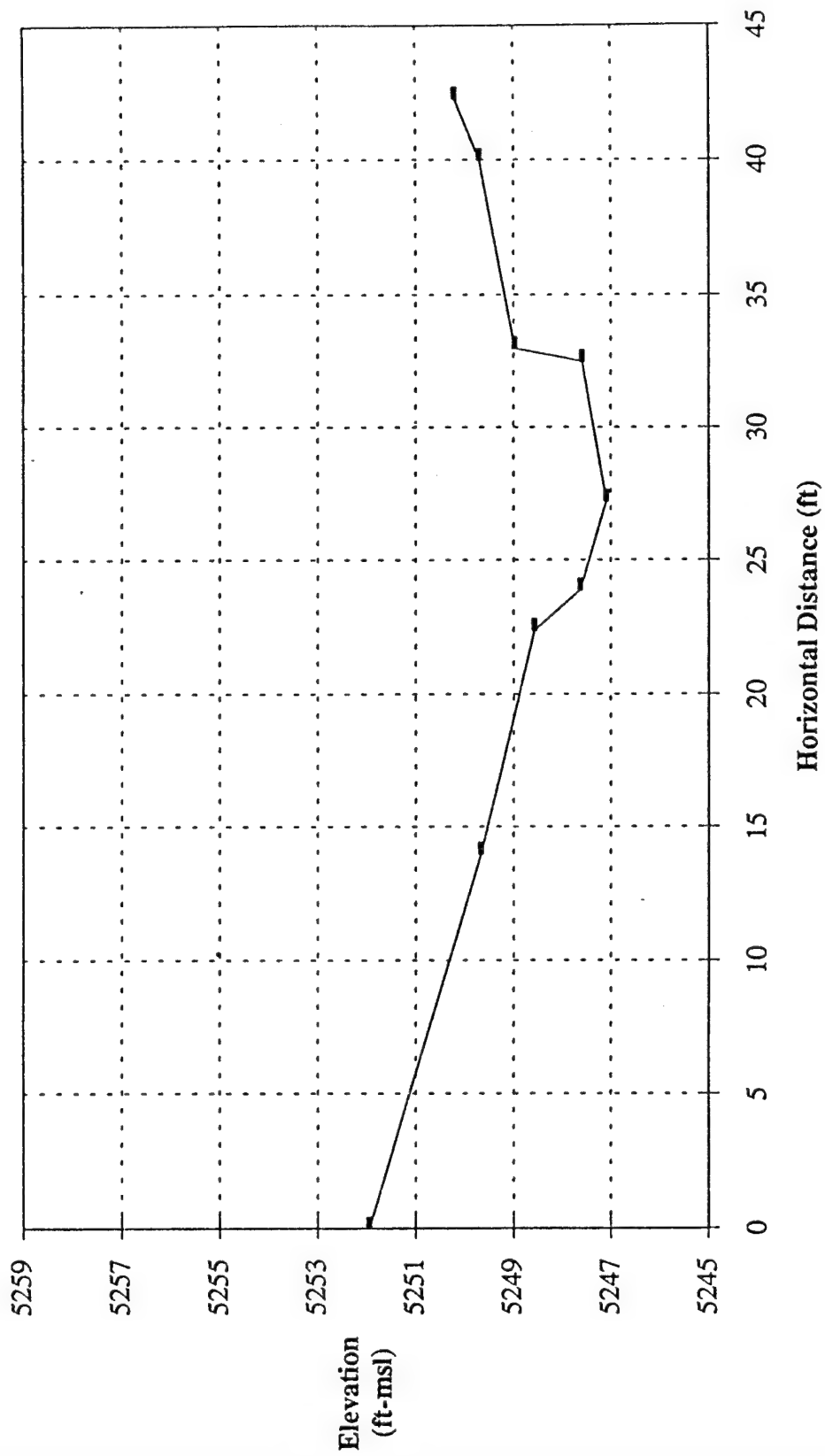
NORTH UVALDA (STATION SW01001) CROSS SECTION 4



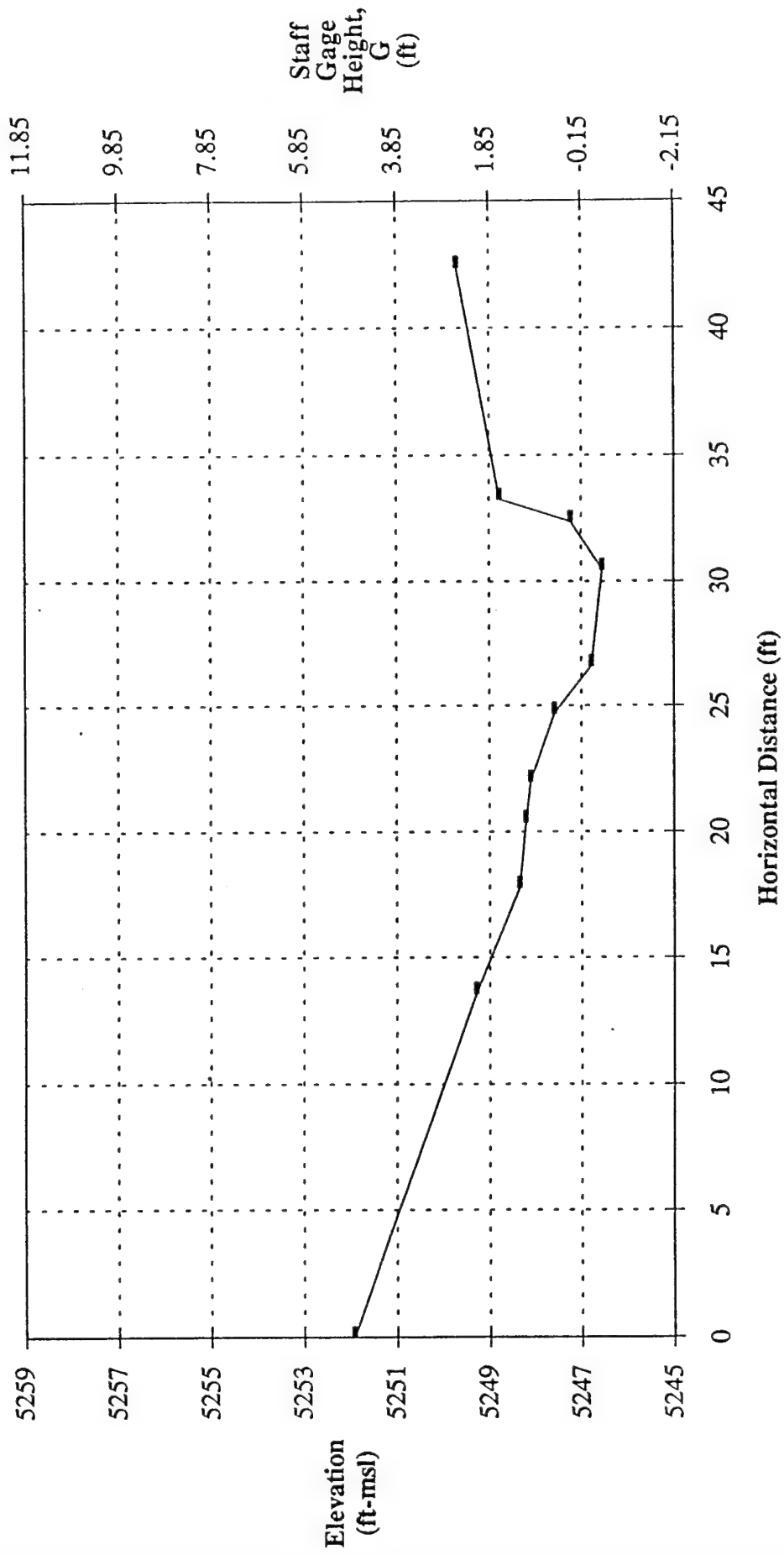
PEORIA INTERCEPTOR (STATION SW11001)
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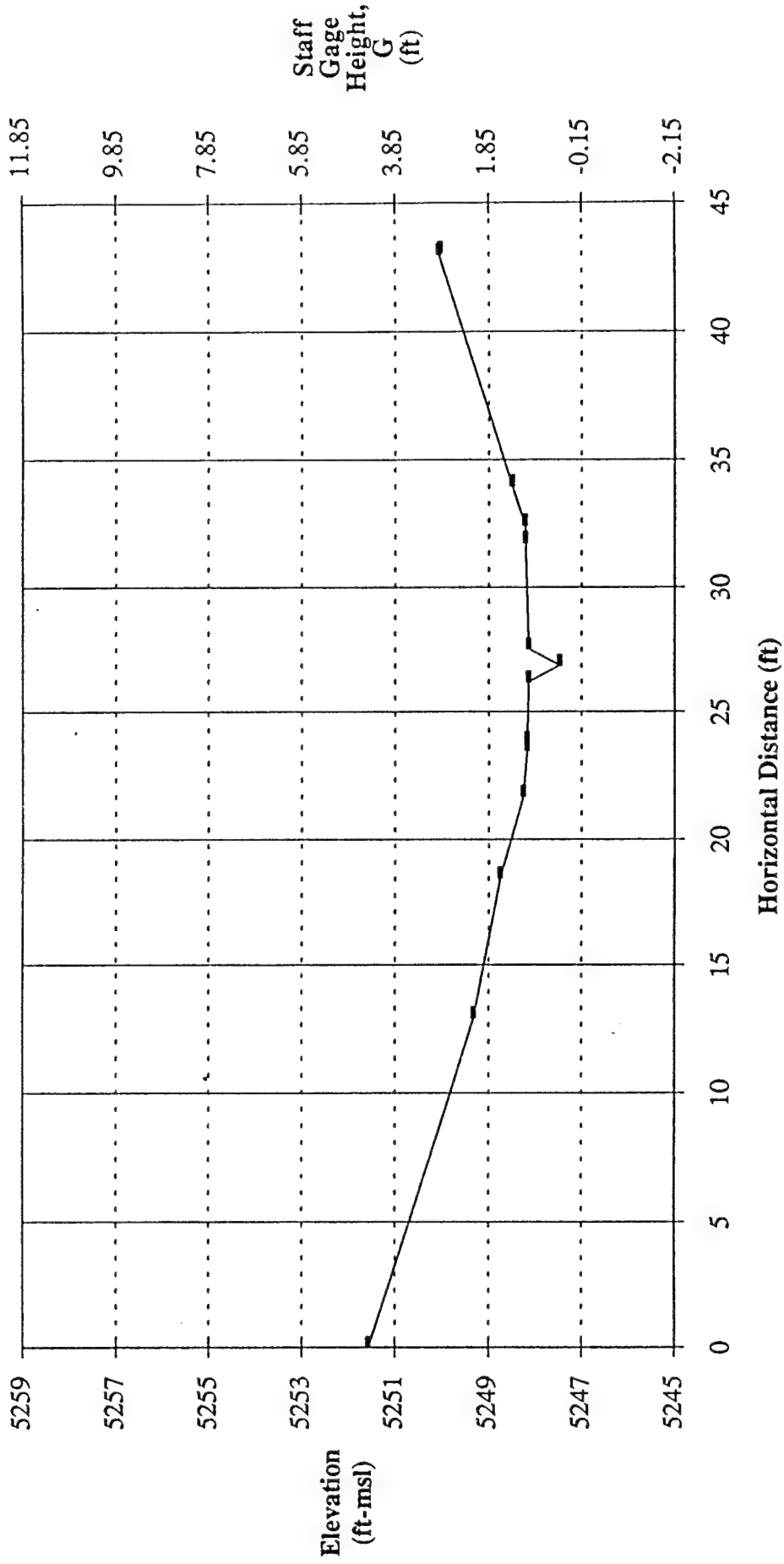
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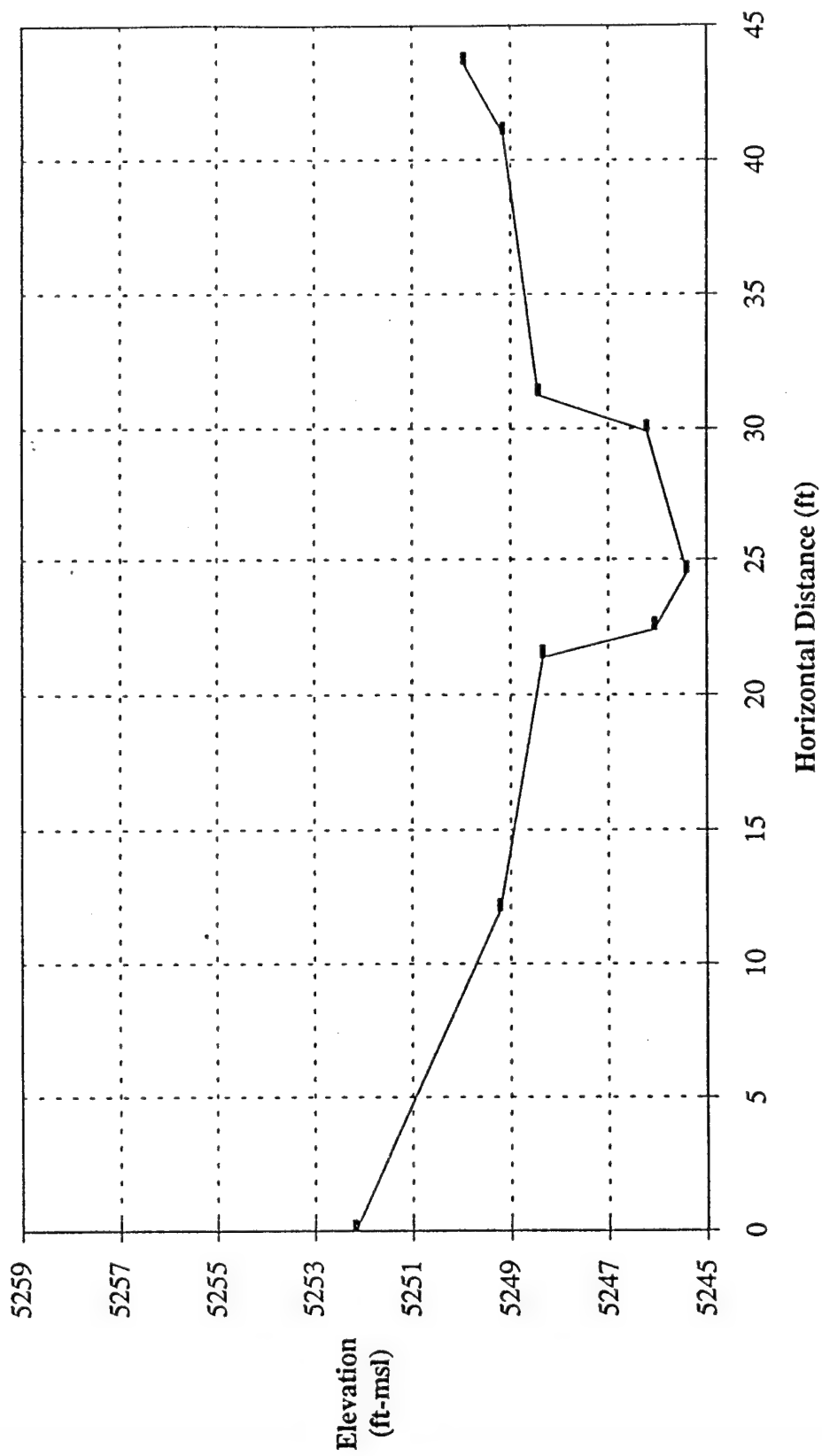
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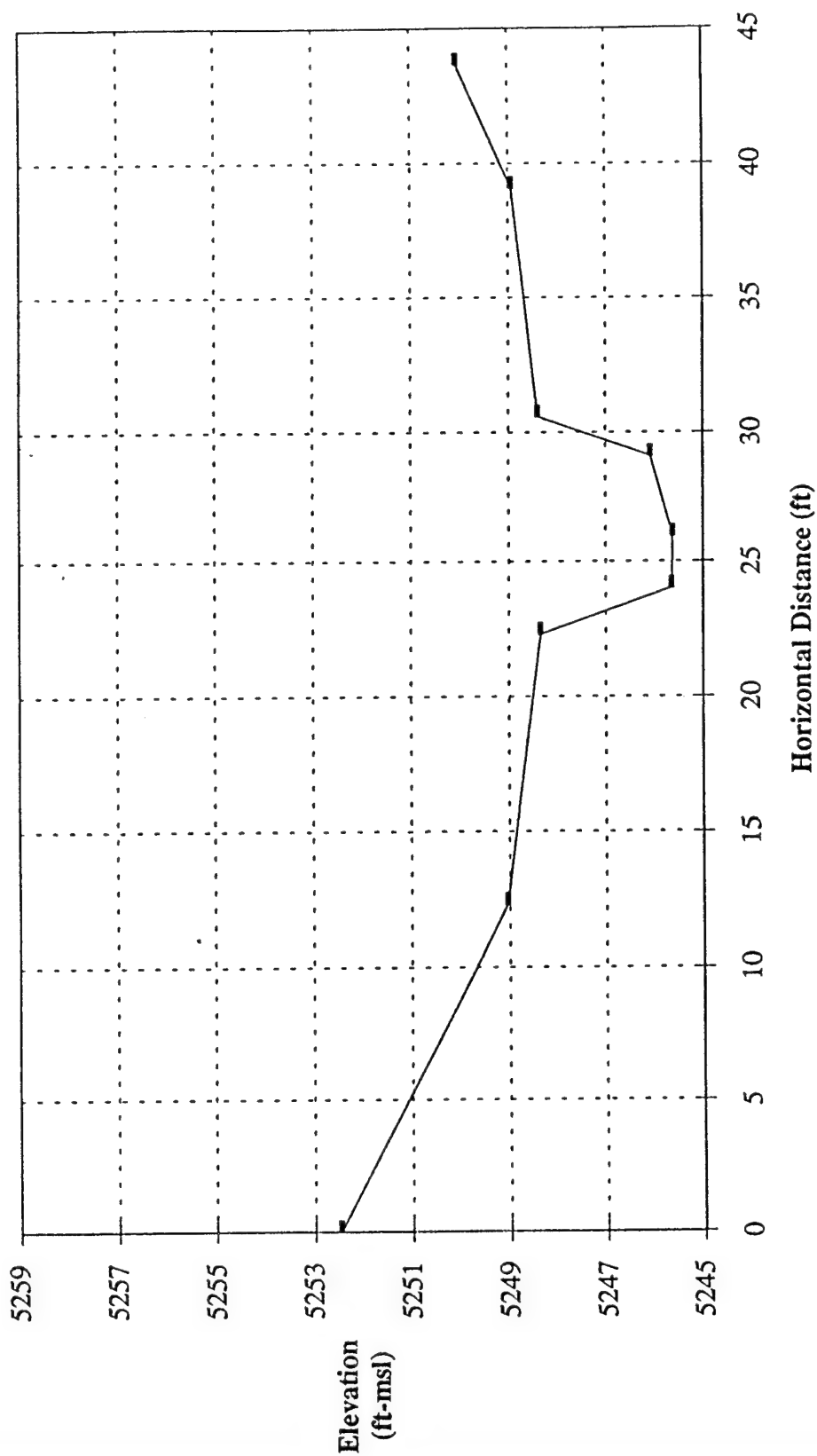
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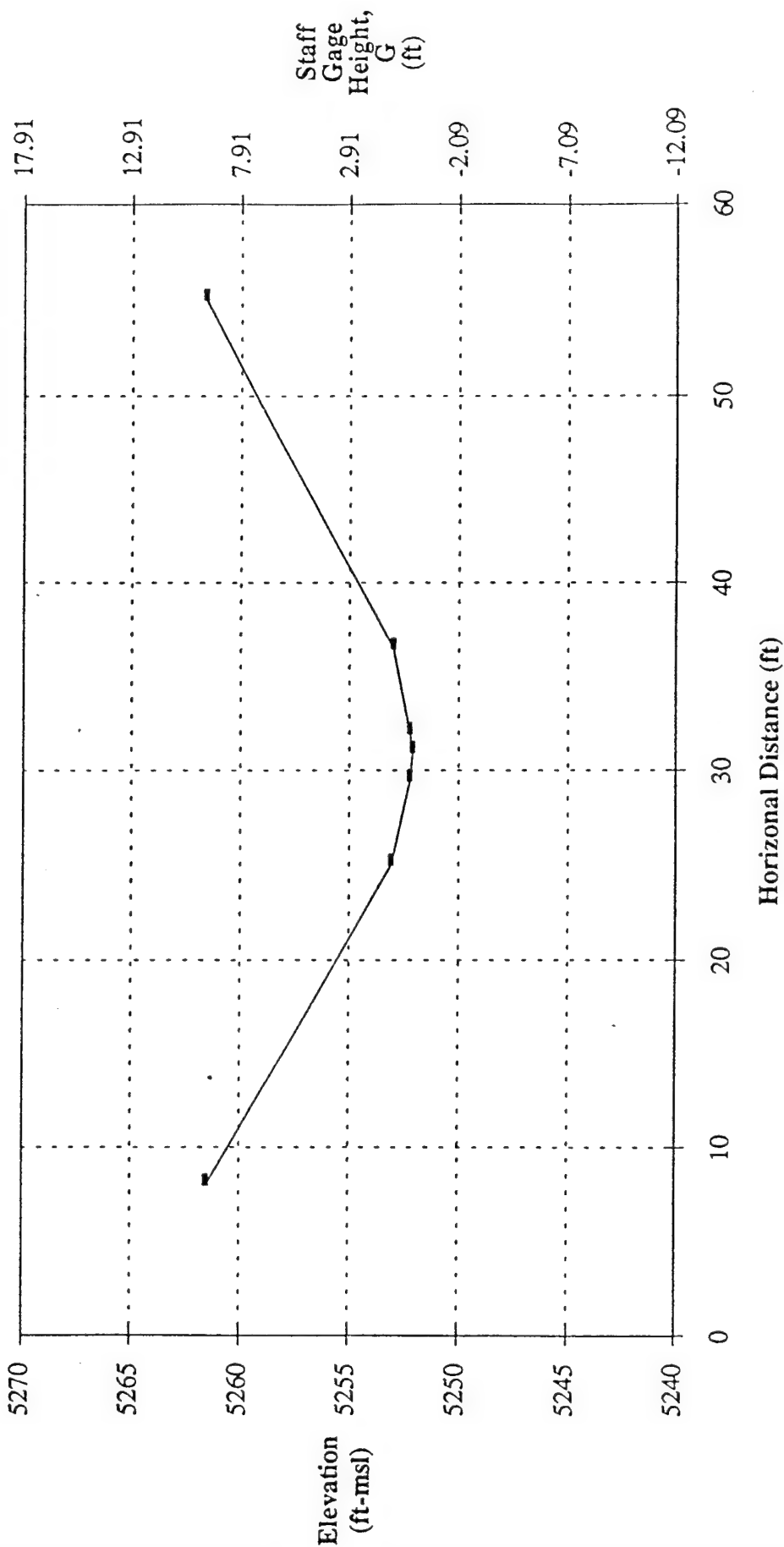
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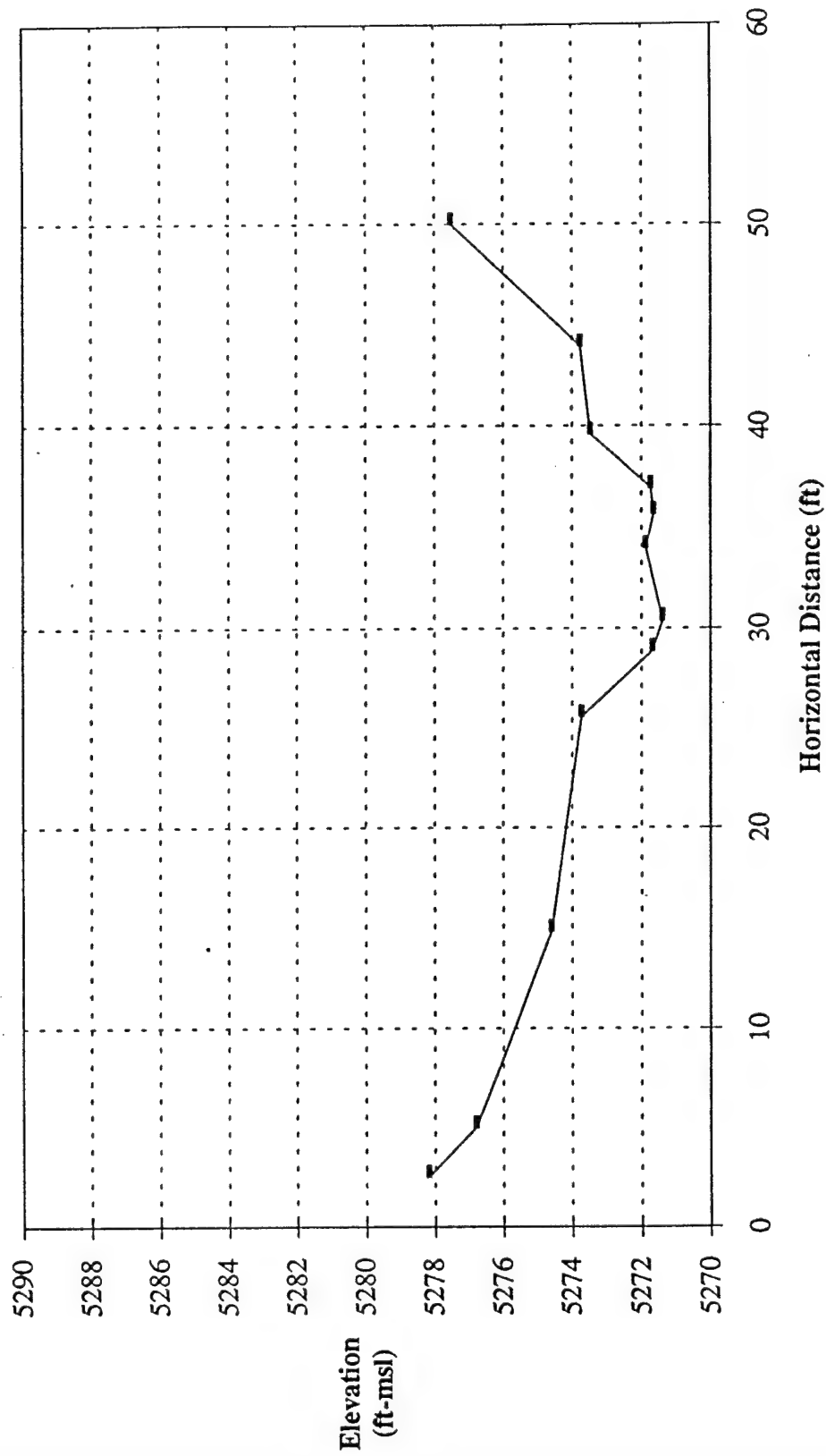
PEORIA INTERCEPTOR (STATION SW11001)
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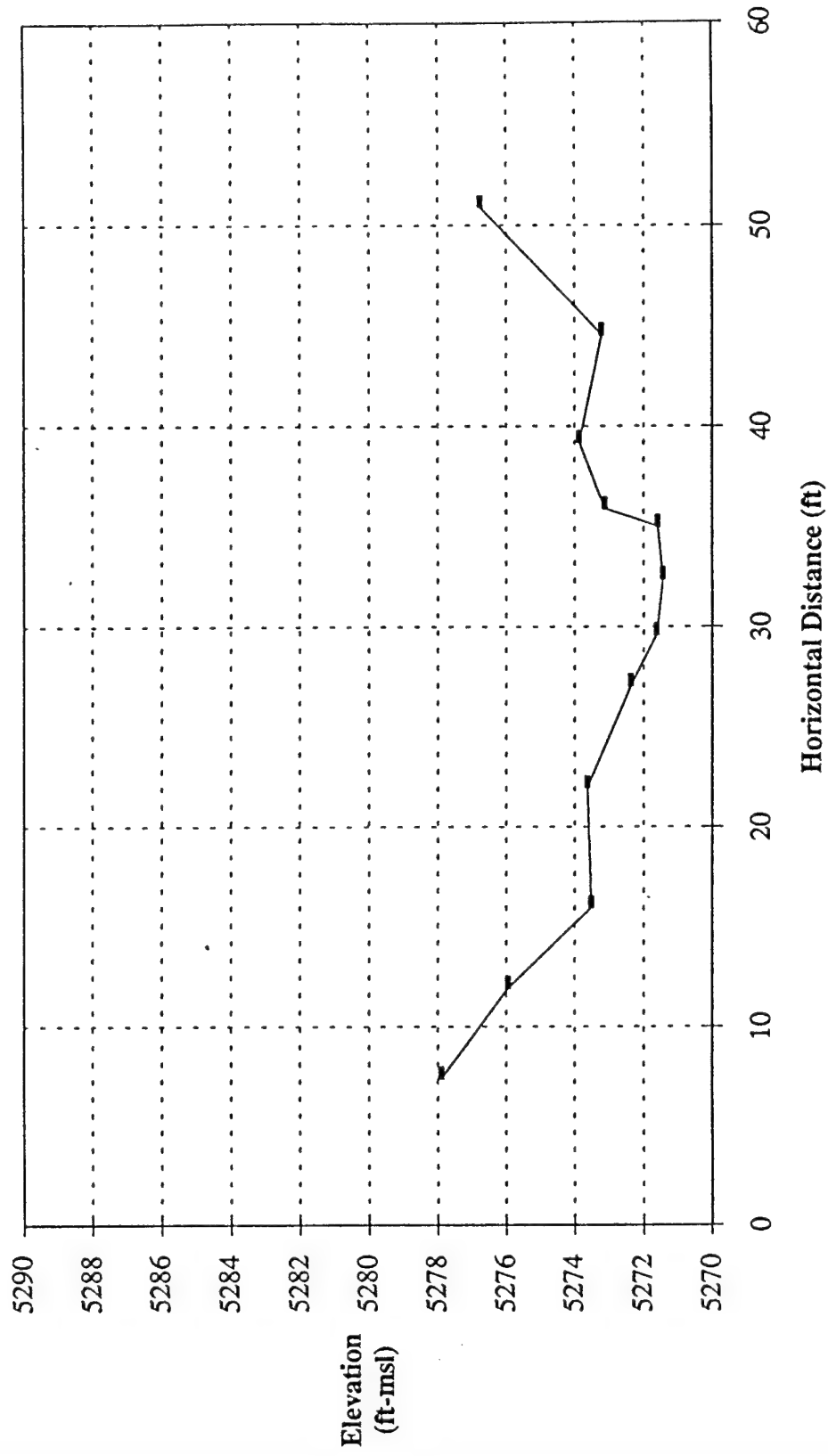
HAVANA INTERCEPTOR (STATION SW11002)
CROSS SECTION 1



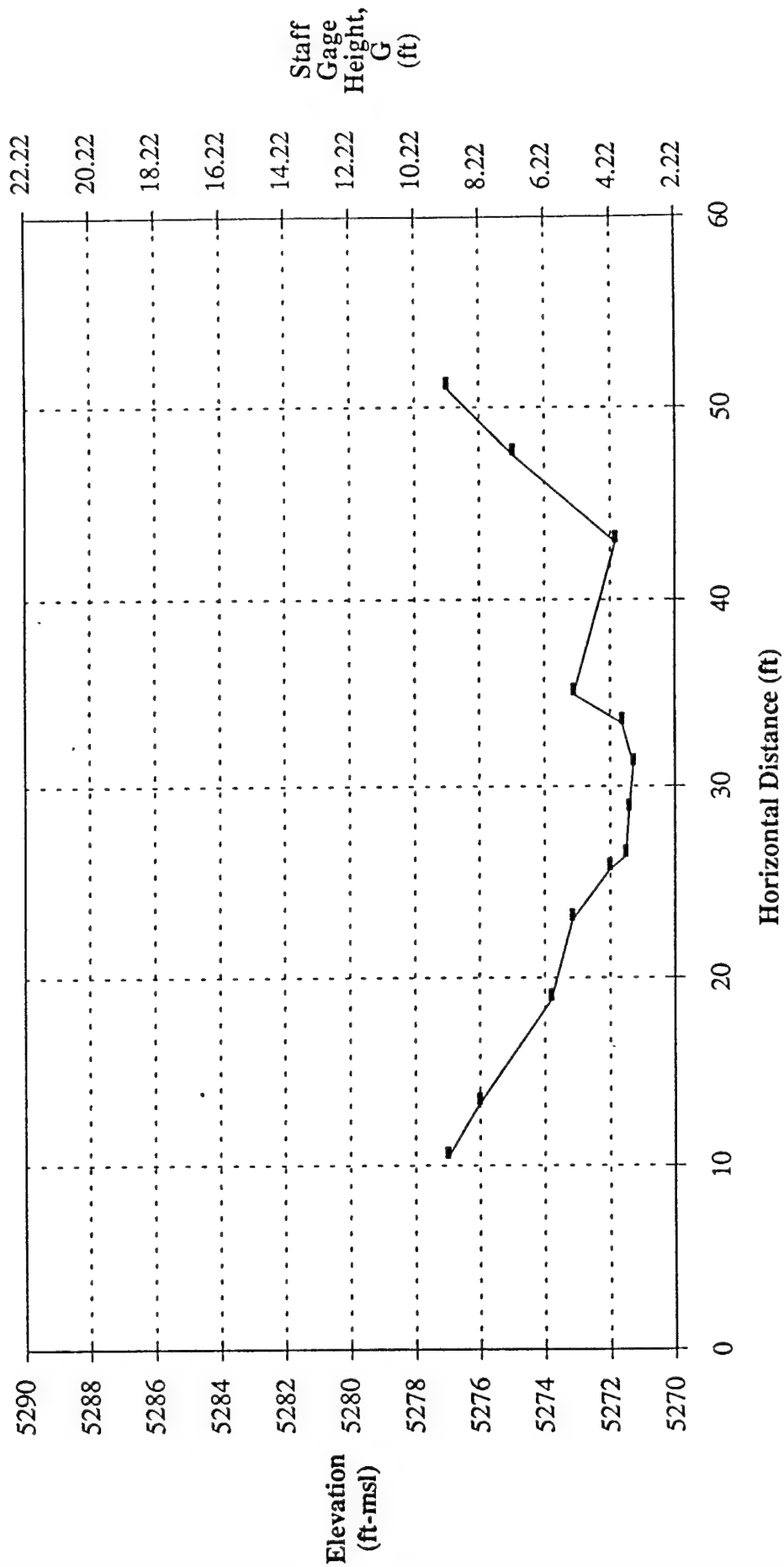
SOUTH UVALDA (STATION 12005)
CROSS SECTION 1



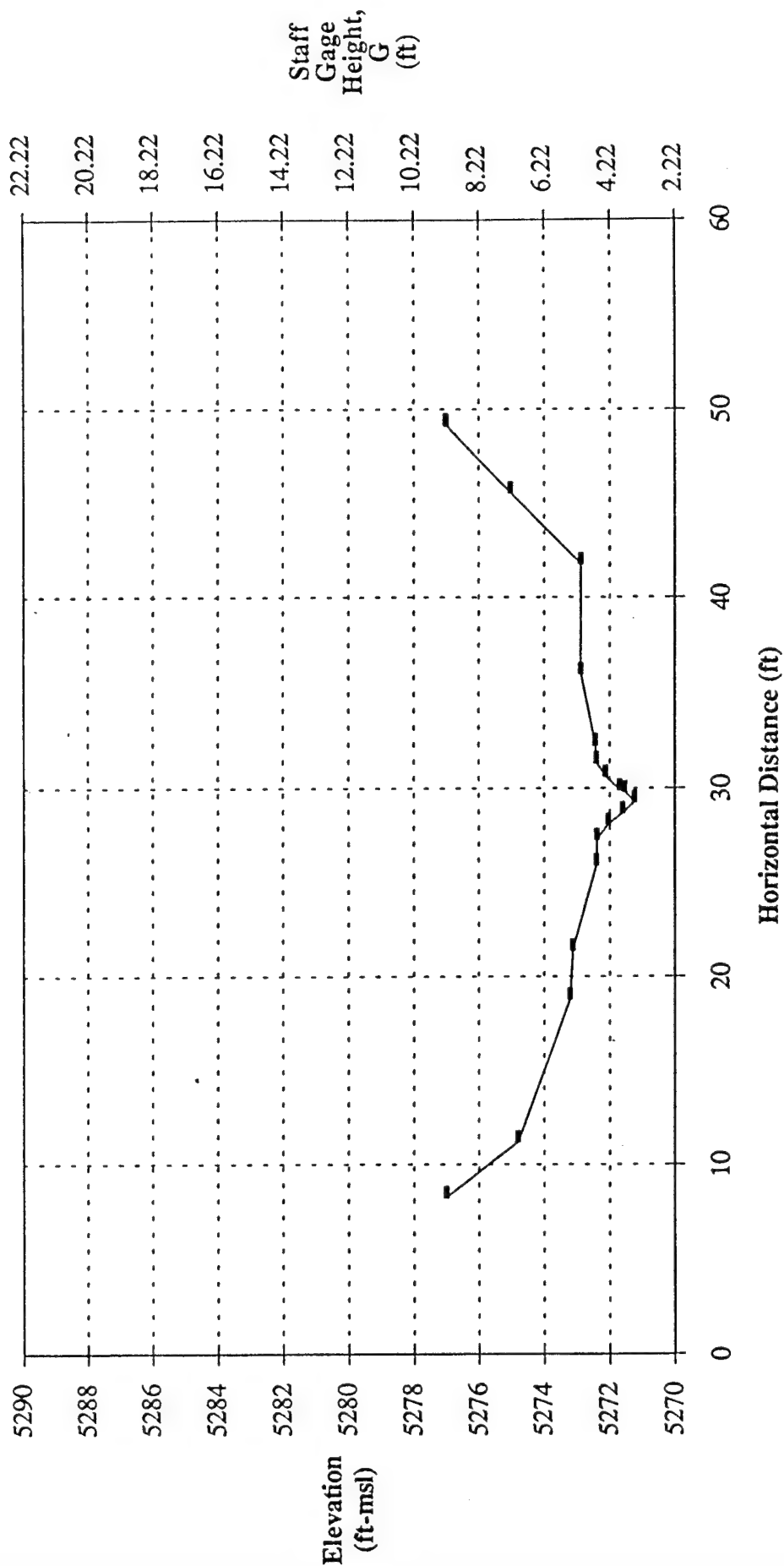
SOUTH UVALDA (STATION 12005)
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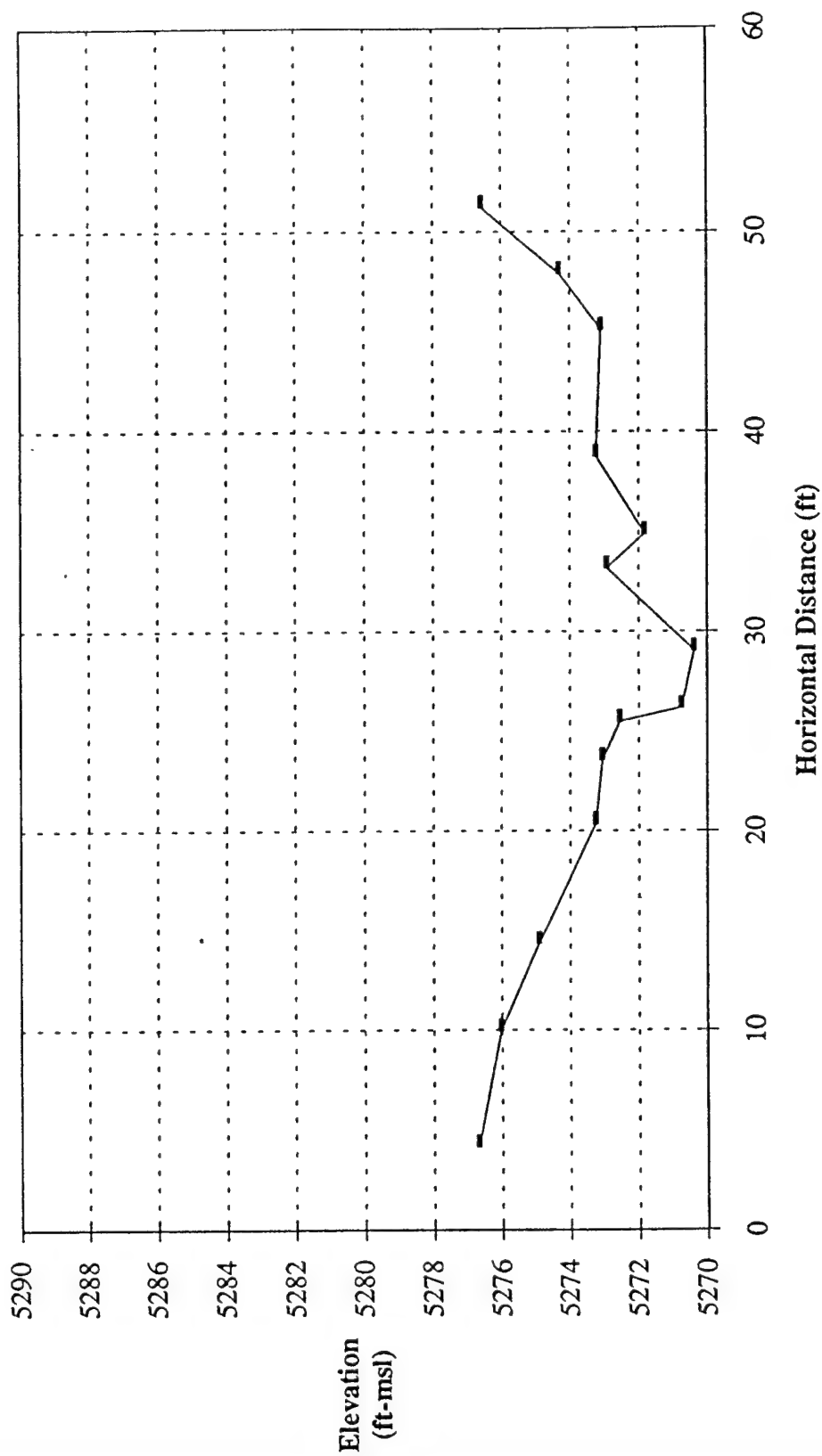
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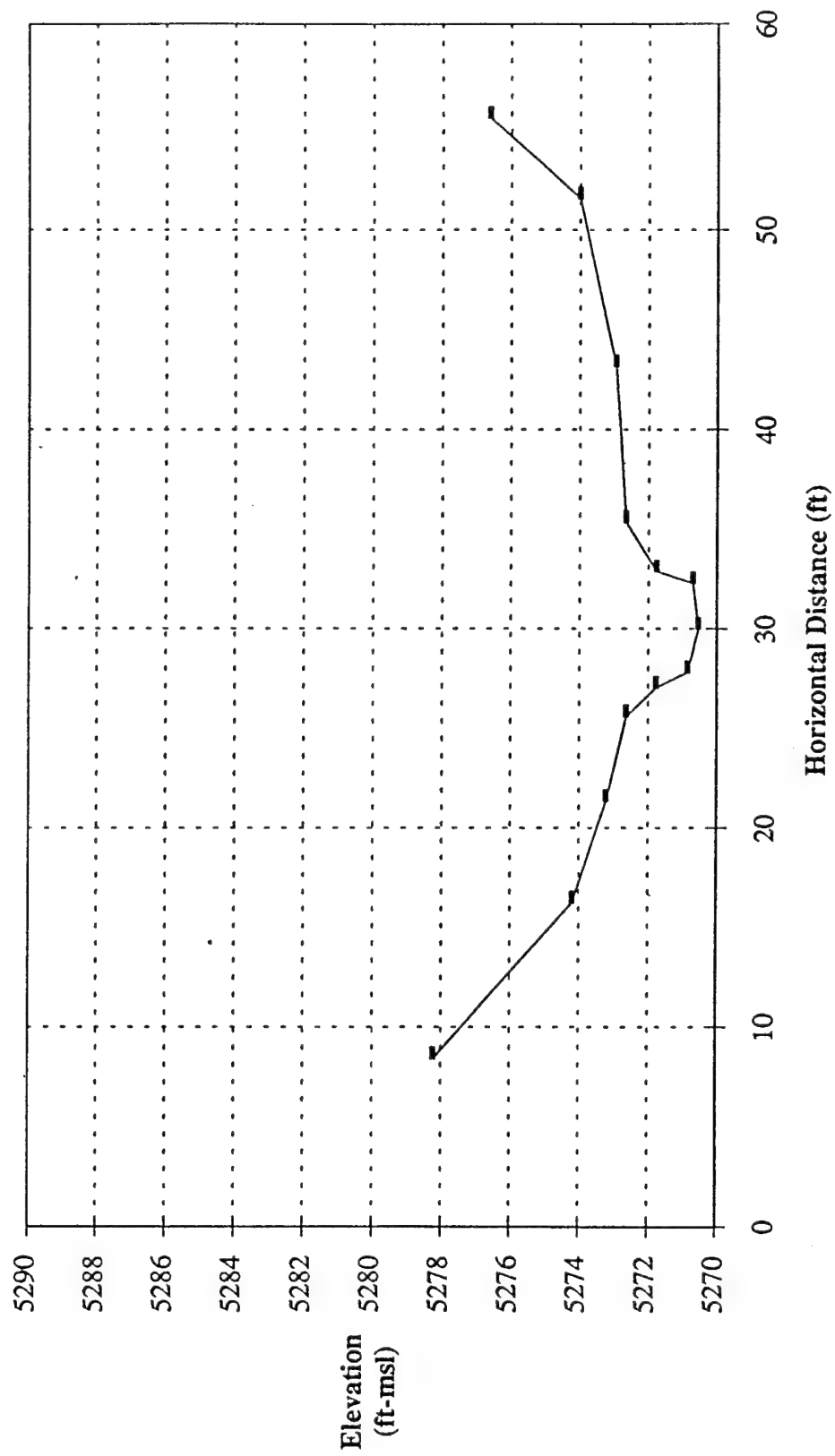
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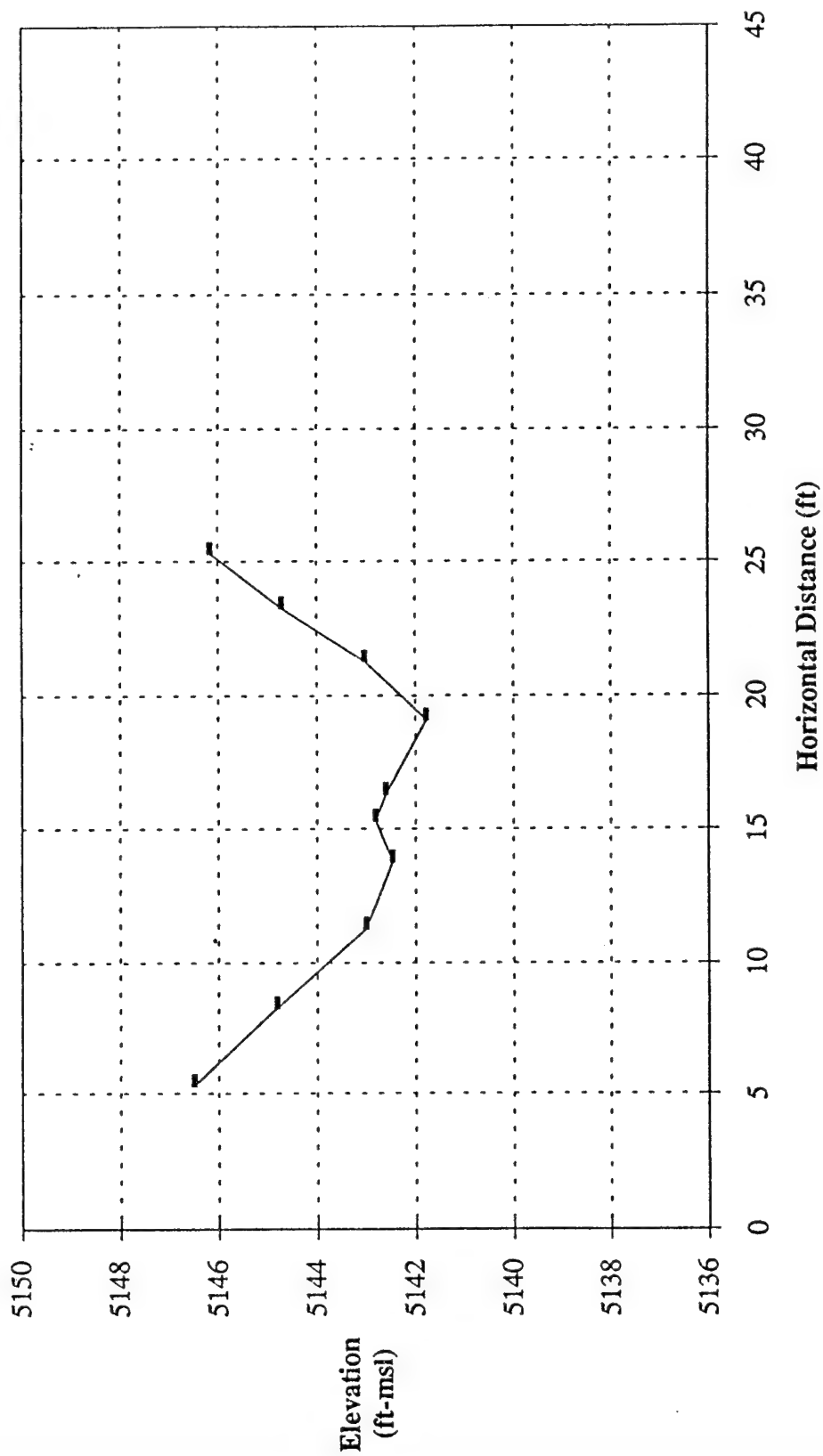
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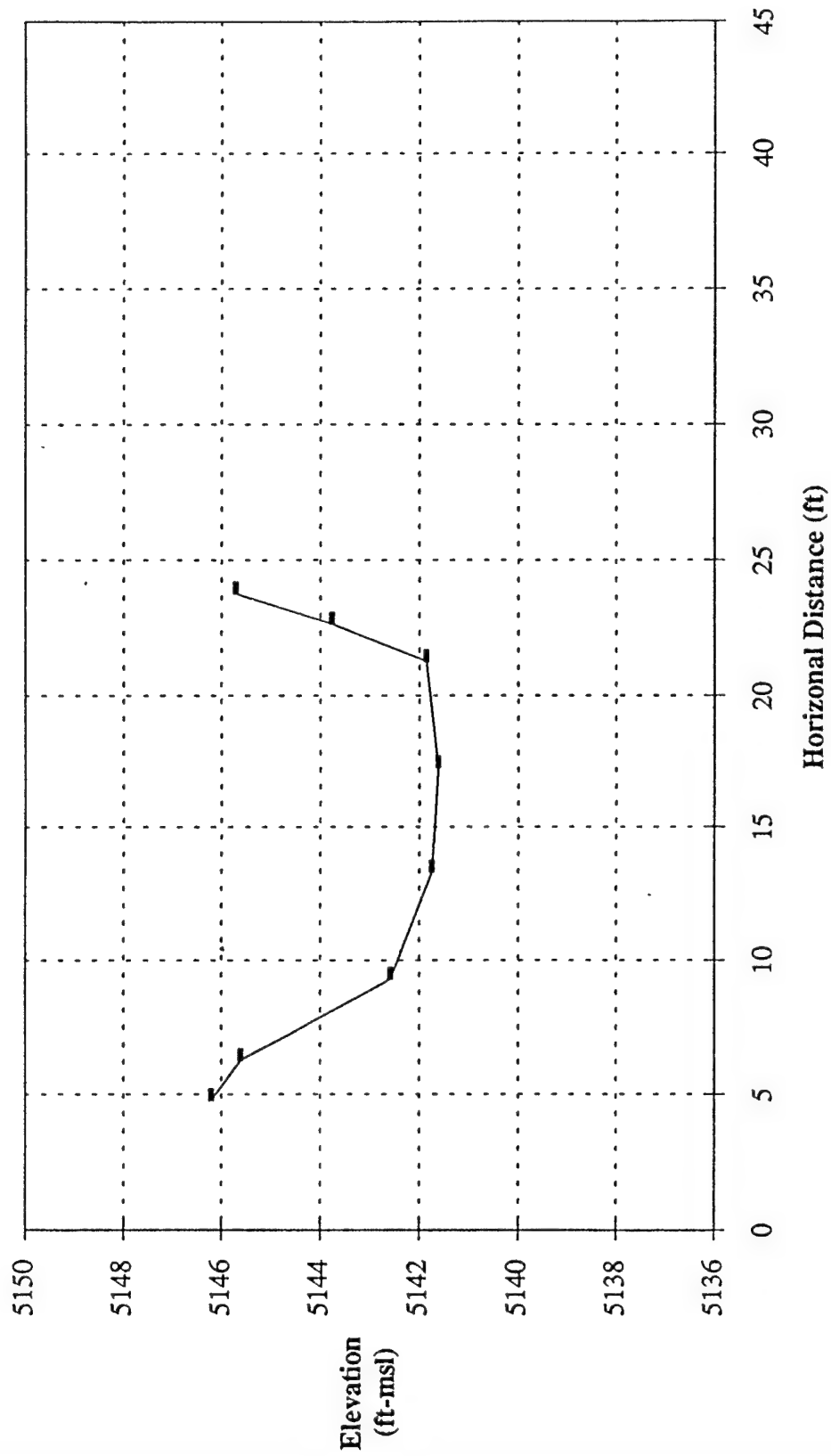
SOUTH UVALDA (STATION SW12005)
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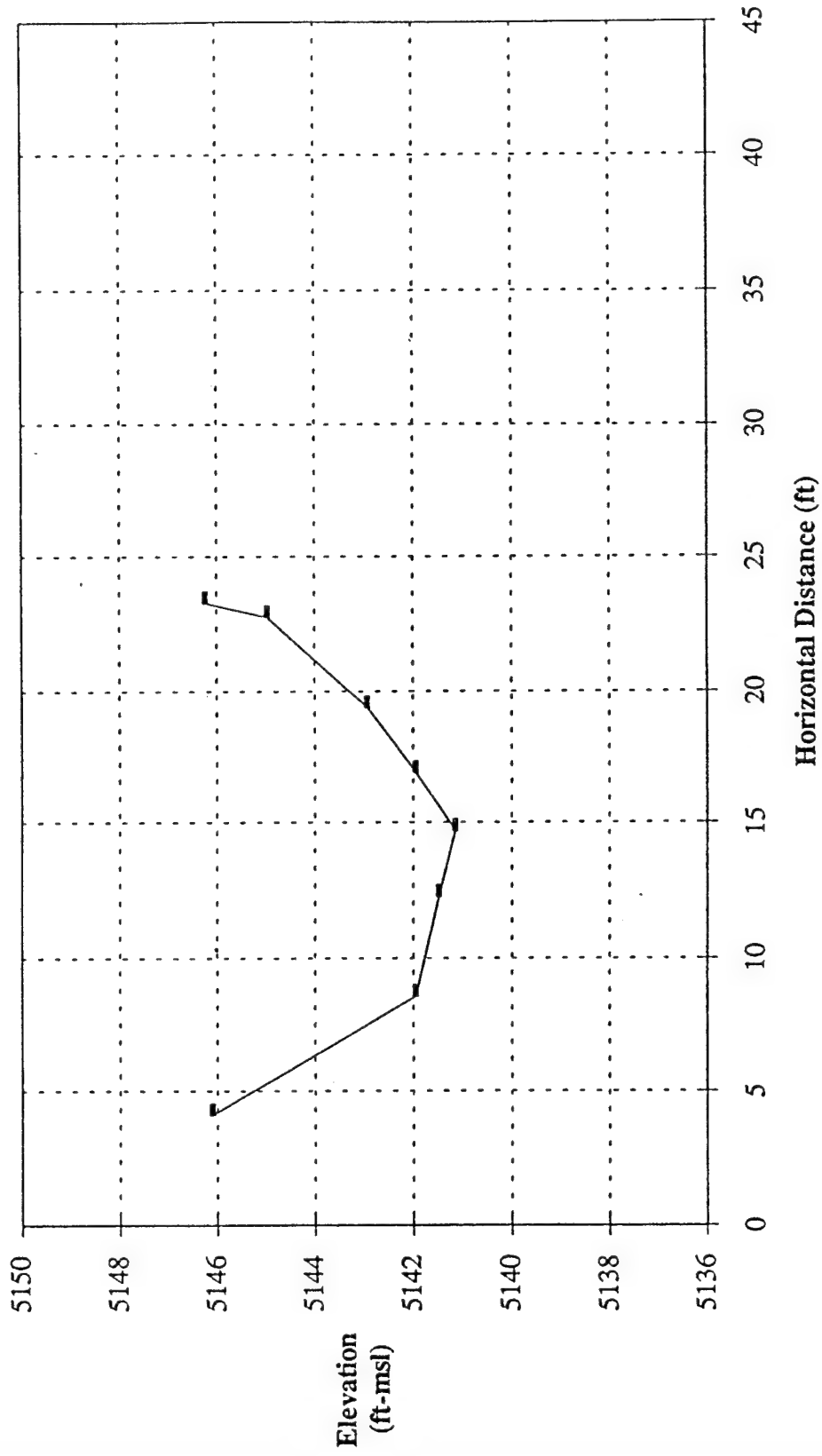
NORTH FIRST CREEK (STATION SW24002)
CROSS SECTION I



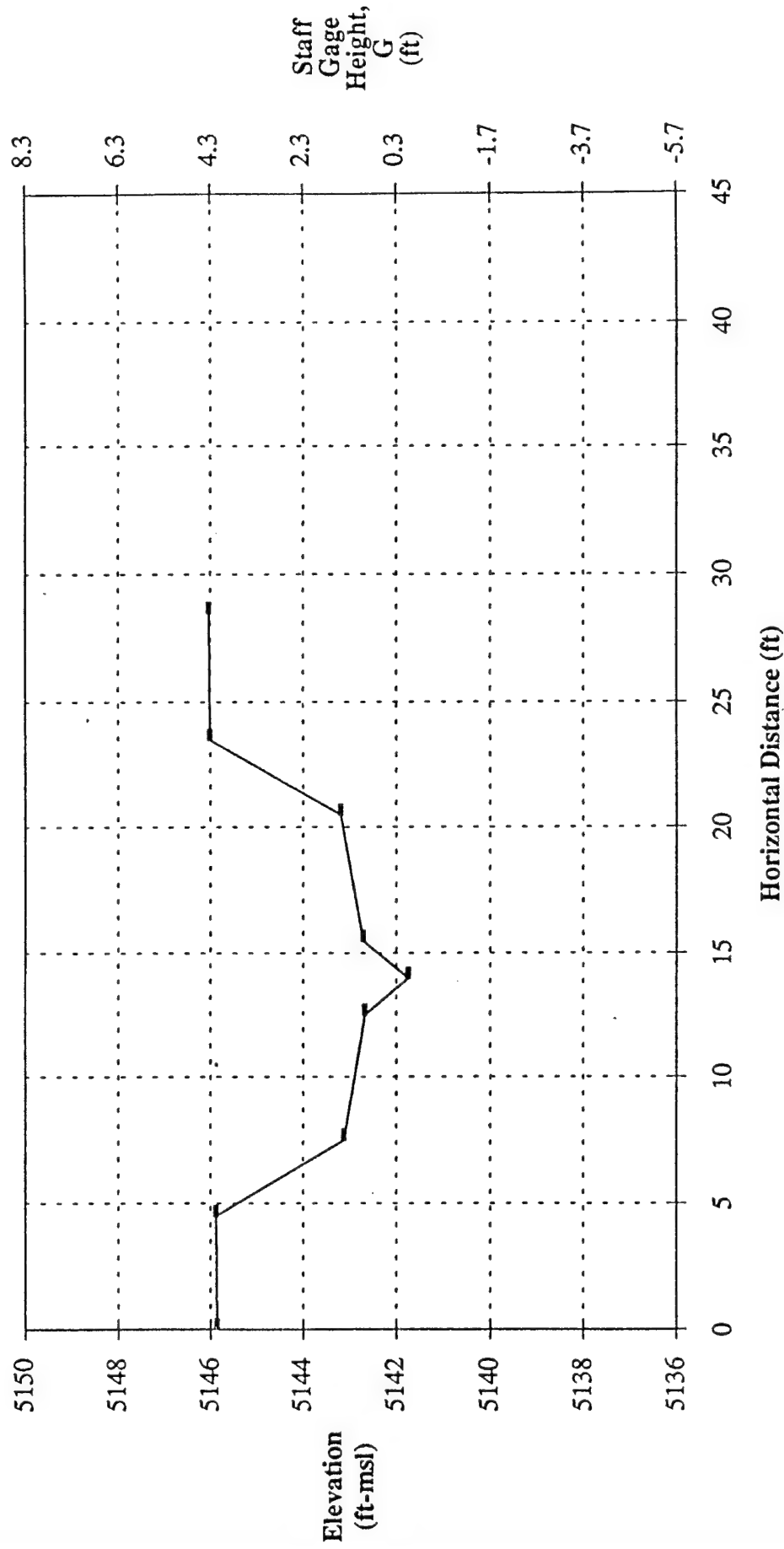
NORTH FIRST CREEK (STATION SW24002)
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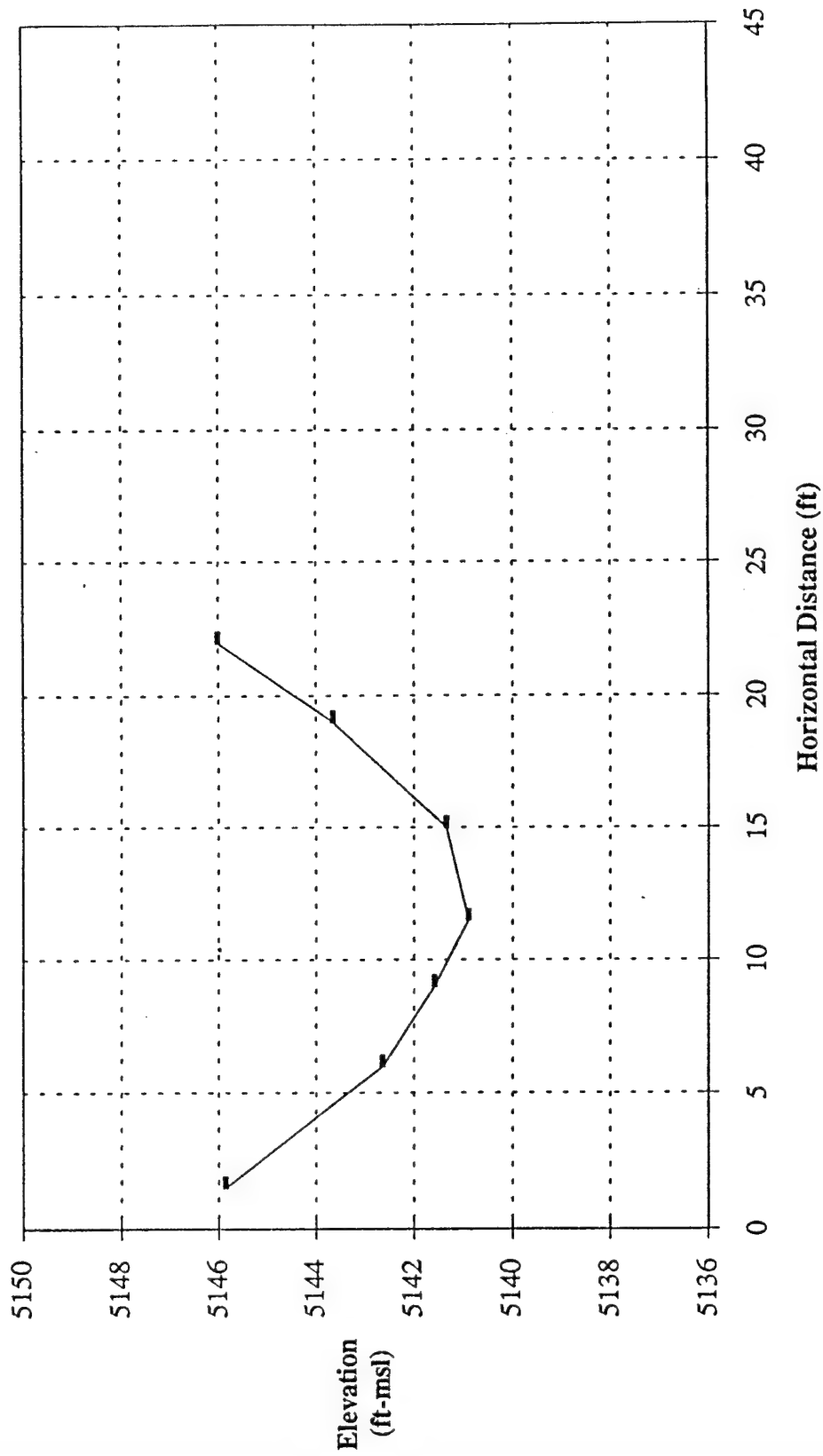
NORTH FIRST CREEK (STATION SW24002)
CROSS SECTION 3



NORTH FIRST CREEK (STATION SW24002) CROSS SECTION 4

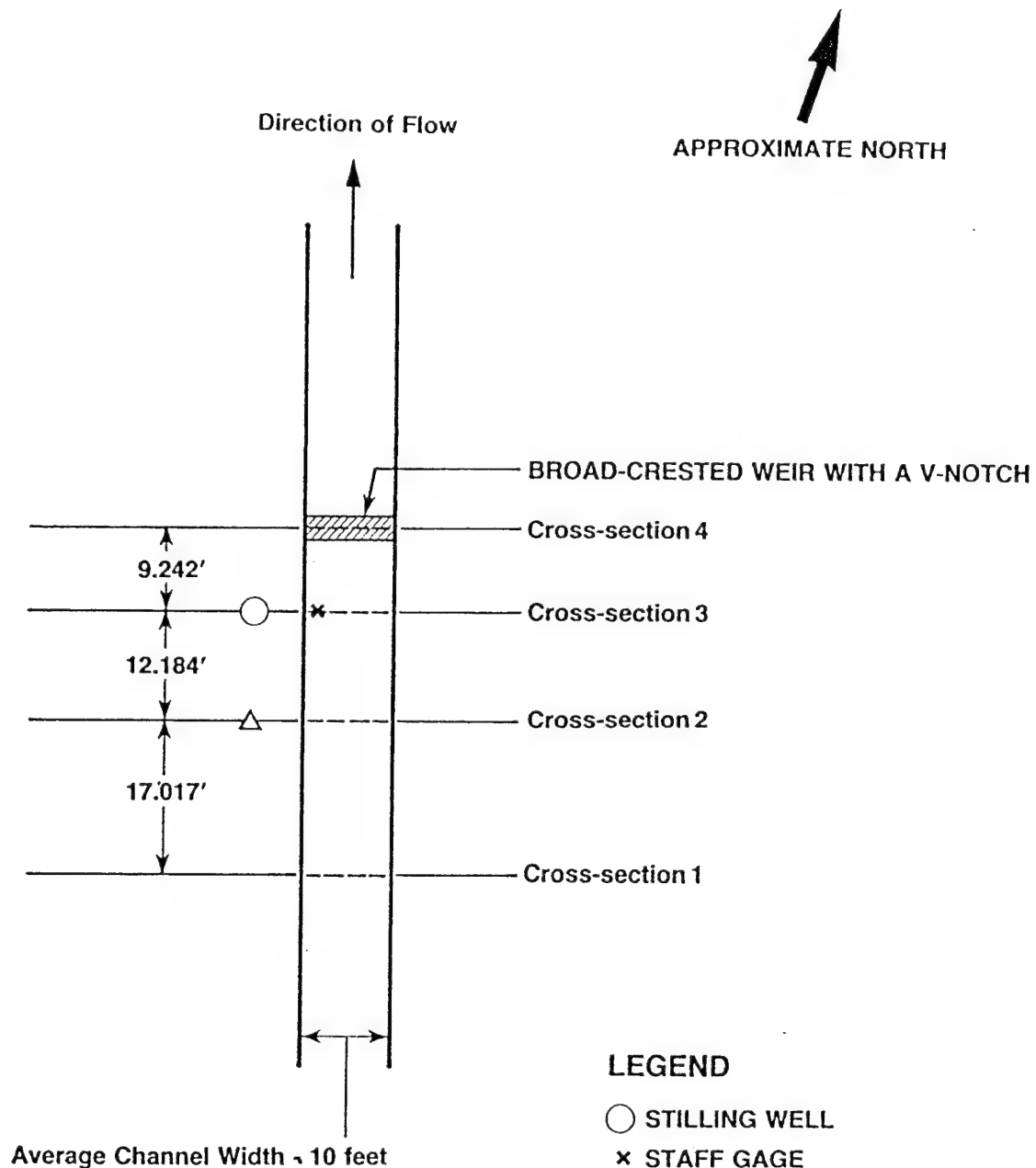


NORTH FIRST CREEK (STATION SW24002)
CROSS SECTION 5



APPENDIX A-1.2.2

Monitoring Station Plan Views



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

Prepared for :

U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

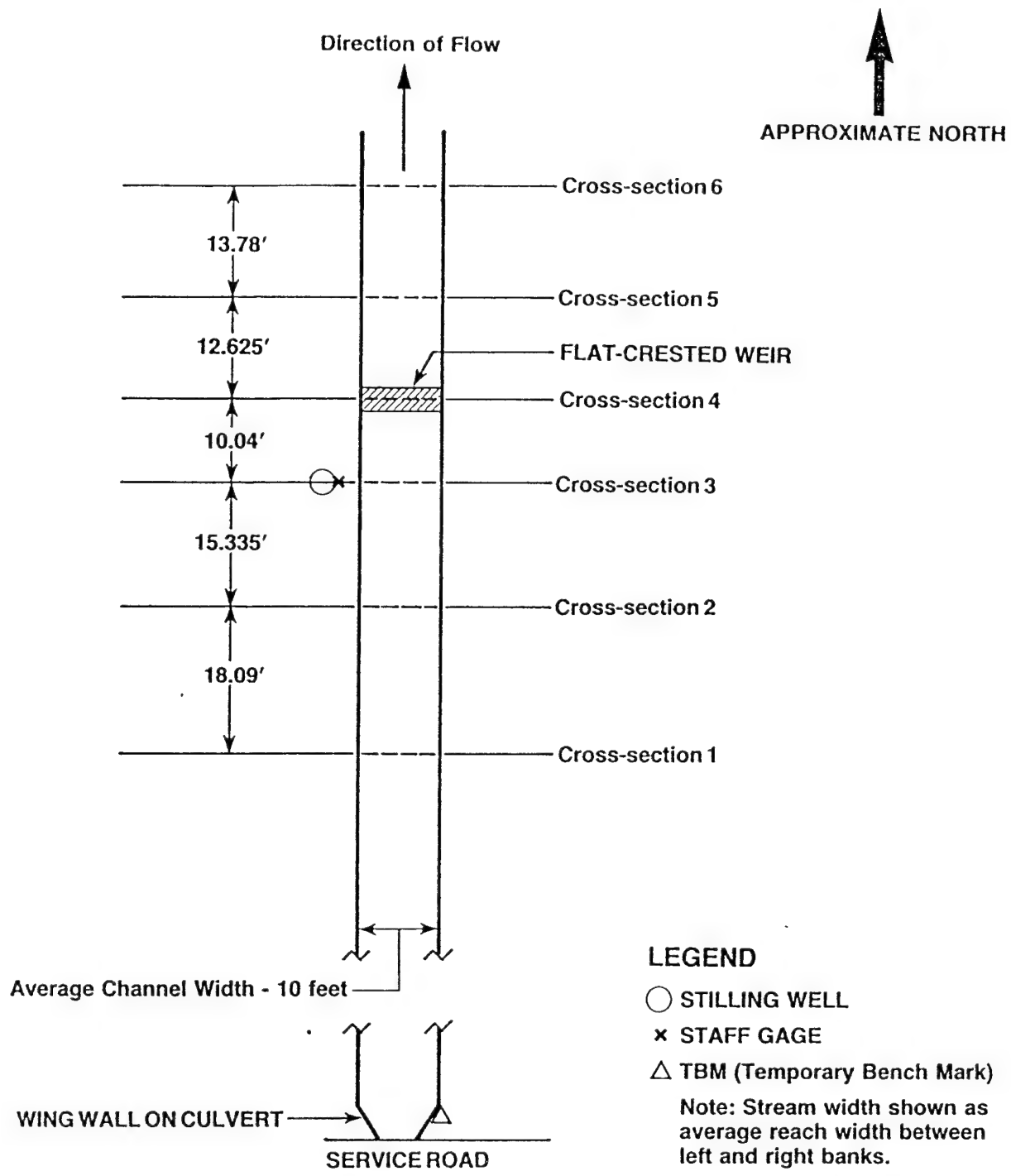
Prepared by :

R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-1

North Uvalda (SW01001)
Cross-Section Locations

CMP SW FY89



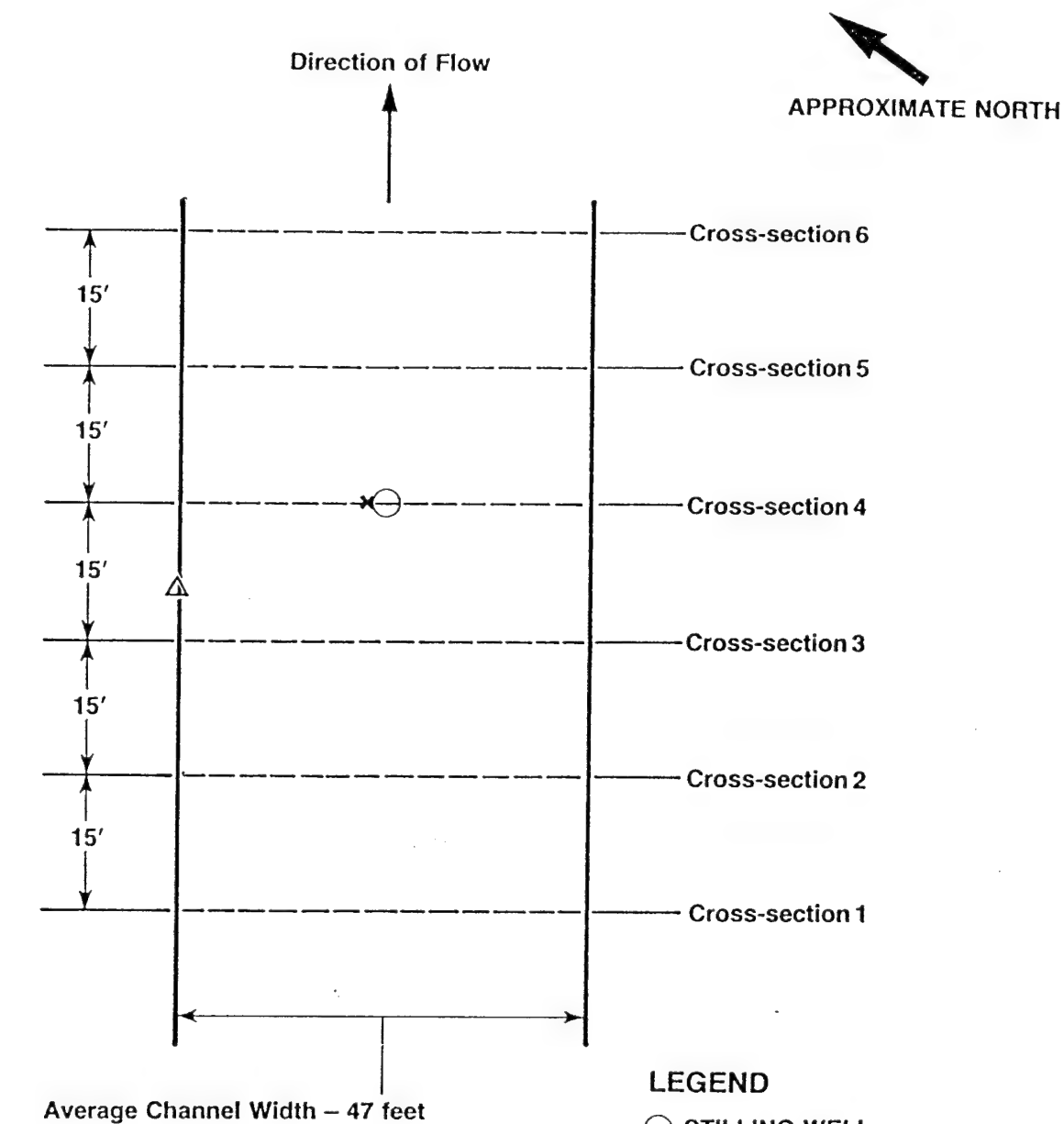
Prepared for :
U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

Prepared by :
R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-2

Peoria Interceptor
(SW11001)

Cross-Section Locations
CMP SW FY89



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

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U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

Prepared by :

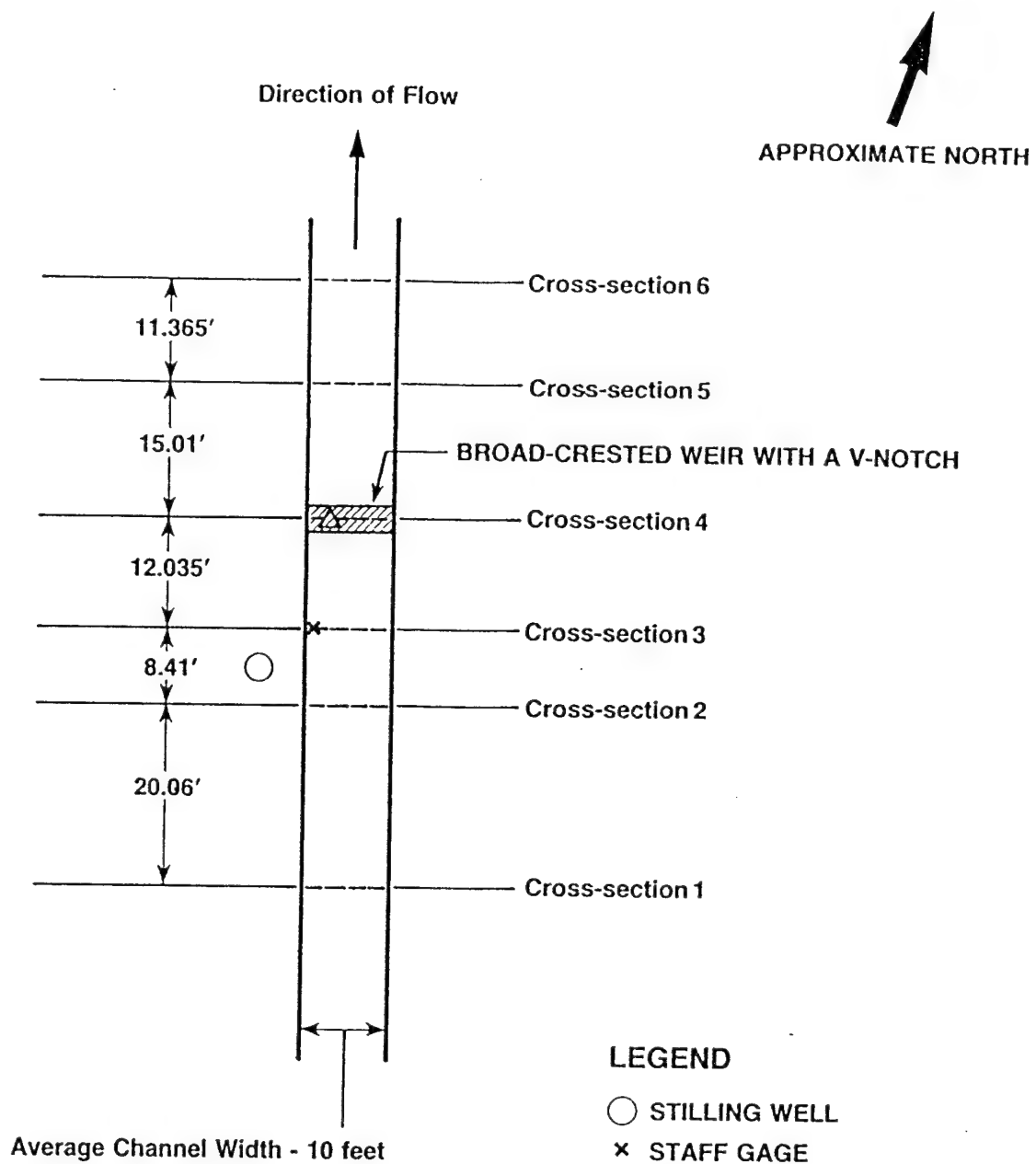
R.L. Stollar & Associates, Inc.
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Figure A-1.2.2-3

Havana Interceptor
(SW11002)

Cross-Section Locations

CMP SW FY89



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

20 feet
SCALE

Prepared for :

U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

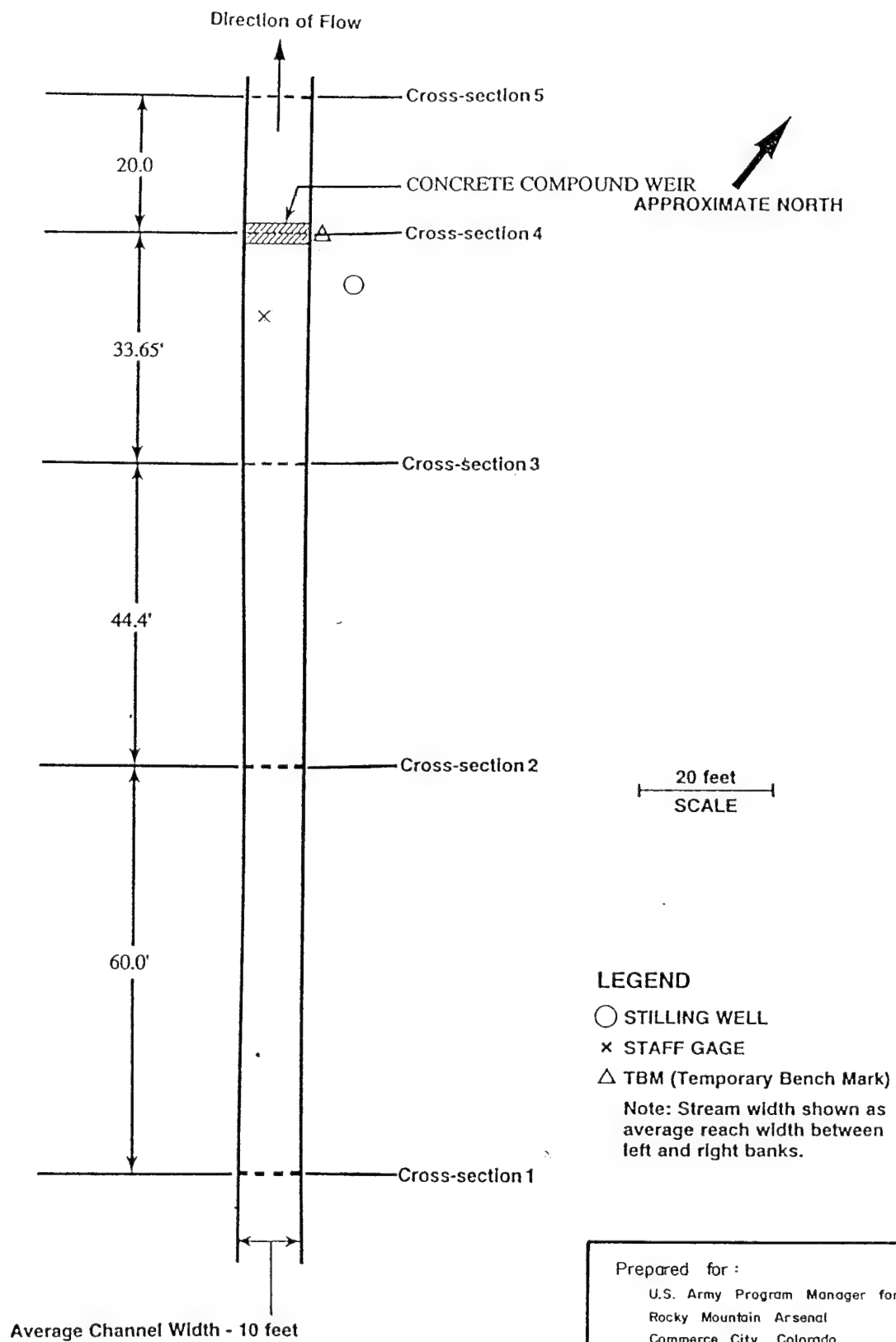
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Figure A-1.2.2-4

South Uvalda (SW 12005)
Cross-Section Locations

CMP SW FY89



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

Prepared for :

U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

Prepared by :

R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-5

North First Creek
(SW24002)

Cross-Section Locations

CMP SW FY89

APPENDIX A-1.2.3

Cross Section Survey Data

Appendix A-1.2.3

Table A-1.2.3-1 North Uvalda (SW01001) Cross Section Survey Data

| Horizontal Distance (ft) | Elevation (ft-msl) | Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|--------------------------------|-----------------------|
| <u>Cross Section 1</u> | | <u>Cross Section 3</u> | |
| 0.00 | 5260.980 | 0.40 | 5259.105 |
| 4.00 | 5259.310 | 2.40 | 5258.305 |
| 6.30 | 5257.915 | 4.40 | 5255.750 |
| 7.90 | 5256.425 | 6.60 | 5255.955 |
| 10.20 | 5255.925 | 7.20 | 5255.760 |
| 12.20 | 5256.090 | 8.20 | 5255.800 |
| 13.60 | 5255.805 | 10.00 | 5255.715 |
| 17.90 | 5255.925 | 13.20 | 5255.855 |
| 18.60 | 5256.370 | 14.00 | 5256.350 |
| 19.40 | 5256.655 | 15.70 | 5256.690 |
| 21.20 | 5257.445 | 17.30 | 5256.855 |
| 22.50 | 5257.550 | | |
| <u>Cross Section 2</u> | | <u>Cross Section 4</u> | |
| 0.00 | 5259.740 | 0.00 | 5260.040 |
| 4.00 | 5258.070 | 3.00 | 5259.055 |
| 6.00 | 5256.995 | 5.60 | 5257.840 |
| 7.50 | 5255.810 | 6.00 | 5257.040 |
| 10.00 | 5255.745 | 9.10 | 5256.315 |
| 11.70 | 5255.695 | 11.40 | 5256.025 |
| 12.60 | 5255.865 | 12.70 | 5255.790 |
| 14.70 | 5255.930 | 13.40 | 5255.695 |
| 15.70 | 5256.525 | 14.10 | 5255.775 |
| 19.40 | 5257.535 | 16.00 | 5256.125 |
| 24.50 | 5256.675 | 17.50 | 5256.585 |
| 28.50 | 5258.010 | 19.00 | 5256.675 |
| | | 20.50 | 5256.775 |
| | | 21.40 | 5257.095 |
| | | 24.00 | 5257.880 |
| | | 30.30 | 5258.400 |

Appendix A-1.2.3

Table A-1.2.3-2 Peoria Interceptor (SW11001) Cross Section Survey Data

| Horizontal Distance (ft) | Elevation (ft-msl) | Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|--------------------------------|-----------------------|
| <u>Cross Section 1</u> | | <u>Cross Section 4</u> | |
| 0.00 | 5252.665 | 0.00 | 5251.580 |
| 9.40 | 5250.400 | 12.90 | 5249.315 |
| 24.60 | 5248.695 | 18.50 | 5248.760 |
| 25.30 | 5247.295 | 21.70 | 5248.260 |
| 29.40 | 5246.470 | 23.50 | 5248.180 |
| 30.90 | 5247.235 | 23.80 | 5248.480 |
| 31.50 | 5249.005 | 26.20 | 5248.150 |
| 33.80 | 5249.690 | 26.87 | 5247.480 |
| 41.80 | 5250.525 | 27.54 | 5248.150 |
| | | 31.80 | 5248.210 |
| | | 32.50 | 5248.220 |
| | | 34.00 | 5248.500 |
| | | 43.00 | 5250.070 |
| | | 43.10 | 5250.030 |
| <u>Cross Section 2</u> | | <u>Cross Section 5</u> | |
| 0.00 | 5251.955 | 0.00 | 5252.185 |
| 14.00 | 5249.655 | 12.00 | 5249.215 |
| 22.40 | 5248.570 | 21.40 | 5248.345 |
| 23.90 | 5247.630 | 22.40 | 5246.060 |
| 27.20 | 5247.095 | 24.50 | 5245.410 |
| 32.50 | 5247.590 | 29.90 | 5246.225 |
| 33.00 | 5248.970 | 31.30 | 5248.435 |
| 40.00 | 5249.700 | 41.00 | 5249.155 |
| 42.30 | 5250.205 | 43.60 | 5249.950 |
| <u>Cross Section 3</u> | | <u>Cross Section 6</u> | |
| 0.00 | 5251.935 | 0.00 | 5252.480 |
| 13.60 | 5249.290 | 12.30 | 5249.045 |
| 17.80 | 5248.355 | 22.30 | 5248.350 |
| 20.40 | 5248.215 | 24.00 | 5245.625 |
| 22.00 | 5248.115 | 26.00 | 5245.625 |
| 24.70 | 5247.590 | 29.10 | 5246.085 |
| 26.60 | 5246.790 | 29.10 | 5246.085 |
| 30.50 | 5246.555 | 39.10 | 5248.935 |
| 32.40 | 5247.235 | 43.70 | 5250.055 |
| 33.30 | 5248.780 | | |
| 42.40 | 5249.695 | | |

Appendix A-1.2.3

Table A-1.2.3-3 Havana Interceptor (SW11002) Cross Section Survey Data

| Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|
| 8.00 | 5261.540 |
| 25.00 | 5253.075 |
| 29.50 | 5252.215 |
| 31.00 | 5252.090 |
| 32.00 | 5252.220 |
| 36.50 | 5252.975 |
| 55.00 | 5261.645 |

Appendix A-1.2.3

Table A-1.2.3-4 South Uvalda (SW12005) Cross Section Survey Data

| Horizontal Distance (ft) | Elevation (ft-msl) | Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|--------------------------------|-----------------------|
| <u>Cross Section 1</u> | | <u>Cross Section 3</u> | |
| 2.50 | 5278.170 | 10.42 | 5277.000 |
| 5.00 | 5276.790 | 13.33 | 5276.020 |
| 14.80 | 5274.610 | 18.83 | 5273.810 |
| 25.60 | 5273.740 | 23.03 | 5273.170 |
| 28.90 | 5271.680 | 25.63 | 5272.005 |
| 30.40 | 5271.380 | 26.33 | 5271.515 |
| 33.90 | 5271.885 | 28.73 | 5271.425 |
| 35.60 | 5271.730 | 31.13 | 5271.285 |
| 36.90 | 5271.730 | 33.33 | 5271.635 |
| 39.60 | 5273.470 | 34.93 | 5273.105 |
| 44.00 | 5273.770 | 43.03 | 5271.845 |
| 50.00 | 5277.520 | 47.53 | 5274.990 |
| | | 51.23 | 5277.130 |
| <u>Cross Section 2</u> | | <u>Cross Section 4</u> | |
| 7.42 | 5277.890 | 6.02 | 5277.615 |
| 11.92 | 5275.955 | 11.22 | 5274.810 |
| 15.92 | 5273.515 | 18.82 | 5273.210 |
| 22.02 | 5273.635 | 21.42 | 5273.135 |
| 27.12 | 5272.370 | 25.92 | 5272.400 |
| 29.62 | 5271.615 | 27.32 | 5272.400 |
| 32.42 | 5271.440 | 28.12 | 5272.040 |
| 35.02 | 5271.580 | 28.72 | 5271.600 |
| 35.92 | 5273.120 | 29.32 | 5271.240 |
| 39.22 | 5273.870 | 29.82 | 5271.535 |
| 44.52 | 5273.220 | 29.92 | 5271.695 |
| 50.92 | 5276.760 | 30.62 | 5272.130 |
| | | 31.32 | 5272.405 |
| | | 32.22 | 5272.435 |
| | | 35.92 | 5272.885 |
| | | 41.82 | 5272.880 |
| | | 45.62 | 5275.040 |
| | | 49.22 | 5277.030 |

Table A-1.2.3-4

South Uvalda (SW12005) Cross Section Survey Data (continued)

| Horizontal Distance (ft) | Elevation (ft-msl) | Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|--------------------------------|-----------------------|
| <u>Cross Section 5</u> | | <u>Cross Section 6</u> | |
| 4.17 | 5276.700 | 8.42 | 5278.230 |
| 9.97 | 5276.040 | 16.22 | 5274.190 |
| 14.37 | 5274.915 | 21.42 | 5273.205 |
| 20.37 | 5273.265 | 25.62 | 5272.640 |
| 23.57 | 5273.070 | 27.02 | 5271.770 |
| 25.47 | 5272.560 | 27.82 | 5270.840 |
| 26.17 | 5270.740 | 30.02 | 5270.525 |
| 29.07 | 5270.385 | 32.32 | 5270.690 |
| 33.17 | 5272.930 | 32.92 | 5271.770 |
| 34.87 | 5271.835 | 35.42 | 5272.660 |
| 38.77 | 5273.245 | 43.22 | 5272.950 |
| 45.17 | 5273.100 | 51.52 | 5273.995 |
| 47.97 | 5274.305 | 55.42 | 5276.615 |
| 51.17 | 5276.580 | | |

Appendix A-1.2.3

Table A-1.2.3-5 North First Creek (SW24002) Cross Section Survey Data

| Horizontal Distance (ft) | Elevation (ft-msl) | Horizontal Distance (ft) | Elevation (ft-msl) |
|--------------------------------|-----------------------|--------------------------------|-----------------------|
| <u>Cross Section 1</u> | | <u>Cross Section 4</u> | |
| 5.30 | 5146.500 | 0.00 | 5145.860 |
| 8.30 | 5144.820 | 4.50 | 5145.885 |
| 11.30 | 5143.010 | 7.50 | 5143.130 |
| 13.80 | 5142.820 | 12.50 | 5142.680 |
| 15.30 | 5142.470 | 14.00 | 5141.750 |
| 16.30 | 5142.610 | 15.50 | 5142.710 |
| 19.10 | 5141.780 | 20.50 | 5143.200 |
| 21.30 | 5143.040 | 23.50 | 5146.010 |
| 23.30 | 5144.720 | 28.50 | 5146.040 |
| 25.30 | 5146.160 | | |
| <u>Cross Section 2</u> | | <u>Cross Section 5</u> | |
| 4.80 | 5146.210 | 1.50 | 5145.870 |
| 6.30 | 5146.610 | 6.00 | 5142.640 |
| 9.30 | 5142.590 | 9.00 | 5141.590 |
| 13.30 | 5141.750 | 11.50 | 5140.900 |
| 17.30 | 5141.620 | 15.00 | 5141.340 |
| 21.30 | 5141.860 | 19.00 | 5143.660 |
| 22.70 | 5143.770 | 22.00 | 5146.020 |
| 23.80 | 5145.710 | | |
| <u>Cross Section 3</u> | | | |
| 4.10 | 5146.110 | | |
| 8.60 | 5141.950 | | |
| 12.30 | 5141.480 | | |
| 12.30 | 5141.150 | | |
| 16.90 | 5141.950 | | |
| 19.40 | 5142.935 | | |
| 22.80 | 5144.970 | | |
| 23.30 | 5146.230 | | |

APPENDIX A-1.2.4

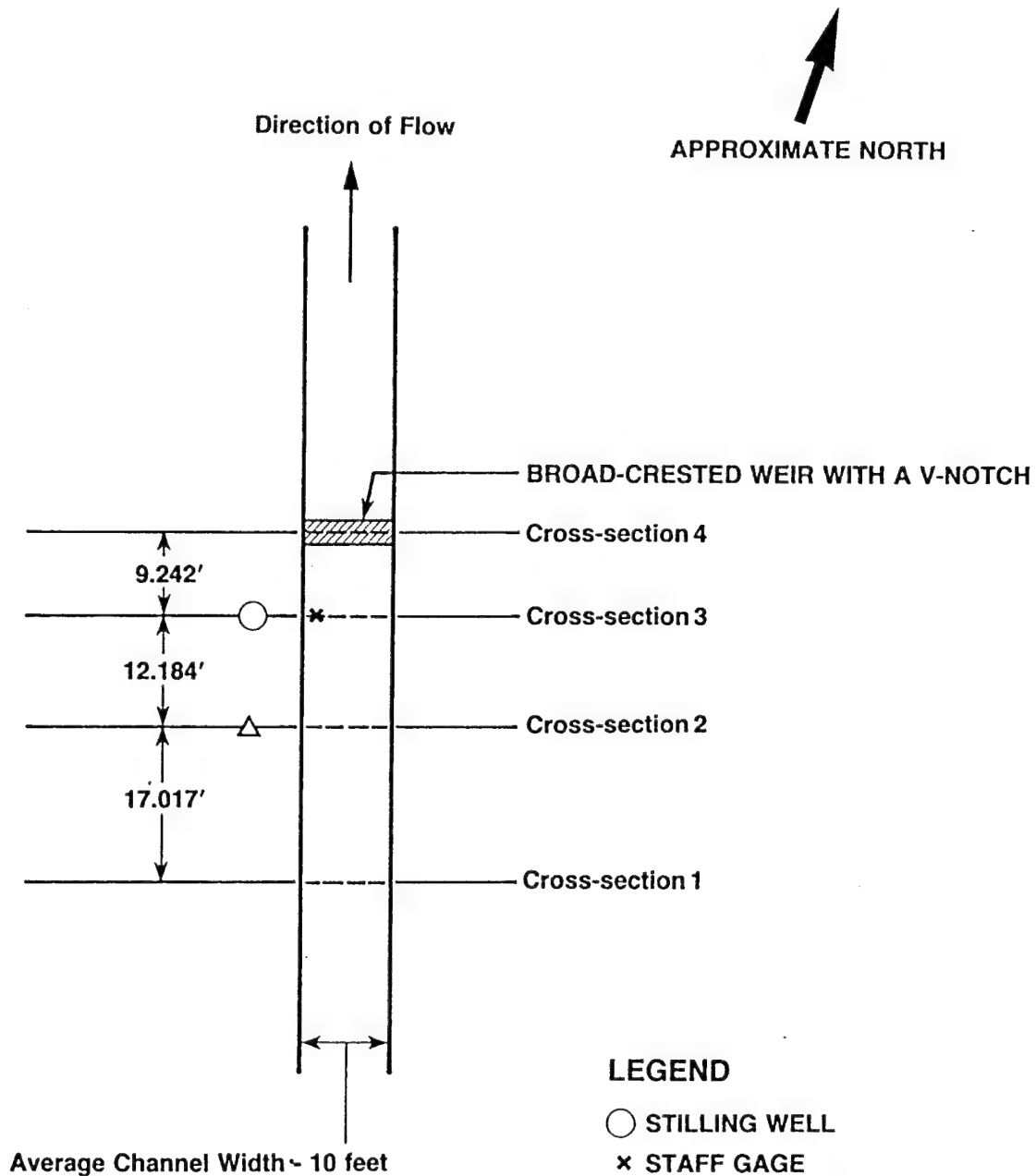
Channel Reach Survey Procedure

Vertical control was established by referencing to an existing temporary bench mark (TBM) located at or near each structure. Each TBM is permanently secured such that additional or future surveys can be referenced to the same elevation. The need to do additional surveying may arise as a result of flooding which could cause changes in channel geometry, from aggradation or degradation of the stream channel bottom as a result of increased or decrease sediment transport, and from modifications or changes in the control structure, staff location or staff elevation.

Each stream cross section was referenced either to the TBM or an established pin at the nearest upstream or downstream cross section to maintain vertical control. All rod readings were recorded to the nearest 0.005 feet. For each surveying instrument location, a backsight and foresight to established pins was recorded. All level loops were closed on the original TBM at each location, with an allowable vertical closure error not-to-exceed 0.01 feet. An end-to-end test or "peg test" was conducted on the surveying instrument each day prior to use to ensure instrument accuracy.

Horizontal control was established by driving 5/8-inch rebar stakes (pins) at the endpoints of each cross section. The pins serve as reference locations for each cross section and may be used for future surveys, if required. Each pin was tagged with aluminum tags etched with the station identification, pin identification and date. Pins were positioned on both sides of the stream channel perpendicular to flow lines in the stream. The location of the pins is high enough such that a wide range of high flows will be contained within the surveyed cross sections. Each pin was hammered into the ground approximately 1.5 feet. The remaining 0.5 feet was painted orange and tagged with orange surveyor's flagging for ease of locating in the future. For step-backwater modeling purposes, baseline and azimuth measurements were not required. Since all cross sections were staked and identified, horizontal control with reference to magnetic north can easily be obtained by additional surveys.

All cross sections were surveyed from left to right looking in a downstream direction. Horizontal stations were determined to the nearest 0.1 feet using a cloth tape stretched between the pins. Horizontal stationing was determined for all slope breaks along each cross section, for the left and right overbank reaches, left and right channel banks, left and right edge of water and for the thalweg of each cross section. Additionally, the water surface elevation at each cross section were determined to compute the energy grade of a particular reach.



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

20 feet
SCALE

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U.S. Army Program Manager for
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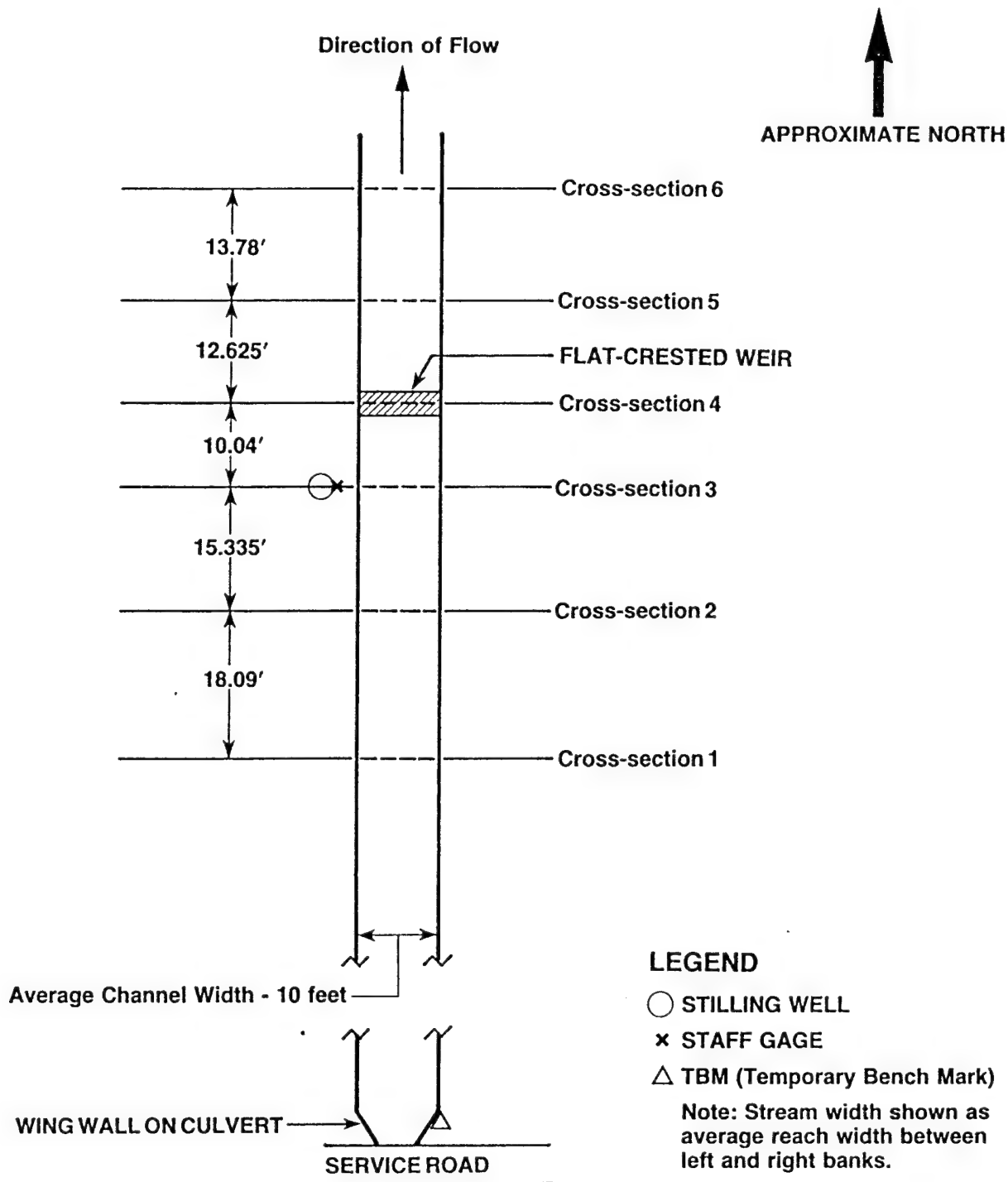
Prepared by :

R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-1

North Uvalda (SW01001)
Cross-Section Locations

CMP SW FY89

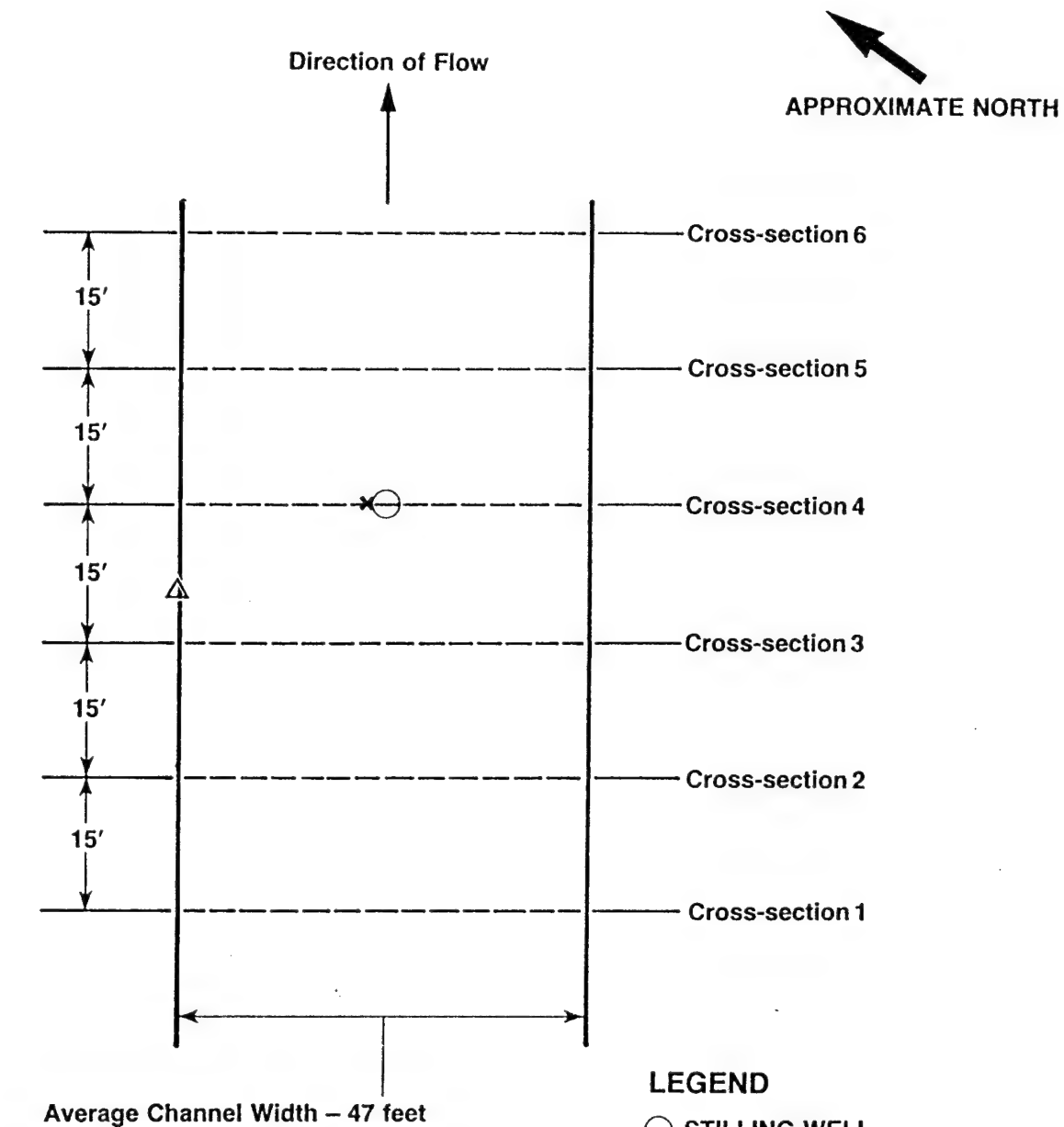


20 feet
SCALE

Prepared for :
U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

Prepared by :
R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-2
Peoria Interceptor
(SW11001)
Cross-Section Locations
CMP SW FY89



20 feet
SCALE

LEGEND

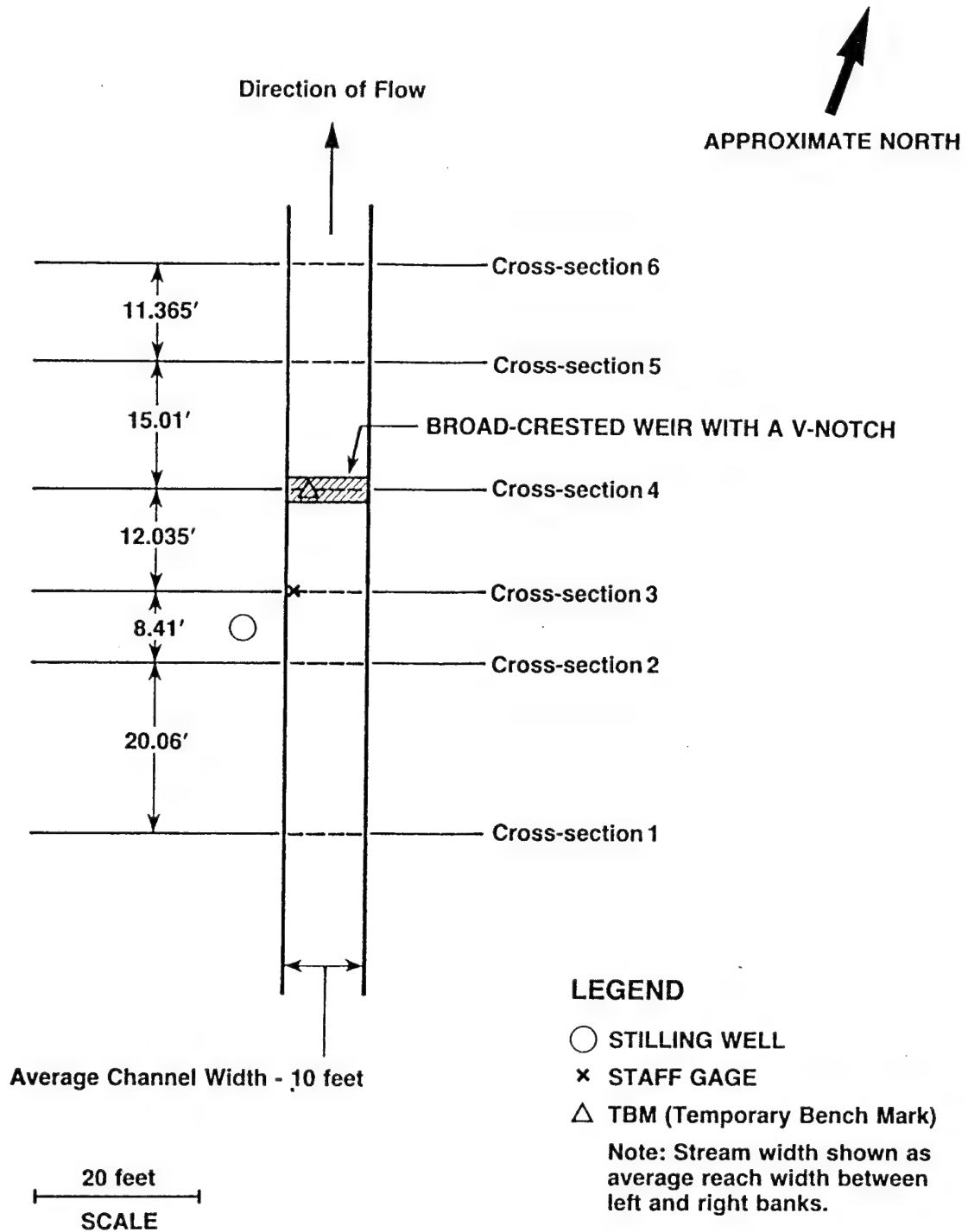
- STILLING WELL
- x STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

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Riverside Technology, Inc.

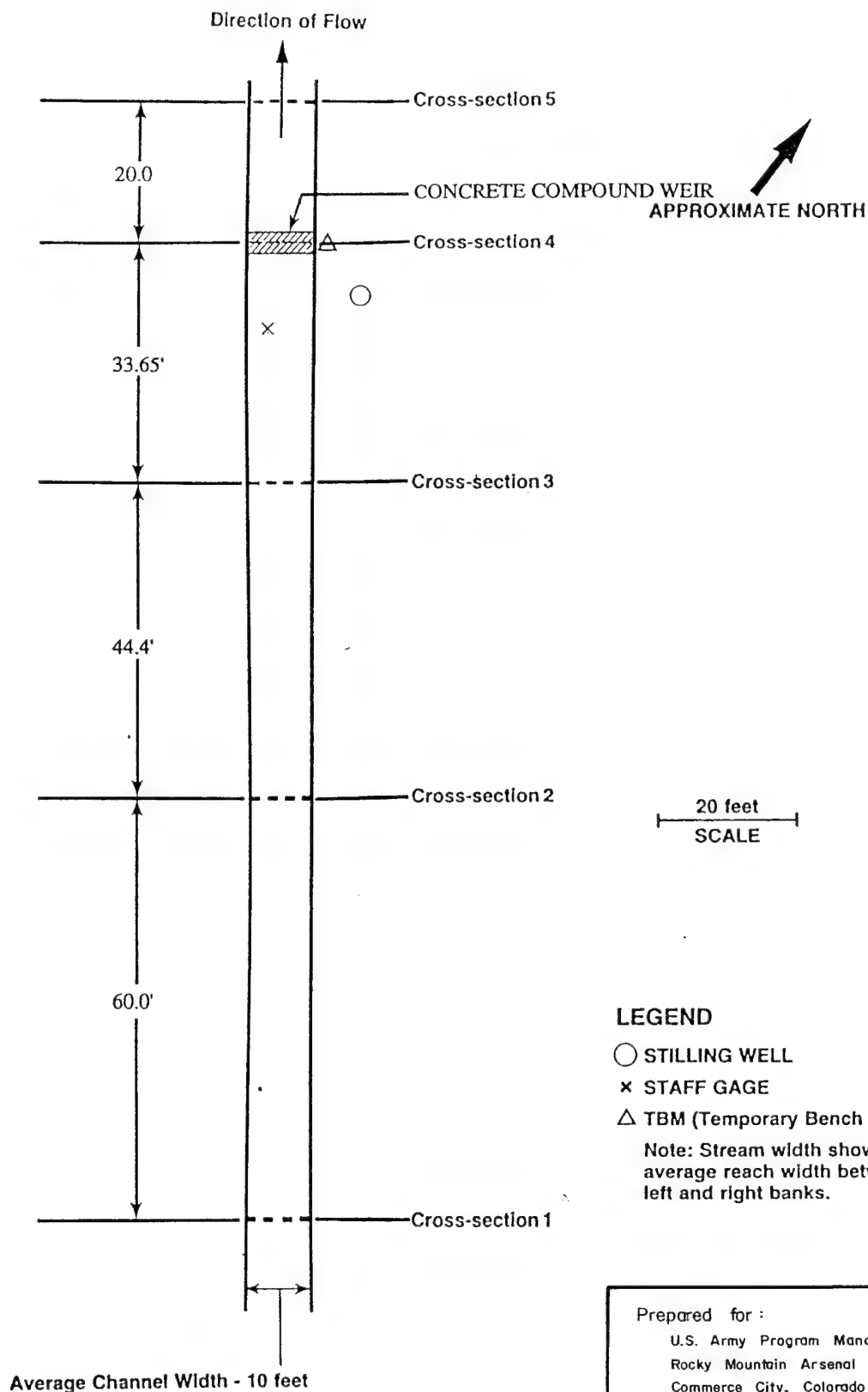
Figure A-1.2.2-3
Havana Interceptor
(SW11002)
Cross-Section Locations
CMP SW FY89



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Figure A-1.2.2-4
 South Uvalda (SW12005)
 Cross-Section Locations
 CMP SW FY89



LEGEND

- STILLING WELL
- × STAFF GAGE
- △ TBM (Temporary Bench Mark)

Note: Stream width shown as average reach width between left and right banks.

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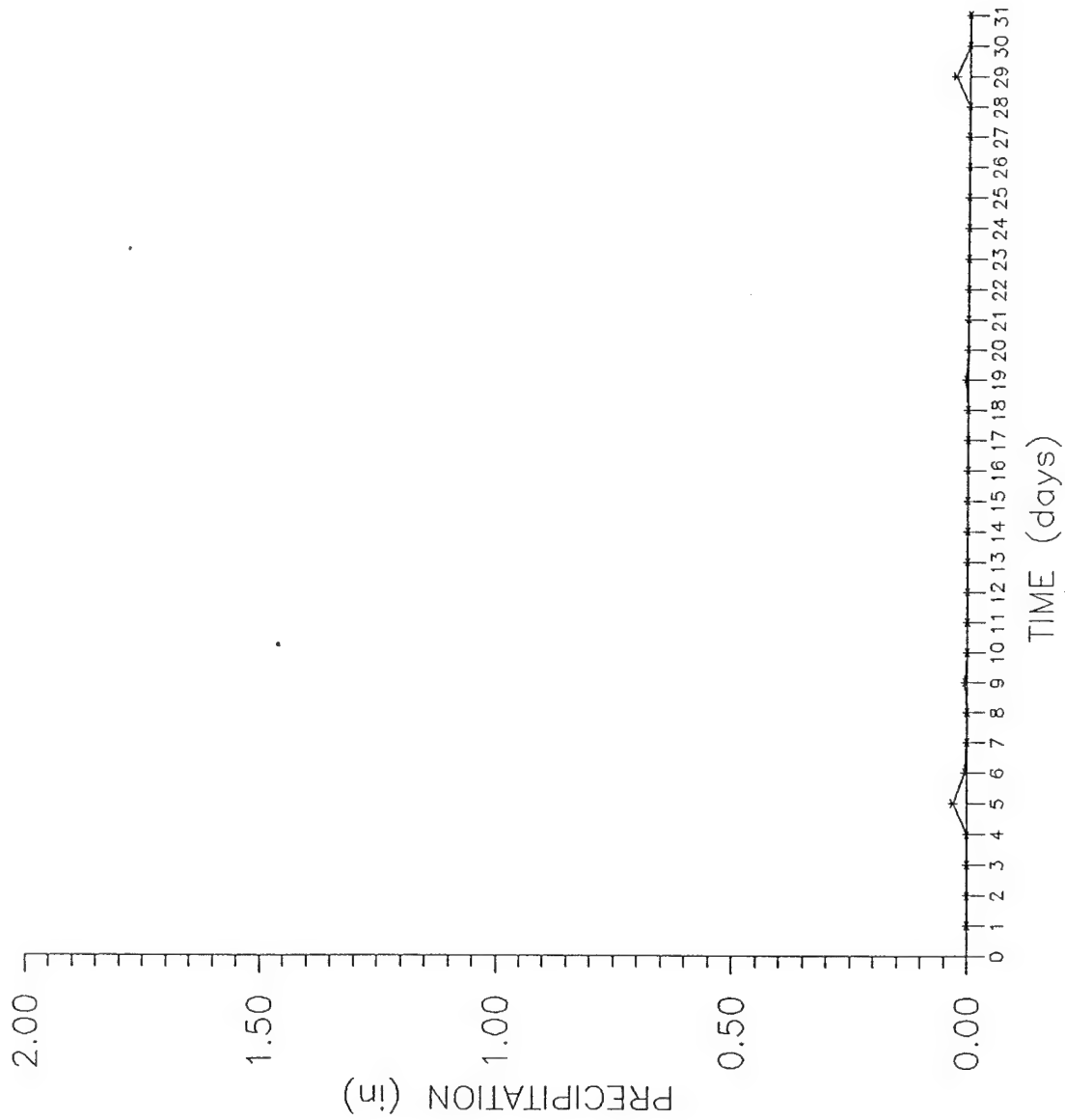
R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-1.2.2-5

North First Creek
(SW24002)

Cross-Section Locations

CMP SW FY89

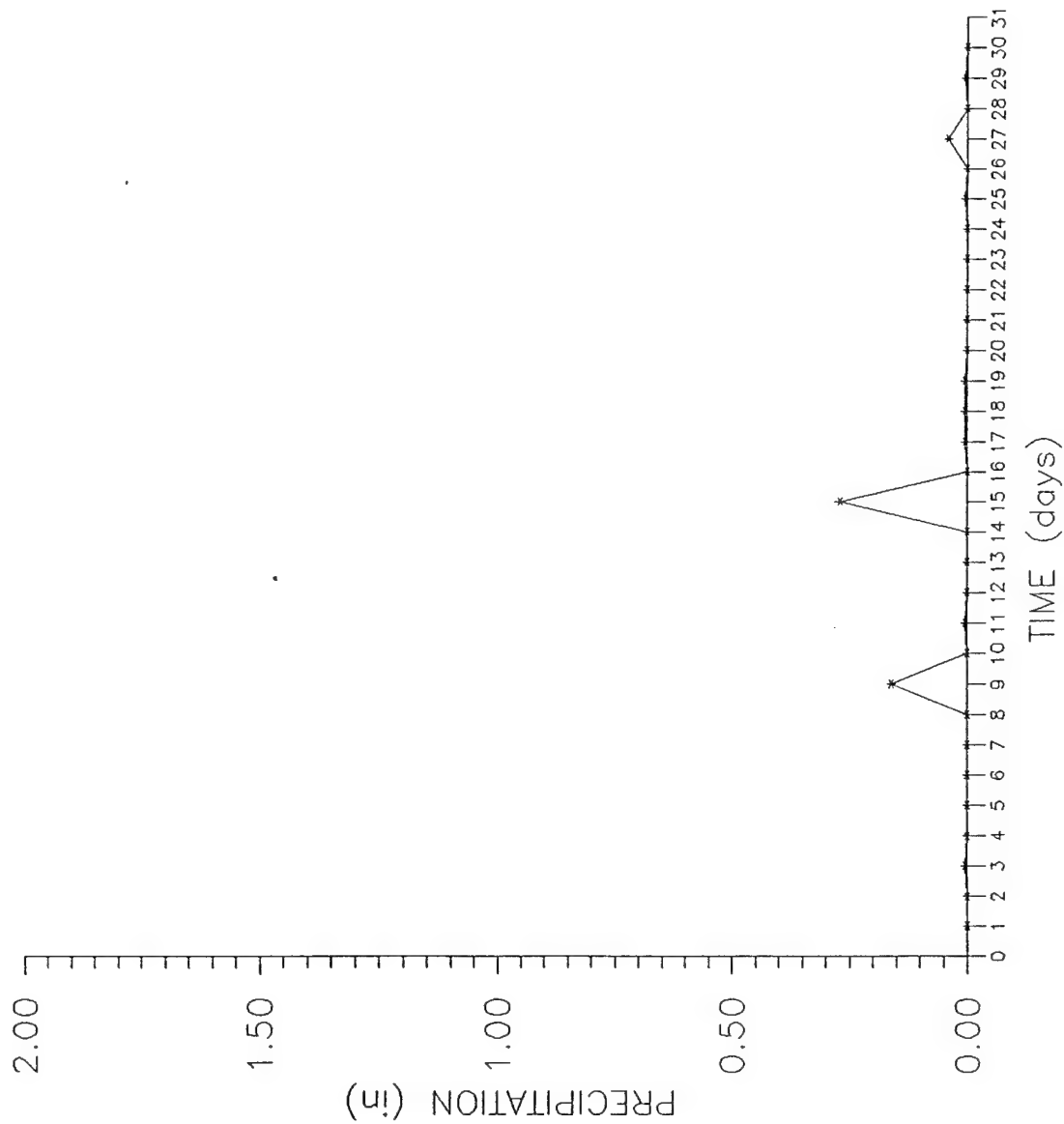


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Figure A-11.1-1

October 1988 Precipitation

CMP SW FY89



----- PRECIPITATION

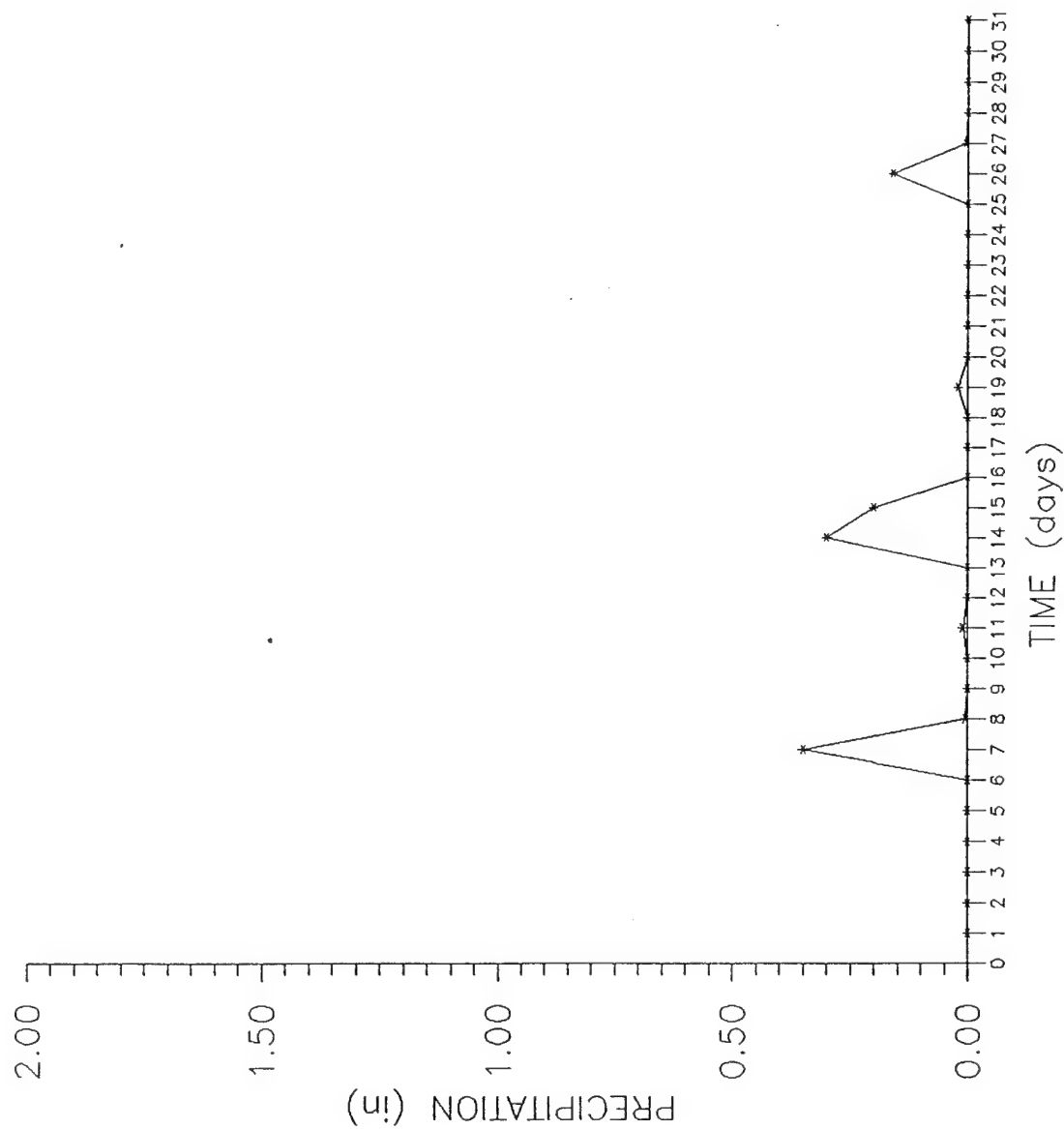
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Figure A-11.1-2

November 1988 Precipitation

CMP SW FY89

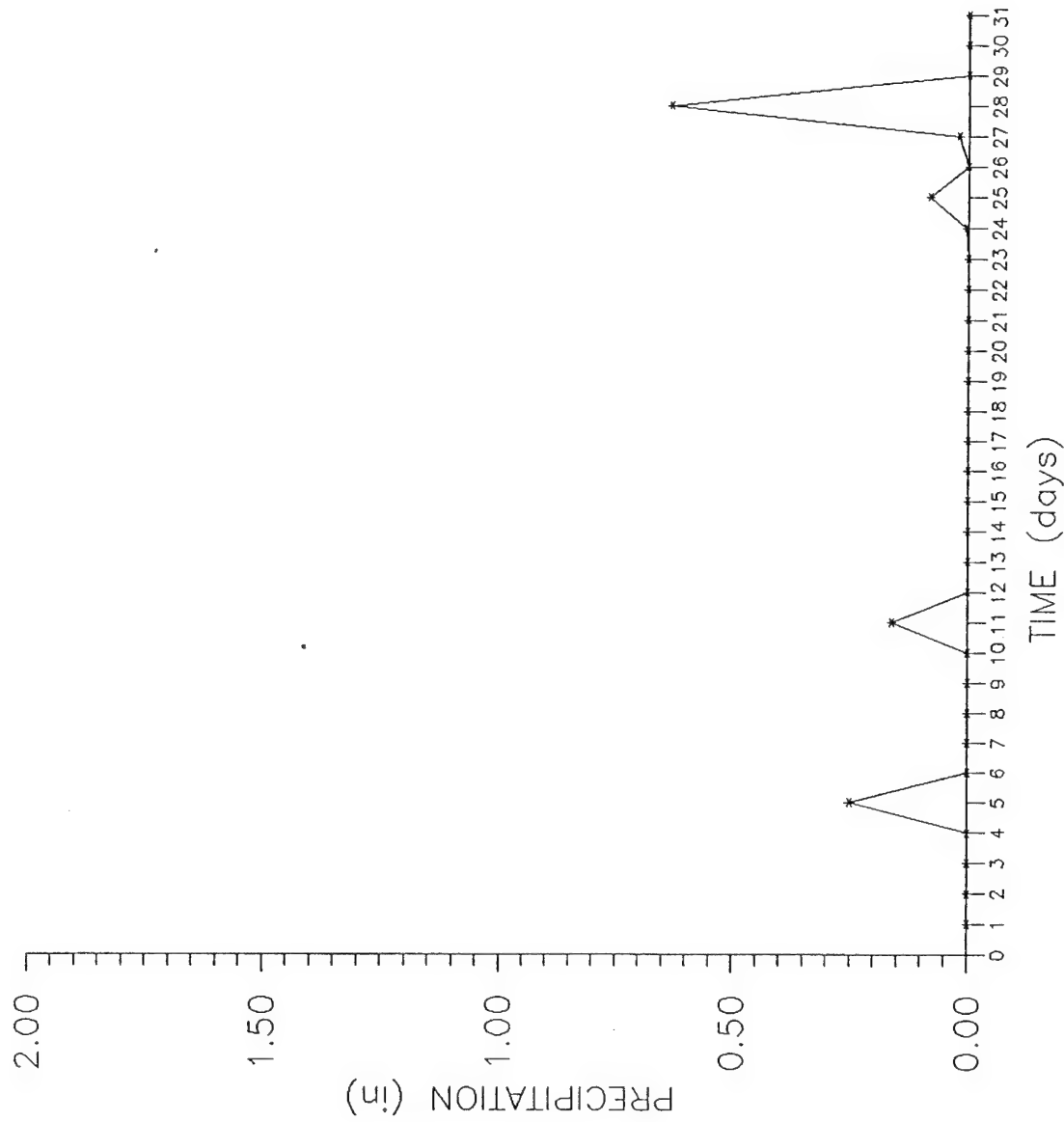


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Figure A-11.1-3

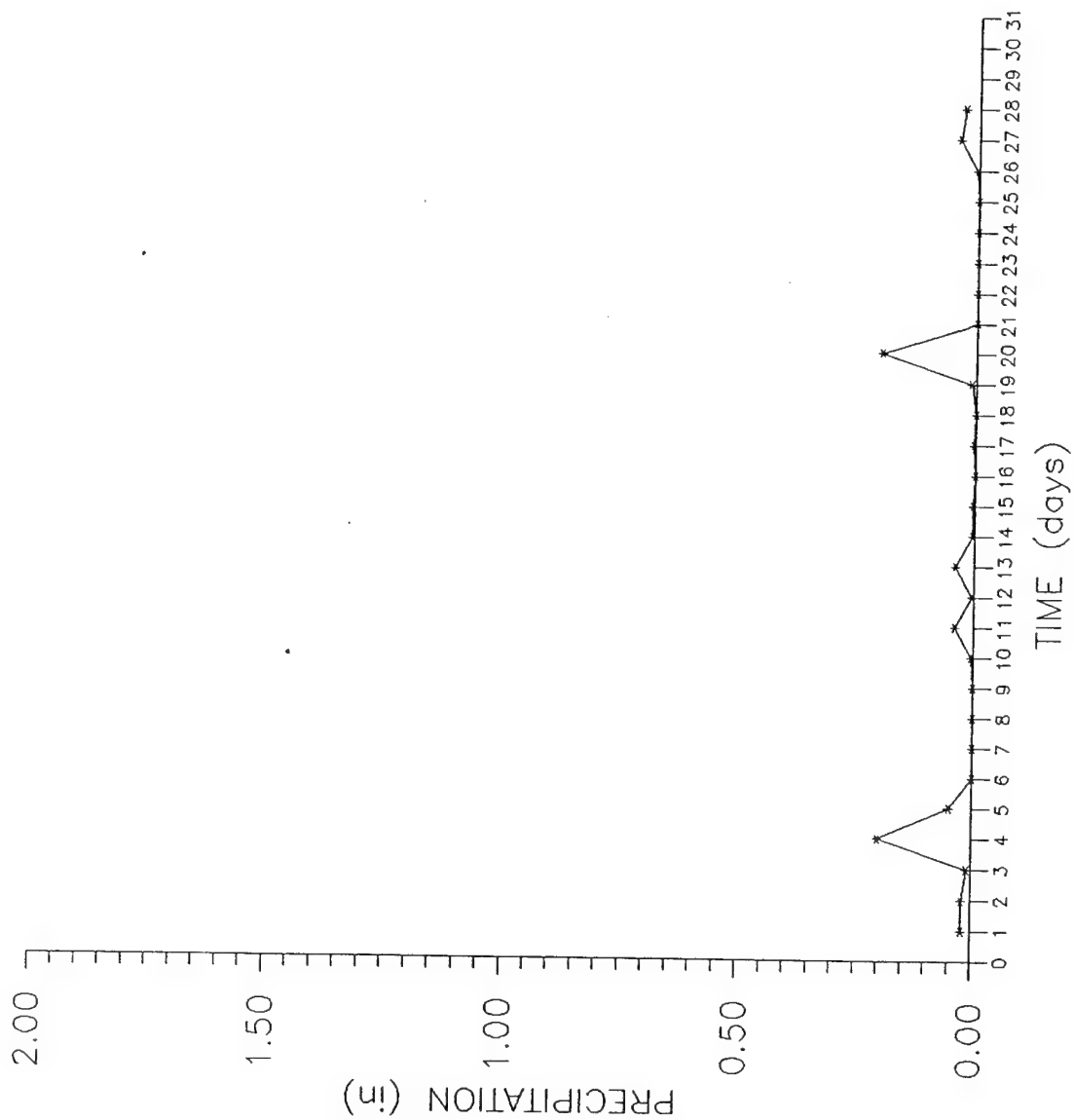
December 1988 Precipitation

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Figure A-11.1-4
 January 1989 Precipitation

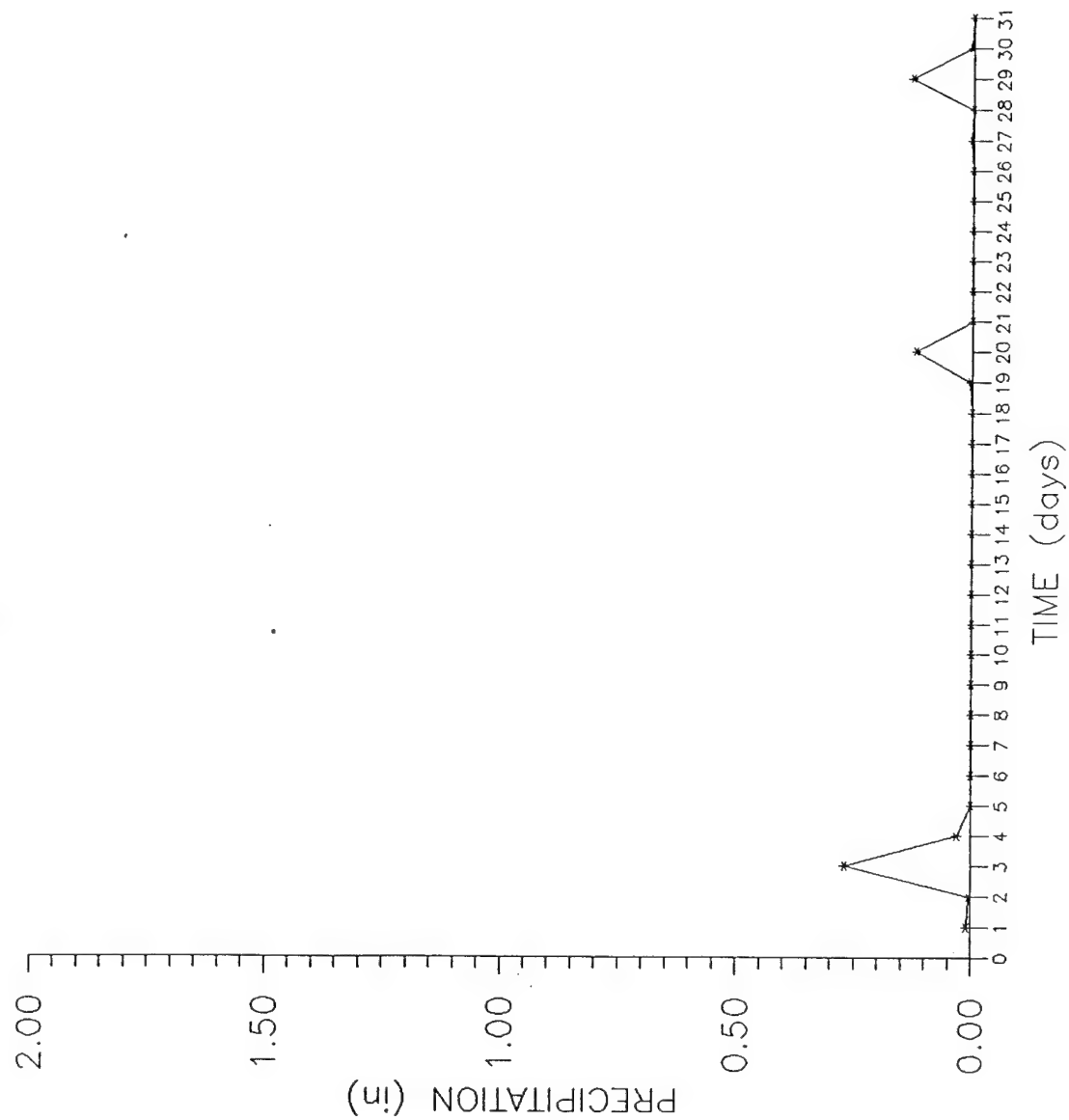


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Figure A-11.1-5

February 1989 Precipitation

CMP SW FY89



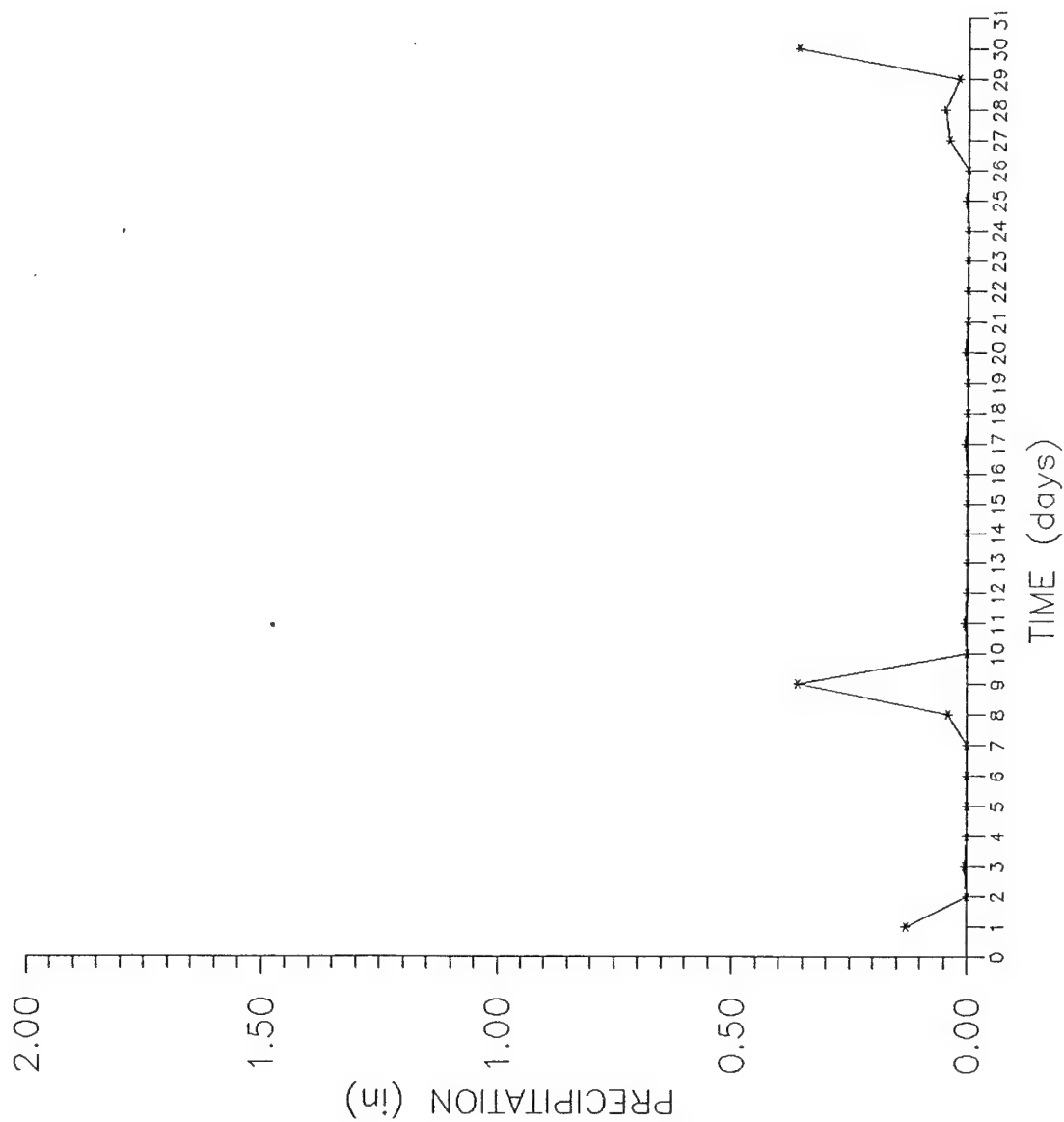
----- PRECIPITATION

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Figure A-11.1-6

March 1989 Precipitation

CMP SW FY89



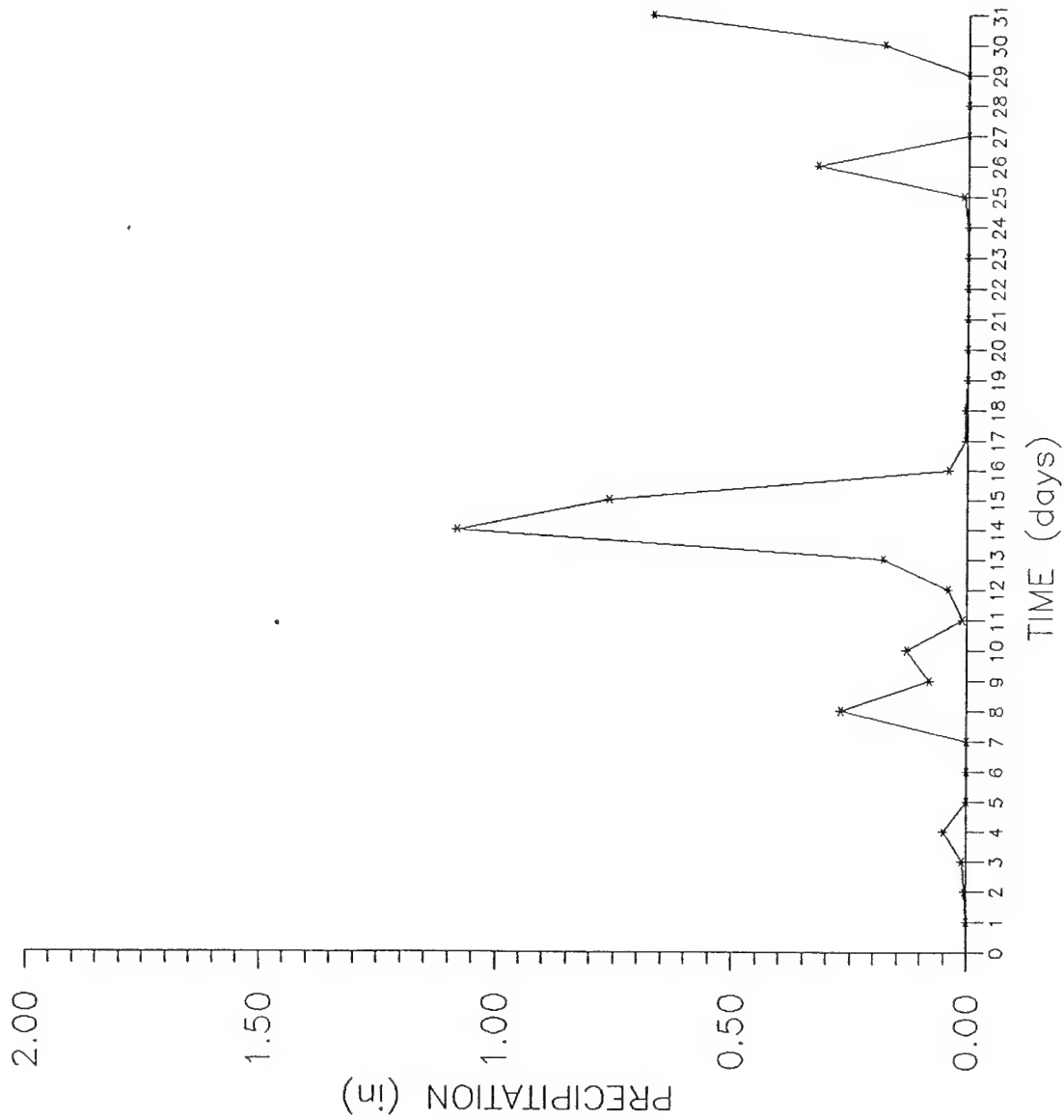
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Figure A-11.1-7

April 1989 Precipitation

CMP SW FY89

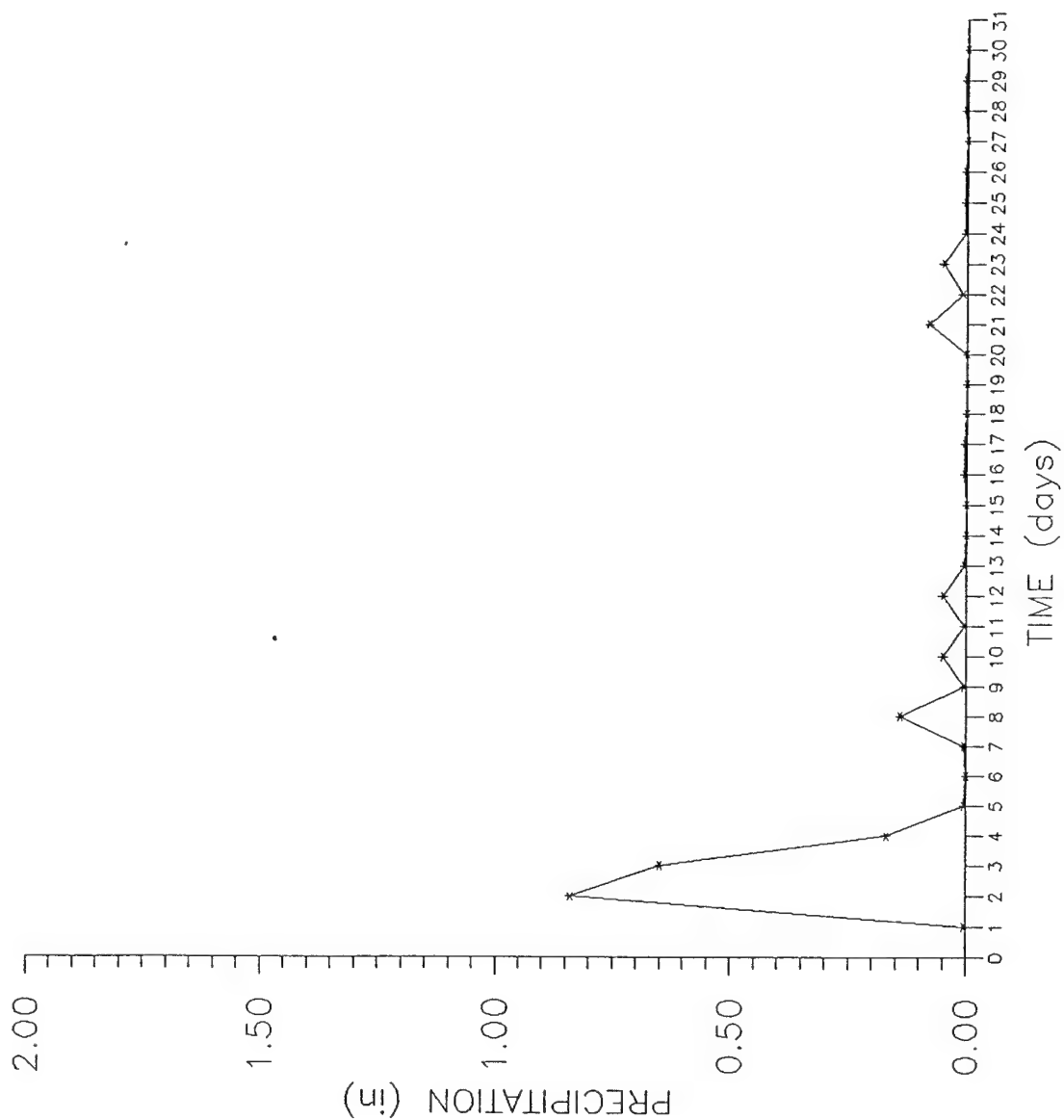


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Figure A-11.1-8

May 1989 Precipitation

CMP SW FY89



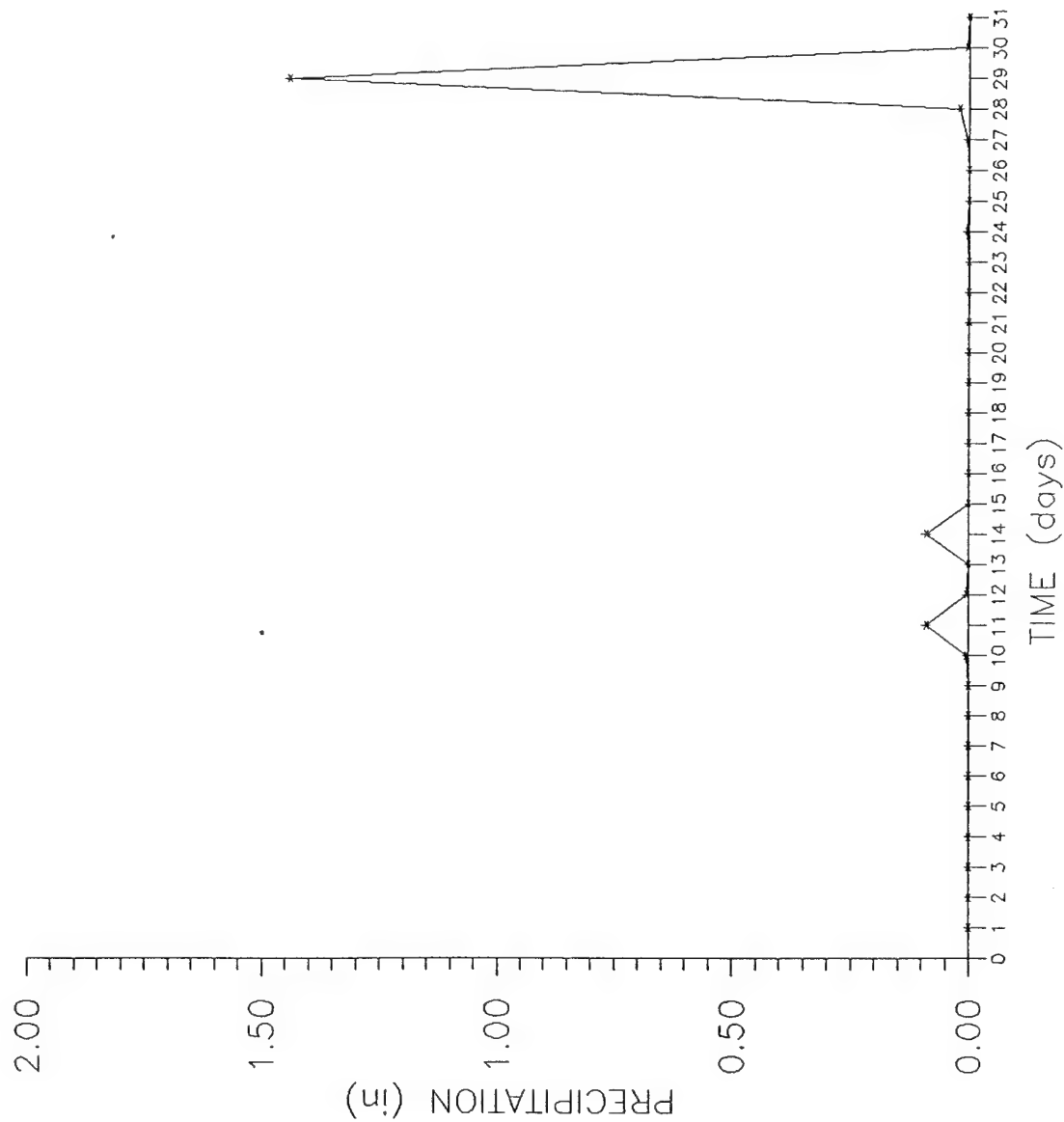
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Figure A-11.1 -9

June 1989 Precipitation

CMP SW FY89

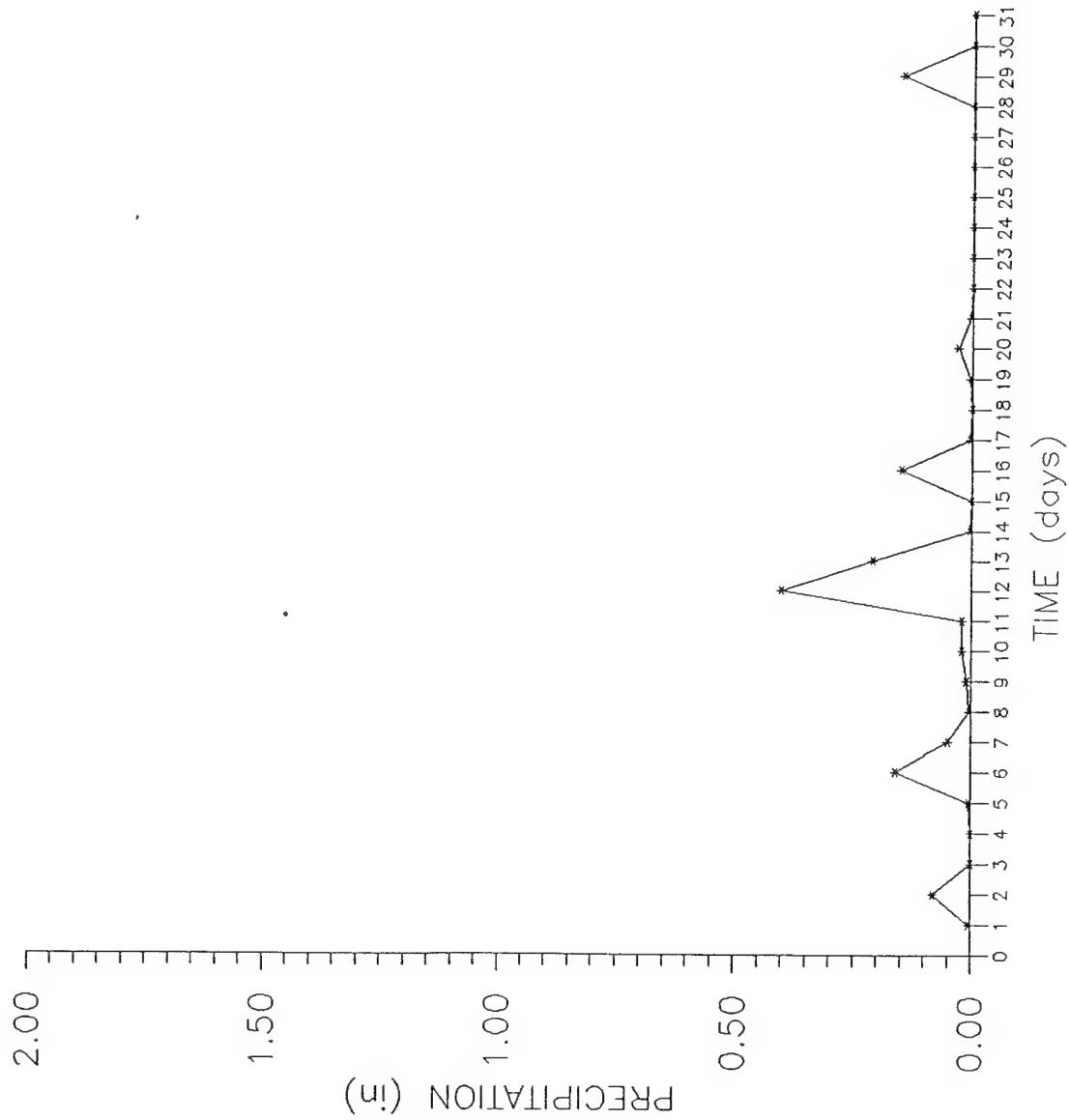


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Figure A-11.1-10

July 1989 Precipitation

CMP SW FY89



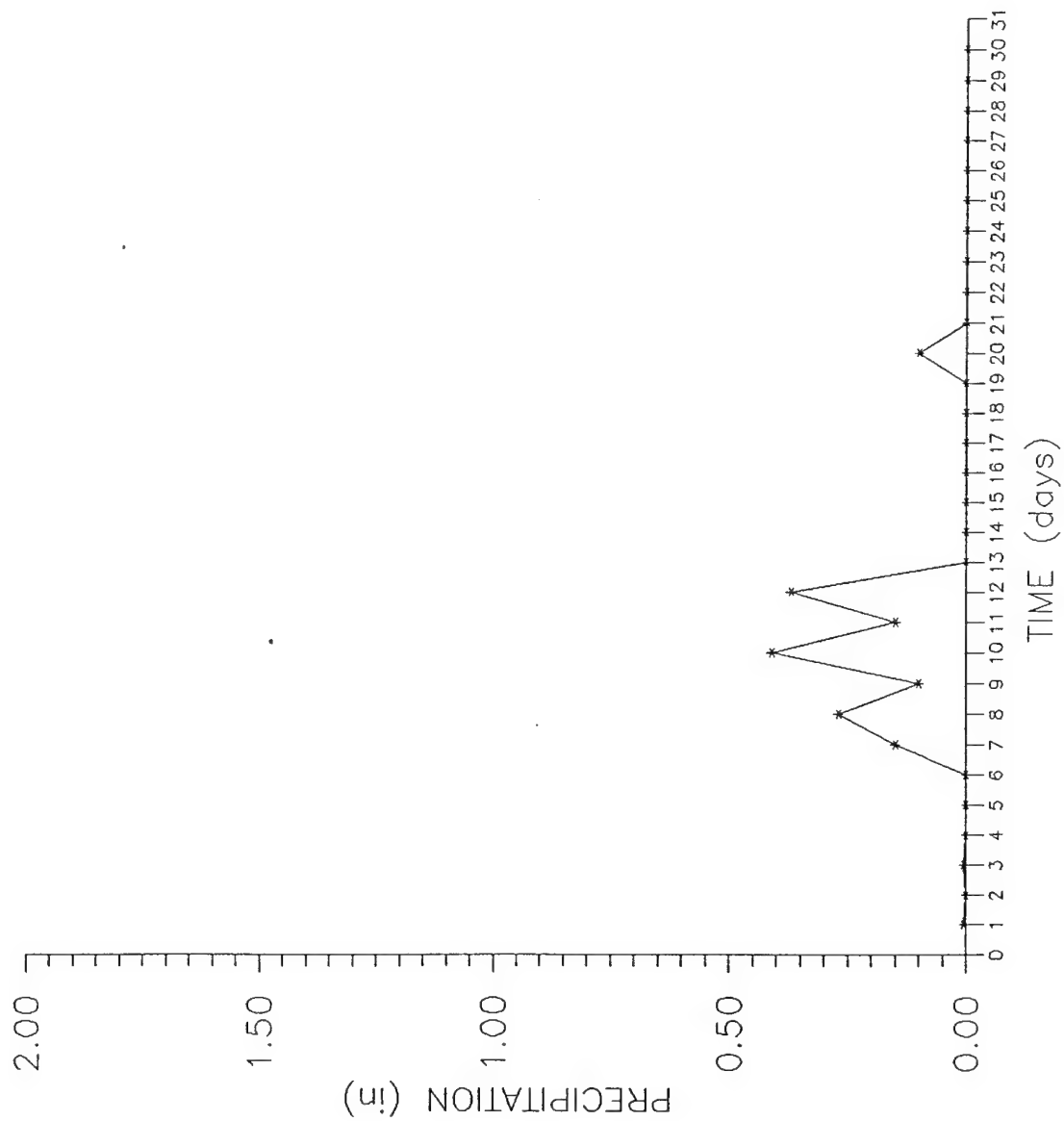
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Figure A-11.1-11

August 1989 Precipitation

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Figure A-11.1-12

September 1989 Precipitation

CMP SW FY89

APPENDIX A-2

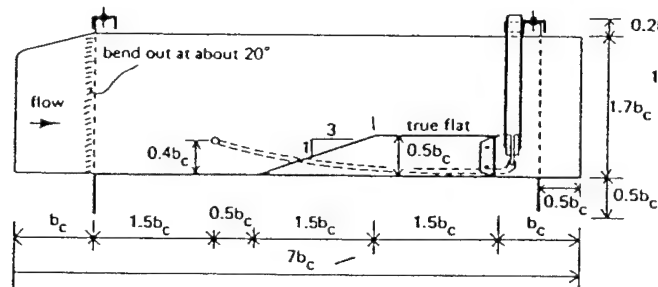
Instantaneous Discharge Measurements

APPENDIX A-2.1

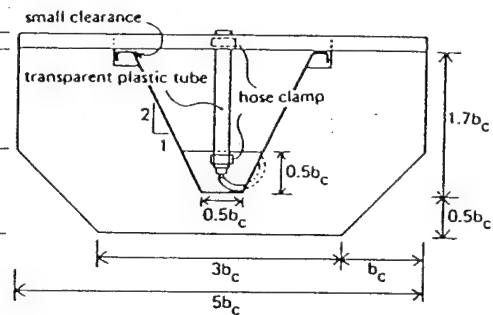
Flume Specifications

VIEWS

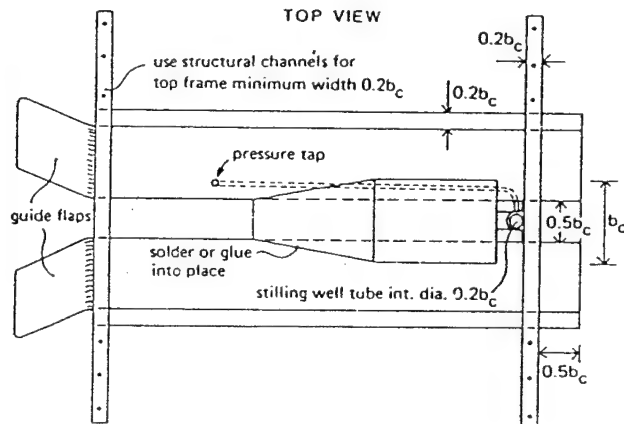
LONGITUDINAL SECTION



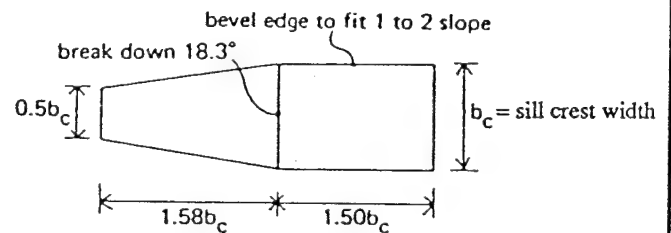
END VIEW



TOP VIEW



TOP VIEW SILL DETAIL



| 100 mm Flume | 200 mm Flume |
|---|---|
| $b_c = 100 \text{ mm}$ $= 3.94 \text{ in}$ | $b_c = 200 \text{ mm}$ $= 7.87 \text{ in}$ |

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Prepared by :

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Riverside Technology, Inc.

Figure A-2.1-1

100mm and 200mm
Long-Throated Flume
Specifications

CMP SW FY89

Appendix A-2.1

Table 2.1-1 Stage Discharge Relationship for 100 mm Portable Long-throated

| h (ft) | Q (cfs) |
|-----------|------------|
| 0.04 | 0.0078 |
| 0.05 | 0.0113 |
| 0.06 | 0.0153 |
| 0.07 | 0.0198 |
| 0.08 | 0.0247 |
| 0.09 | 0.0301 |
| 0.10 | 0.0360 |
| 0.11 | 0.0424 |
| 0.12 | 0.0492 |
| 0.13 | 0.0565 |
| 0.14 | 0.0643 |
| 0.15 | 0.0726 |
| 0.16 | 0.0814 |
| 0.17 | 0.0907 |
| 0.18 | 0.1004 |
| 0.19 | 0.1107 |
| 0.20 | 0.1214 |
| 0.21 | 0.1327 |
| 0.22 | 0.1445 |
| 0.23 | 0.1568 |
| 0.24 | 0.1697 |
| 0.25 | 0.1831 |
| 0.26 | 0.1970 |
| 0.27 | 0.2114 |
| 0.28 | 0.2264 |
| 0.29 | 0.2420 |
| 0.30 | 0.2582 |
| 0.31 | 0.2748 |
| 0.32 | 0.2921 |
| 0.33 | 0.3099 |

- (1) Design and ratings taken from "Flow Measuring Flumes for Open Channel Systems"; Marinus G. Bos, John A. Repogle, Albert J. Clemmens, 1984 by John Wiley & Sons, Inc.
- (2) "h" is upstream sill - referenced head.

Appendix A-2.1

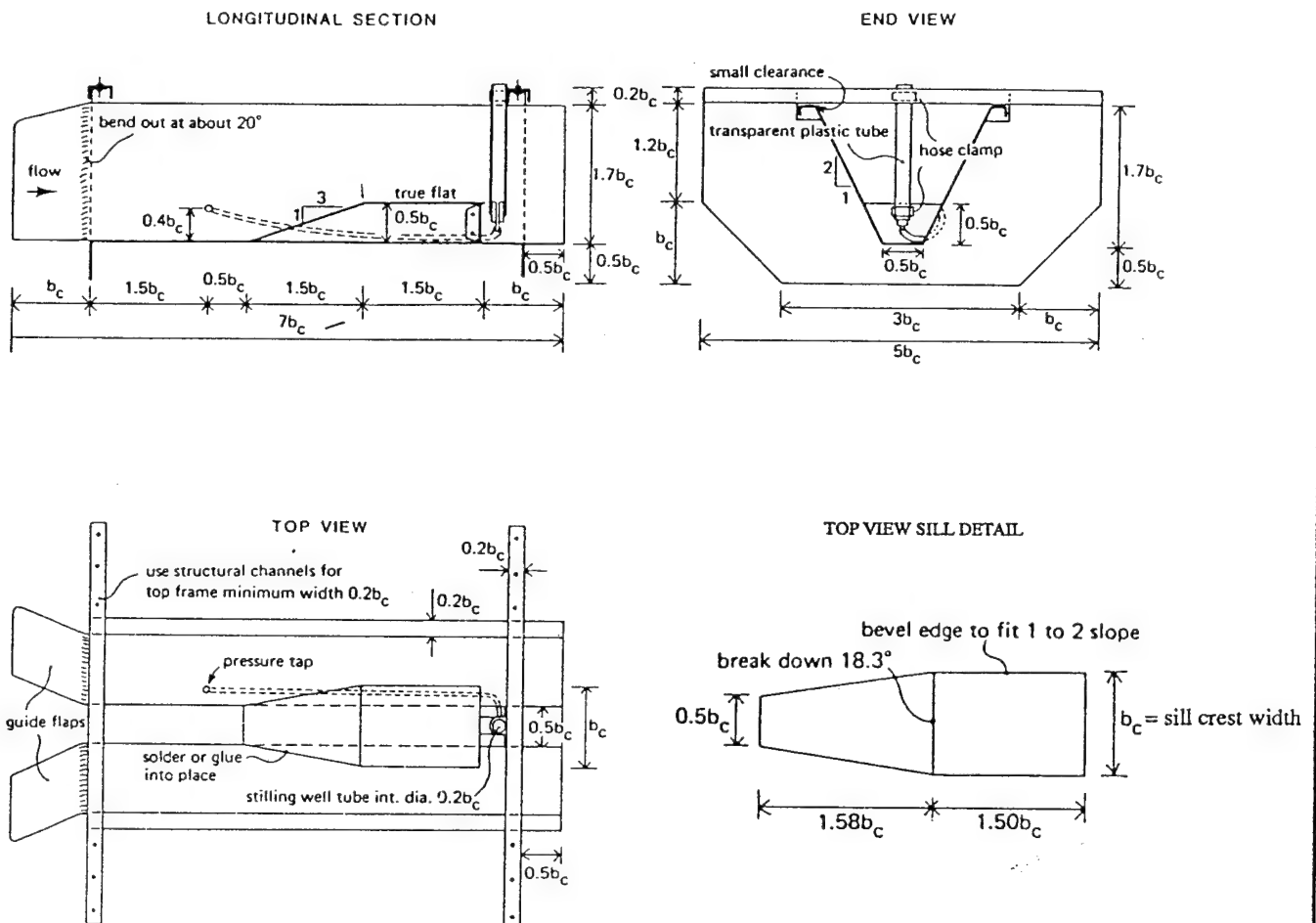
Table 2.1-2 Depth Discharge Relationship for Long-throated Portable Flume with 0.66 ft (200 mm) wide sill (1)

| h (ft) | Q (cfs) | h (ft) | Q (cfs) |
|-----------|------------|-----------|------------|
| 0.07 | 0.0367 | 0.37 | 0.6008 |
| 0.08 | 0.0456 | 0.38 | 0.6303 |
| 0.09 | 0.0552 | 0.39 | 0.6606 |
| 0.10 | 0.0655 | 0.40 | 0.6915 |
| 0.11 | 0.0765 | 0.41 | 0.7232 |
| 0.12 | 0.0883 | 0.42 | 0.7557 |
| 0.13 | 0.1007 | 0.43 | 0.7887 |
| 0.14 | 0.1137 | 0.44 | 0.8226 |
| 0.15 | 0.1275 | 0.45 | 0.8572 |
| 0.16 | 0.1419 | 0.46 | 0.8927 |
| 0.17 | 0.1570 | 0.47 | 0.9288 |
| 0.18 | 0.1727 | 0.48 | 0.9656 |
| 0.19 | 0.1891 | 0.49 | 0.9656 |
| 0.20 | 0.2062 | 0.50 | 1.042 |
| 0.21 | 0.2240 | 0.51 | 1.081 |
| 0.22 | 0.2424 | 0.52 | 1.121 |
| 0.23 | 0.2615 | 0.53 | 1.161 |
| 0.24 | 0.2813 | 0.54 | 1.203 |
| 0.25 | 0.3017 | 0.55 | 1.245 |
| 0.26 | 0.3229 | 0.56 | 1.288 |
| 0.27 | 0.3447 | 0.57 | 1.332 |
| 0.28 | 0.3672 | 0.58 | 1.376 |
| 0.29 | 0.3903 | 0.59 | 1.422 |
| 0.30 | 0.4142 | 0.60 | 1.468 |
| 0.31 | 0.4387 | 0.61 | 1.515 |
| 0.32 | 0.4640 | 0.62 | 1.563 |
| 0.33 | 0.4900 | 0.63 | 1.611 |
| 0.34 | 0.5167 | 0.64 | 1.661 |
| 0.35 | 0.5440 | 0.65 | 1.711 |
| 0.36 | 0.5721 | 0.66 | 1.762 |

(1) Design and ratings taken from "Flow Measuring Flumes for Open Channel Systems"; Marinus G. Bos, John A. Repogle, Albert J. Clemmens, 1984 by John Wiley & Sons, Inc.

(2) "h" is upstream sill - referenced head.

VIEWS



| 100 mm Flume | 200 mm Flume |
|---|---|
| $b_c = 100 \text{ mm}$ $= 3.94 \text{ in}$ | $b_c = 200 \text{ mm}$ $= 7.87 \text{ in}$ |

Prepared for :
U.S. Army Program Manager for
Rocky Mountain Arsenal
Commerce City, Colorado

Prepared by :
R.L. Stollar & Associates, Inc.
Riverside Technology, Inc.

Figure A-2.1-1
100mm and 200mm
Long-Throated Flume
Specifications
CMP SW FY89

APPENDIX A-2.2

Discharge Measurement Procedures

A-2.2 Pygmy and Type-AA Current Meter Discharge Measurement Procedure

The following details procedure methods used in performing an instantaneous discharge measurement using pygmy or Type-AA current meters.

The calibration check for the Pygmy and Type-AA current meters are as follows:

- the rotor and shaft alignment was checked by spinning the bucket wheel;
- the cups were checked for damage and bending;
- the Type-AA tailpiece condition was checked; and
- a spin test was performed to check the condition of the bearing and record. A normal Type-AA meter spin test should never have been less than 1 1/2 minutes. The normal spin for a Pygmy meter should never have been less than 1/2 minute.

The Marsh-McBirney current meter is a factory calibrated electromagnetic-type meter and cannot be adjusted in the field. However, the battery, the electromagnetic sensor and internal electrical circuitry was checked. In addition the above field inspection procedures, each meters' manufacturer suggested instructions for routine care and maintenance was followed.

The following procedures were implemented to measure and calculate current meter instantaneous discharge rates:

- A measuring tape was stretched across the stream at right angles to the direction of flow to determine the width of the stream and to be used in the measurement of each flow cell.
- The spacing of the subsections (flow cells) was generally made by dividing the total width of the stream into 20 subsections. Sections were usually chosen so that no section contained more than 10 percent of the total flow. Equal widths (subsections) across a cross section were used unless the discharge was well distributed. For RMA where 20 sections were not usually possible a minimum distance of 0.3 feet between subsections was generally used.
- Recording stream stage from the staff gage and the recorder (if present). Identifying the starting point by either LEW or REW (left edge of water or right edge of water, respectively, when facing downstream). Recording the starting time on the

measurement sheet and on the recorder (if present). Recording the staff gage periodically during measurement and time in order to determine the mean gage height for the measurement.

- Recording the distance from the initial measuring point to the edge of water and the depth at the edge of water.
- For stream depths encountered during WY88, measurements were made at 0.6 depth using a top setting wading rod. This rod is masked so as to automatically suspend the current meter at 0.6 depth by "setting" the total depth on the wading rod.
- After the meter was set at the proper depth, it was allowed to stabilize to the stream current. The wading rod was kept in a vertical position and the current meter was held parallel to the direction of flow. The hydrologist stood in a position that least affected the velocity of the water passing the current meter by standing downstream and off to one side of the rod.
- The measuring and recording of flow velocity using the Pygmy or Type-AA meters was performed in accordance with the manufacturer's instructions. The minimum time for measuring velocity in each subsection was 40 seconds. A headphone set was wired into the meters and a click was heard in the headphones that corresponded to each meter revolution. The number of revolutions was recorded for each 40 second time interval. The velocity for each subsection was either calculated or obtained from the meter manufacturer's table for the numbered revolutions per 40 seconds. Marsh-McBirney meter measurements were obtained from the direct digital display on the instrument.
- The remaining stream flow measurement was obtained by moving to each of the verticals and repeating the process. Upon completion of the measurement the time and bank where the section ended and the stream staff gage and recorder water level was recorded on the discharge measurement sheet.
- The description of the stream bed, flow conditions, location of the measurement, weather and any other pertinent information which may have affected the accuracy of the measurement or the stage discharge relationship was recorded on the discharge measurement sheet.
- A field calculation that added the section widths, totalled the section widths and computed the discharge was performed.

Long-Throated Flume Discharge Measurement Procedure

Instantaneous discharge measurements are taken using either the 100mm or 200mm long-throated flumes depending on stream stage and flow conditions. The 100mm flume is capable of measuring flows ranging from 0.0078 cfs to 0.3099 cfs, and the 200mm flume is capable of measuring flows ranging from 0.0367 cfs to 1.762 cfs.

Both flumes are custom built, galvanized sheetmetal rated structures. A water intake port in the flume channel is hydraulically connected to a clear plastic stilling well that is attached to the structure. The water level in the flume channel is measured as hydraulic head in the stilling well. The structures are mathematically rated, which enables a conversion of the measured hydraulic head to a corresponding discharge.

Procedures for obtaining instantaneous discharge measurements with either the 100mm or 200mm long-throated flumes are as follows:

- Select a site in the channel for the flume. This site should be in a reach of the channel that is straight both upstream and downstream of the flume site. The channel should be free of obstructions and have uniform flow.
- Record gage height (if available) and time in the log book and on the data sheet.
- Prepare the channel at the flume site by removing any rocks or debris which will interfere with leveling and sealing of the flume during installation.
- Install the flume in the channel making sure the flume is stable and level. Leveling of the cross-slope and longitudinal slope may be done with a carpenter's level.
- Seal the bottoms and sides of both the upstream and downstream faces of the wingwalls of the flume with soil. The flume must be completely sealed so that all flow is diverted through the flume for an accurate measurement.
- Allow the flow to stabilize over the sill of the flume. Check for leaks around the edges and bottom of the flume and seal if necessary.
- Obtain the sill-referenced head by measuring the distance from the top of the sill to the water level in the stilling well with a metal tape measure.
- For each size of flume, a rating table was prepared (see stage discharge relationship

tables). Using the proper rating table, find the h value, in feet, and record the corresponding discharge value, in cfs. The head, discharge, time and gage height (if available) are recorded in the log book and on the data sheet. Generally, there are three discharge measurements taken at five minute intervals at each site.

APPENDIX A-2.3

1989 Water Year Instantaneous
Discharge Measurement Records

WY89 Discharge Measurements Summary

APPENDIX A-2.3 TABLE A-2.3-1

SUMMARY OF DISCHARGE MEASUREMENTS FOR MONITORING STATIONS

| SITE ID# | SITE NAME | DATE | INSTRUMENT TYPE | DISCH (CFS) | STAGE (FT) START/STOP | COMMENTS LOCATION |
|----------|-------------------------|-------|--------------------|----------------|--------------------------|------------------------------|
| SW01001 | N. UVALDA | 89269 | FLUME-100MM | 0.03 | 0.19 | STAGE CONVERTED TO DISCHARGE |
| SW02006 | STEAM PLANT EFFLUENT | 89117 | FLUME-200MM | 0.34 | NA | EVEN WITH SURVEY STK |
| | | 89167 | FLUME-100MM | 0.09 | NA | EVEN WITH SURVEY STK |
| | | 89201 | FLUME-100MM | 0.06 | NA | EVEN WITH SURVEY STK |
| | | 89270 | FLUME-100MM | 0.11 | NA | 10FT UP STAKE |
| SW07001 | UVALDA DITCH A | 89268 | FLUME-100MM | 0.06 | NA | |
| SW07002 | UVALDA DITCH B | 89268 | FLUME-100MM | 0.17 | NA | |
| SW08001 | | 89272 | FLUME-100MM | 0.14 | NA | 1100' ABOVE SW08003 |
| SW08003 | S FIRST CREEK | 89097 | PYG CURRENT METER | 0.59 | 0.49 | 25FT BELOW GAGE |
| | | 89102 | PYG CURRENT METER | 1.06 | 0.58/0.57 | 43FT BELOW GAGE |
| | | 89115 | FLUME-200MM | 0.72 | 0.47 | 40FT BELOW GAGE |
| | | 89123 | FLUME-200MM | 0.86 | 0.50 | 40FT BELOW GAGE |
| | | 89125 | PYG CURRENT METER | 9.23 | 1.23/1.22 | 40FT BELOW GAGE |
| | | 89134 | NA | 6.40 | 1.10 | CALCULATED FROM STAGE |
| | | 89171 | FLUME-200MM | 0.69 | 0.48 | 30FT BELOW GAGE |
| | | 89201 | FLUME-100MM | 0.01 | 0.13 | 30FT BELOW GAGE |
| | | 89269 | FLUME-100MM | 0.10 | 0.22 | 30FT BELOW GAGE |
| | | 89272 | FLUME-100MM | 0.06 | 0.20 | 30FT BELOW WEIR |
| SW08004 | | 89272 | FLUME-100MM | 0.04 | NA | 1400' BELOW SW08003 |
| SW11001 | PEORIA INT | 89116 | FLUME-200MM | 0.13 | 0.72 | 30FT BELOW WEIR |
| | | 89134 | NA | 14.01 | 1.56 | CALCULATED FROM STAGE |
| | | 89201 | FLUME-200MM | 0.16 | 0.69 | 30FT BELOW WEIR |
| | | 89270 | FLUME-100MM | 0.05 | 0.70 | 100FT BELOW GAGE |
| SW11002 | HAVANA INT | 89101 | PYG CURRENT METER | 1.46 | 0.52/0.51 | 8FT DWNSTR BUBBLER |
| | | 89116 | PYG CURRENT METER | 0.37 | 0.25 | UNDER OLD BRIDGE |
| | | 89130 | NA | 20.87 | 1.00 | CALCULATED FROM STAGE |
| | | 89201 | FLUME-200MM | 0.37 | 0.23 | END OF CONC CHANNEL |
| | | 89270 | FLUME-200MM | 0.49 | 0.25 | END OF CONC CHANNEL |

APPENDIX A-2.3 TABLE A-2.3-1

SUMMARY OF DISCHARGE MEASUREMENTS FOR MONITORING STATIONS

| SITE ID# | SITE NAME | DATE | INSTRUMENT TYPE | DISCH (CFS) | STAGE (FT) START/STOP | COMMENTS LOCATION |
|----------|--------------------------------|-------|--------------------|----------------|--------------------------|-----------------------|
| SW12001 | UVALDA DITCH C | 89110 | PYG CURRENT METER | 0.33 | NA | |
| | | 89268 | FLUME-200MM | 0.27 | NA | |
| SW12005 | S. UVALDA | 89080 | PYG CURRENT METER | 0.26 | 3.85 | 30FT BELOW WEIR |
| | | 89080 | PYG CURRENT METER | 0.30 | 3.85 | 30FT BELOW WEIR |
| | | 89107 | PYG CURRENT METER | 0.35 | 3.80 | 30FT BELOW WEIR |
| | | 89111 | FLUME-200MM | 0.26 | 3.84 | 30FT BELOW GAGE |
| | | 89130 | NA | 4.53 | 4.58 | CALCULATED FROM STAGE |
| | | 89171 | FLUME-200MM | 0.54 | 3.88 | 40FT BELOW GAGE |
| | | 89269 | FLUME-200MM | 0.30 | 0.51 | 30FT BELOW GAGE |
| SW12008 | | 89272 | FLUME-200MM | 0.17 | 0.50 | 50FT BELOW GAGE |
| | | | | | | |
| SW12008 | | 89272 | FLUME-200MM | 0.11 | NA | .41MILES BELOW 12005 |
| SW12009 | | 89272 | FLUME-200MM | 0.10 | NA | .90MILES BELOW 12005 |
| SW24001 | SEWAGE PLANT | 89138 | NA/VOLUMETRIC | 0.01 | NA | END OF PIPE |
| | | 89270 | NA/VOLUMETRIC | NA | NA | VARIABLE FLOW |
| SW24002 | N FIRST CREEK | 89096 | PYG CURRENT METER | 0.32 | 0.47 | 35FT BELOW WEIR |
| | | 89111 | PYG CURRENT METER | 0.31 | 0.46/0.47 | 55FT BELOW GAGE |
| | | 89123 | FLUME-200MM | 0.79 | 0.52 | 30FT BELOW GAGE |
| | | 89135 | PYG CURRENT METER | 3.35 | 0.93/0.92 | |
| SW24004 | FIRST CREEK NORTH BOUNDARY | 89114 | FLUME-200MM | 0.14 | NA | |
| SW30002 | FIRST CREEK AT NORTH PLANTS | 89114 | FLUME-200MM | 0.46 | NA | |
| SW36001 | BASIN A | 89271 | NA-VOLUMETRIC | 0.02 | 0.11 | END OF DISC PIPE |

APPENDIX A-2.3 TABLE A-2.3-1

SUMMARY OF DISCHARGE MEASUREMENTS FOR MONITORING STATIONS

| SITE ID# | SITE NAME | DATE | INSTRUMENT TYPE | DISCH (CFS) | STAGE (FT) START/STOP | COMMENTS LOCATION |
|----------|-------------|-------|--------------------|----------------|--------------------------|----------------------|
| SW37001 | FIRST CREEK | 89097 | PYG CURRENT METER | 0.29 | 0.51 | 40FT ABOVE FLUME |
| | OFF-POST | 89110 | PYG CURRENT METER | 0.31 | 0.52 | 30FT ABOVE GAGE |
| | | 89123 | FLUME-200MM | 0.54 | 0.58 | 40FT ABOVE FLUME |
| | | 89194 | FLUME-100MM | 0.02 | 0.58 | 10FT BELOW FLUME |

NA - NOT APPLICABLE

PYG - GURLEY 625 PYGMY CURRENT METER

WY89 Discharge Measurement Field Records

R. L. STOLLAR & ASSOCIATES

COMPILED BY

COMPILED BY

CHECKED BY _____

69289

WIDTH NA AREA NA VEL. NA GH. 19 DISCH. 5.3

WIDTH NA AREA NA VEL. NA GH. 19 DISCH. 5.3

MASTER TYPE

SPIN BEFORE MEAS. ΔA AFTER ΔA

WADING, UP STR., DOWNS I.R., SIDE BRIDGE

MEASUREMENT RATED EXCELLENT (2%) GOOD (5%) FAIR (8%) POOR (OVER 8%) BASED ON

100

OTHER 7.5%

CAGE 27-01-0001

60 24

RESIDUES REMOVED 110 INTAKE FLUSHED 1

[illegible]

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| TIME | RECORDED | INDEXED | FILED |
|------|----------|---------|-------|
|------|----------|---------|-------|

WEIGHTED M.G.H.

CORRECT M.G.H.

START @ 1600
FINISH @ 1620

MEASUREMENT NO. _____
COMPILED BY JK
CHECKED BY JK

DATE 89117 4/27 '89 PARTY JK, LB, KH

METHOD LONG, TARGATED G.H. CHANGE NA IN HRS
FLUME NO. SECS

SPIN BEFORE MEAS. NA AFTER NA

FOR RENT, COUNTRY, DOMESTIC, SIDE BRIDGE

FEET, MILE, ABOVE, BELOW GAGE, AI

FLOW LOW - UNIFORM WEATHER COOL, CLOUDY, LT WIND

[illegible]

| | | | |
|----------------|-----|----------------|-----|
| RECORD REMOVED | N/A | INTAKE FLUSHED | N/A |
|----------------|-----|----------------|-----|

Observer

[illegible]

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GAGE READINGS

[illegible][illegible]

R. L. STOLLAR & ASSOCIATES

COMPILED BY
CHECKED BY

STATION NAME SOUTH PLANTS STEAM EFF SW 02006

| DATE | WIDTH | AREA | VEI | PARTY | JK |
|--------|--------|------|-----|--------|----|
| 89/107 | 2 | 6/16 | | '19 89 | |
| | ~ 1.5' | | | | |

WIDTH ~1.5' AREA 171.11 sq ft VEL. G.H. DISCH. 0.0907

METHOD 100 MM NO. SECS NA G.H. CHANGE NA IN HRS

METER TYPE N/A

SPIN BEFORE MEAS. NA AFTER NA
MEAS PLOTS % DIFF FROM RATING

WADING, UPSTR., DOWNSTR., SIDE BRIDGE _____ FEET, MILE, ABOVE, BELOW GAGE AND
MIAS. FLOTS _____ % DIFF. FROM _____ HA LING

MEASUREMENT RATED EXCELLENT (2%) GOOD (5%) FAIR (8%) POOR (OVER 8%) BASED ON

FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW-UNIFORM WEATHER WARM, SUNNY, NO WIND

OTHER _____

| | | | | | |
|------|------|-----------|-------|---------|---------|
| GAGE | NONE | INSTALLED | | 2/15/50 | 1175 |
| | | | | | 40 1162 |

1125 WATER 2000 OF@

RECORD REMOVED NA INTAKE FLUSHED NA

OBSERVER _____

100

| CONTROL | NO CONTROL | INSTALLED |
|---------|------------|-----------|
| | | |

| | REMARKS |
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| 0099 | |

NEWARK

| G.H. OF ZERO FLOW | FT |
|-------------------|------|
| 10.0 | 10.0 |
| 10.1 | 10.1 |
| 10.2 | 10.2 |
| 10.3 | 10.3 |
| 10.4 | 10.4 |
| 10.5 | 10.5 |
| 10.6 | 10.6 |
| 10.7 | 10.7 |
| 10.8 | 10.8 |
| 10.9 | 10.9 |
| 11.0 | 11.0 |
| 11.1 | 11.1 |
| 11.2 | 11.2 |
| 11.3 | 11.3 |
| 11.4 | 11.4 |
| 11.5 | 11.5 |
| 11.6 | 11.6 |
| 11.7 | 11.7 |
| 11.8 | 11.8 |
| 11.9 | 11.9 |
| 12.0 | 12.0 |
| 12.1 | 12.1 |
| 12.2 | 12.2 |
| 12.3 | 12.3 |
| 12.4 | 12.4 |
| 12.5 | 12.5 |
| 12.6 | 12.6 |
| 12.7 | 12.7 |
| 12.8 | 12.8 |
| 12.9 | 12.9 |
| 13.0 | 13.0 |
| 13.1 | 13.1 |
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| 13.5 | 13.5 |
| 13.6 | 13.6 |
| 13.7 | 13.7 |
| 13.8 | 13.8 |
| 13.9 | 13.9 |
| 14.0 | 14.0 |
| 14.1 | 14.1 |
| 14.2 | 14.2 |
| 14.3 | 14.3 |
| 14.4 | 14.4 |
| 14.5 | 14.5 |
| 14.6 | 14.6 |
| 14.7 | 14.7 |
| 14.8 | 14.8 |
| 14.9 | 14.9 |
| 15.0 | 15.0 |
| 15.1 | 15.1 |
| 15.2 | 15.2 |
| 15.3 | 15.3 |
| 15.4 | 15.4 |
| 15.5 | 15.5 |
| 15.6 | 15.6 |
| 15.7 | 15.7 |
| 15.8 | 15.8 |
| 15.9 | 15.9 |
| 16.0 | 16.0 |
| 16.1 | 16.1 |
| 16.2 | 16.2 |
| 16.3 | 16.3 |
| 16.4 | 16.4 |
| 16.5 | 16.5 |
| 16.6 | 16.6 |
| 16.7 | 16.7 |
| 16.8 | 16.8 |
| 16.9 | 16.9 |
| 17.0 | 17.0 |
| 17.1 | 17.1 |
| 17.2 | 17.2 |
| 17.3 | 17.3 |
| 17.4 | 17.4 |
| 17.5 | 17.5 |
| 17.6 | 17.6 |
| 17.7 | 17.7 |
| 17.8 | 17.8 |
| 17.9 | 17.9 |
| 18.0 | 18.0 |
| 18.1 | 18.1 |
| 18.2 | 18.2 |
| 18.3 | 18.3 |
| 18.4 | 18.4 |
| 18.5 | 18.5 |
| 18.6 | 18.6 |
| 18.7 | 18.7 |
| 18.8 | 18.8 |
| 18.9 | 18.9 |
| 19.0 | 19.0 |
| 19.1 | 19.1 |
| 19.2 | 19.2 |
| 19.3 | 19.3 |
| 19.4 | 19.4 |
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| 19.8 | 19.8 |
| 19.9 | 19.9 |
| 20.0 | 20.0 |
| 20.1 | 20.1 |
| 20.2 | 20.2 |
| 20.3 | 20.3 |
| 20.4 | 20.4 |
| 20.5 | 20.5 |
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| 20.8 | 20.8 |
| 20.9 | 20.9 |
| 21.0 | 21.0 |
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| 23.8 | 23.8 |
| 23.9 | 23.9 |
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| 24.9 | 24.9 |
| | |

| GAGE READINGS | |
|---------------|--|
| | |

| TIME | | RECORDER | INSIDE | OUTSIDE |
|------|--|----------|--------|---------|
|------|--|----------|--------|---------|

[illegible]

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[illegible]

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[illegible]

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| WEIGHTED M.G.H. | |
| CU CORRECTION | |

| | | |
|-----------------|--|--|
| G.I. CONNECTION | | |
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| | |
|------------------------------|--|
| <p>CORRECT M.G.H.</p> | |
|------------------------------|--|

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|---|--------------|----------|-------------|-----------------|----------|------|-----------|
| USED 100 mm LONG THROATED RECTANGULAR FLUME | | | | | | | |
| 1115 | - FLOW | IN PLACE | $h = 0.16$ | | | | |
| 1120 | - $h = 0.17$ | | | | | | |
| 1125 | - $h = 0.17$ | | | | | | |
| 1130 | - $h = 0.17$ | | | | | | |
| CALCULATED $h = 0.17$ FINAL | | | | | | | |
| $Q = 0.0907 \text{ cfs}$ | | | | | | | |

R. L. STOLLAR & ASSOCIATES

COMPILED BY TS
CHECKED BY _____

STATION NAME 502' 02' 00"

DATE 5/27/20 9/27 '19 89 PARTY T2 SEG, GPJ00
WIDTH AREA VEL. G.H. 113 DISCH. 1107

METHOD 12/1/62 NO. SECS 12/1/62 G.H. CHANGE IN HRS.

METER TYPE _____
 SPIN BEFORE MEAS. _____ AFTER _____
 MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
 WADING (UPSTR., DOWNSTR., SIDE BRIDGE) _____ FEET, MILE ABOVE, BELOW GAGE, AND _____
Stations, Street

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW Low WEATHER Hot & Clear

OTHER AIR 80 40 1230

GAGE None installed

RECORD REMOVED _____ INTAKE FLUSHED L _____

OBSERVER _____

CONTROL LINE INSTALLED

REMARKS Well sampling.

G.H. OF ZERO FLOW _____ FT.

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|---|----------|-------|-------------|-----------------|----------|------|-----------|
| We ran long threaded plug | | | | | | | |
| | | 1.04' | | cfs | | Time | |
| #1 | | .19 | | .1107 | | 1320 | |
| #2 | | .19 | | .1107 | | 1325 | |
| #3 | | .19 | | .1107 | | 1330 | |
| Total length of reference tube = 1.5' | | | | | | | |
| Top of tube to top of sill = .48' | | | | | | | |
| Total depth of H ₂ O = 1.01' (in tube) | | | | | | | |
| | .5' | .21 | | .29' | | | |
| | .48' | .29' | | .19' | | | |
| | h = .19' | | | .1107 cfs | | | |

R. L. STOLLAR & ASSOCIATES

COMPILED BY

CHECKED BY

—

DATE 8/268 9/25 19 89 PARTY S.G. G.02 JG
WIDTH AREA VEL. G.H. DISCH. 0.0

METHOD Flow NO. SECS _____ G.H. CHANGE _____ IN _____ HRS.

SPIN BEFORE MEAS. AFTER

WADING, UPSTR., DOWNSTR., SIDE BRIDGE

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW Low, ch. form WEATHER clean, warm

OTHER _____ AIR 75 ♀@ 10/16/

| GAGE | WATER | 12,9 | °F @ | 2523 |
|------|-------|------|------|------|
| None | | | | |

RECORD REMOVED

OBSERVER _____

CONTROL None installed

[illegible]

Don't miss self-learned nation for

24 pens & re. 11/11
G.H. OF ZERO FLOW
CT

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|--|-------|-------------------------|-------------|-----------------|----------|-------|-----------|
| Location | | Reference | | | | | |
| | | B (Ref) | CB | | | Time | |
| #1 | | .141 | | .0643 | | .0945 | |
| #2 | | .141 | | .0643 | | .0950 | |
| #3 | | .141 | | .0643 | | .0950 | |
| Total length of reference tube = 2.5' | | | | | | | |
| Top of tube to top of well = .148' | | | | | | | |
| Total depth of H ₂ O in tube = .16' | | | | | | | |
| | | .15' - .16' = .34' | | | | | |
| | | .148' - .34' = .14' (h) | | | | | |
| | | b = .14 = .0643 cfs | | | | | |

R. L. STOLLAR & ASSOCIATES

76

21

| DATE | WIDTH | AREA | VEI | PARTY | 56 |
|---------|----------|------|-----|-------|----|
| 7/25/89 | 87268.19 | 87 | | GP | 56 |

METER TYPE

MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____

WADING, UPSTR., DOWNSTR., SIDE BRIDGE FE

FLOW low

OTHER _____ AIR _____

GAGE WATER

RECORD REMOVED _____ INTAKE FLUSHED L _____

OBSERVER

CONTROL None Installed

REMARKS No Station, Fall Sampling.

G.H. OF ZERO FLOW

[illegible][illegible]

R. L. STOLLAR & ASSOCIATES

MEASUREMENT NO.
COMPILED BY
CHECKED BY

STATION NAME SW08001 S. 1st Creek

DATE 89272 9/27 19 89 PARTY GP TG

WIDTH 100 m AREA _____ VEL. _____ G.H. 2000 DISCH. 124

METHOD Flores NO. SECS _____ G.H. CHANGE _____ IN _____ HRS. _____

METER TYPE _____
SPIN BEFORE MEAS. _____ AFTER _____
MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
WADING-UPSTR., DOWNSTR., SIDE BRIDGE _____ FEET, MILE ^{6.6 ft} ABOVE, BELOW GAGE, AND _____
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW low, uniform WEATHER _____
OTHER _____ AIR 85 °F @ 1155
GAGE _____ WATER 15.2 gals @ 1155 U
RECORD REMOVED L INTAKE FLUSHED L

OBSERVER _____

| | |
|---------|---|
| CONTROL | None |
| REMARKS | Crack/loss measurement - Fall Sample Suspended sock sample taken |

G.H. OF ZERO FLOW ET

[illegible][illegible]

R. L. STOLLAR & ASSOCIATES DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. _____
COMPILED BY JK
CHECKED BY _____

STATION NAME SOUTH FIRST CREEK

DATE APRIL 12 1989 PARTY JK KH B5
WIDTH 7.8' AREA 3.012 VEL. .295 G.H. .57 DISCH. 1.064

METHOD Flow Meter NO. SECS 40 G.H. CHANGE 0 IN 1.5 HRS.

METER TYPE WILLEY #625 PYGMY WIRENT NO. NN63489
SPIN BEFORE MEAS. 50 AFTER _____
MEAS. PLOTS _____ % DIFF. FROM _____
WADING, UPSTR./DOWNSTR. SIDE BRIDGE 43 (FEET) MILE, ABOVE/BELOW GAGE AND _____

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW LOW TO MODERATE WEATHER SUNNY LIGHT WIND <5 mph

OTHER _____ AIR 50 °F @ 1536
GAGE STAFF GAGE WATER 45 °F @ 1536
RECORD REMOVED NOY INTAKE FLUSHED L NO

OBSERVER _____

CONTROL CONCRETE WEIR ~30 FT UPSTREAM
REMARKS REMOVED TUMBLEWEEDS AND AQUATIC GROWTH
10'-20' below CEMENT CONTROL STRUCTURE

G.H. OF ZERO FLOW _____ FT

| GAGE READINGS | | | |
|-----------------|------------|------------------|-------------|
| TIME | RECORDER | INSIDE | OUTSIDE |
| 1536 | | | |
| 1536 | <u>.57</u> | <u>JK 571.02</u> | <u>0.58</u> |
| 1627 | <u>.57</u> | <u>0.57</u> | <u>0.57</u> |
| 1647 | <u>.57</u> | | <u>.57</u> |
| WEIGHTED M.G.H. | | | |
| G.H. CORRECTION | | | |
| CORRECT M.G.H. | | | |
| | <u>.57</u> | | |

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|-------|-------|-------------|-----------------|-------------|--------------|--------------|
| 2.90 | .15 | .40 | 0 | 40 | 0.000 | .160 | 0.000 |
| 3.20 | .30 | .41 | 12 | 40 | 0.300 | .123 | 0.037 |
| 3.50 | .30 | .42 | 13 | 40 | 0.325 | .126 | 0.041 |
| 3.80 | .30 | .47 | 11 | 40 | 0.275 | .141 | 0.039 |
| 4.10 | .30 | .48 | 13 | 40 | 0.325 | .144 | 0.047 |
| 4.40 | .30 | .49 | 11 | 40 | 0.275 | .147 | 0.040 |
| 4.70 | .30 | .44 | 10 | 40 | 0.250 | .132 | 0.033 |
| 5.00 | .30 | .45 | 10 | 40 | 0.250 | .135 | 0.034 |
| 5.30 | .30 | .45 | 10 | 40 | 0.250 | .135 | 0.034 |
| 5.60 | .30 | .45 | 11 | 40 | 0.275 | .135 | 0.037 |
| 5.90 | .30 | .50 | 12 | 40 | 0.300 | .150 | 0.045 |
| 6.20 | .30 | .51 | 11 | 46 | 0.275 | .153 | 0.047 |
| 6.50 | .30 | .52 | 10 | 40 | 0.250 | .156 | 0.039 |
| 6.80 | .30 | .53 | 10 | 40 | 0.250 | .159 | 0.040 |
| 7.10 | .30 | .52 | 10 | 40 | 0.250 | .156 | 0.039 |
| 7.40 | .30 | .58 | 10 | 40 | 0.250 | .174 | 0.044 |
| 7.70 | .30 | .59 | 11 | 40 | 0.275 | .177 | 0.049 |
| 8.00 | .30 | .58 | 13 | 40 | 0.325 | .174 | 0.057 |
| 8.30 | .30 | .58 | 14 | 40 | 0.350 | .174 | 0.061 |
| 8.60 | .30 | .57 | 14 | 40 | 0.350 | .159 | 0.057 |
| 8.90 | .30 | .49 | 14 | 40 | 0.350 | .147 | 0.050 |
| 9.20 | .30 | .46 | 18 | 40 | 0.450 | .138 | 0.062 |
| 9.50 | .30 | .44 | 18 | 40 | 0.450 | .132 | 0.059 |
| 9.80 | .30 | .41 | 15 | 40 | 0.375 | .123 | 0.046 |
| 10.10 | .30 | .32 | 14 | 40 | 0.350 | .096 | 0.034 |
| 10.40 | .30 | .22 | 0 | 40 | 0.000 | .066 | 0.000 |
| 10.70 | .15 | .00 | 0 | 40 | 0.000 | .000 | 0.000 |
| | | | | | <u>.295</u> | <u>3.612</u> | <u>1.064</u> |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. _____
COMPILED BY _____
CHECKED BY PA

STATION NAME SOUTH FIRST CREEK (SW08003)
DATE MAY 3 '89 PARTY JK+BS
WIDTH _____ AREA _____ VEL. _____ G.H. 0.50 DISCH. 0.56
METHOD 200mm FLYWHEEL SECS _____ G.H. CHANGE 0 IN. 5 HRS. _____

METER TYPE NA
SPIN BEFORE MEAS. _____ AFTER _____
MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
WADING: UPSTR., DOWNSTR., SIDE BRIDGE 40 FEET, MILE, ABOVE, BELOW GAGE, AND _____
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW Uniform WEATHER Sunny
 OTHER AIR 60's F@
 GAGE Good Shape WATER 50's OF@ U
 RECORD REMOVED NO INTAKE FLUSHED LAD
 OBSERVER _____

| | |
|---------|---|
| CONTROL | CLEAR |
| REMARKS | CHECKING FOR VARIATION w/ FULME MEASUREMENT |

_____ G.H. OF ZERO FLOW _____ FT

| GAGE READINGS | | | | |
|-----------------|--------|----------|--------|---------|
| TIME | | RECORDER | INSIDE | OUTSIDE |
| 0915 | BEFORE | 0.50 | — | 0.50 |
| 0920 | DURING | 0.50 | | 0.50 |
| 0925 | " | 0.50 | | 0.50 |
| 0930 | " | 0.50 | | 0.50 |
| 0935 | AFTER | 0.50 | | 0.50 |
| WEIGHTED M.G.H. | | | | |
| G.H. CORRECTION | | | | |
| CORRECT M.G.H. | | | | |

[illegible]

R. L. STOLLAR & ASSOCIATES DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. _____
COMPILED BY _____
CHECKED BY _____

STATION NAME SOUTA FIRST CREEK (608003)
DATE 8/12/89 PART BS, JK, PG
WIDTH 5.5 AREA _____ VEL. _____ G.H. _____ DISCH. _____

METHOD 6 NO. SECS _____ G.H. CHANGE _____ IN _____ HRS. _____

METER TYPE BURLEY 625 PYGMY SER # ANUG349
SPIN BEFORE MEAS. 40 AFTER _____

MEAS. PLOTS _____ % DIFF. FROM _____
WADING, UPSTR. DOWNSTR. SIDE BRIDGE 400 FEET MILE, ABOVE, BELOW GAGE, AND _____

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW HIGH - NON UNIFORM WEATHER WARM SUNNY, BREEZY

OTHER SOMEEDGE BACKWATER AIR 65 @ 102.0

GAGE STAFF - GOOD SHAPE WATER 55 @ 102.0

OBSERVER DOUG GREER - RTV RECORD REMOVED _____ INTAKE FLUSHED L NO

CONTROL V - NOTCH CEMENT WEIR

REMARKS HIGH FLOW FOR UNKNOWN REASONS

CLEARED SAGE OUT DOWNSTREAM OF CONTROL

G.H. OF ZERO FLOW _____ FT

GAGE READINGS

| TIME | RECORDED | INSIDE | OUTSIDE |
|-----------------|----------|--------|---------|
| 1020 NOT | BEFORE | 1.23 | 1.23 |
| 1031 | START | 1.23 | 1.23 |
| 1052 | MID | 1.23 | 1.22 |
| 1108 | END | 1.23 | 1.22 |
| 1110 | AFTER | 1.23 | 1.22 |
| WEIGHTED M.G.H. | | | |
| G.H. CORRECTION | | | |
| CORRECT M.G.H. | | | |

BW = BACK WATER

MEASUREMENT NO.
COMPILED BY
CHECKED BY

STATION NAME SOUTH FIRST CREEK (JW09003)
DATE 8/7/19 PARTY JR KA, LH
WIDTH 21A AREA FLUME VEL. GH. DISCH. _____
METHOD 200MM NO. SECS NA G.H. CHANGE 7 IN. 5 HRS.

METER TYPE N/A
 SPIN BEFORE MEAS. N/A AFTER N/A
 MEAS. PLOTS N/A % DIFF. FROM RATING
 WADING, UP-STR. DOWN-STR., SIDE BRIDGE 30 FEET, MILE, ABOVE BELOW GAGE, AND
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW-MOD WEATHER WARM, SUNNY, LT WIND
OTHER _____ AIR 90° °F @ 1245
GAGE STAFF - GOOD COND WATER 60° °F @ 1245
RECORD REMOVED YES INTAKE FLUSHED L^U AND

OBSERVER _____

| | | |
|---------|-----------|-----|
| CONTROL | ✓ - NOTED | WGR |
| REMARKS | | |

G.H. OF ZERO FLOW _____ FT

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|---------------------------------|-------|-------------|-----------------|--------------|------|-----------|
| 1230 | START MONITORING THROATED FLUME | | | | | | |
| 1235 | $h = 0.40$ | | | | $Q = 0.6915$ | | |
| 1245 | $h = 0.40$ | | | | $Q = 0.6915$ | | |
| 1252 | $h = 0.40$ | | | | $Q = 0.6915$ | | |
| $Q = 0.6915 \text{ cfs}$ | | | | | | | |

DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. _____
COMPILED BY TG
CHECKED BY _____

STATION NAME Sw08003 S. 1st Creek

DATE 8/27/29 1959 PARTY T6 GAO
WIDTH AREA VEL. GH. 0.20 DISCH. 0.0

METHOD 100m NO. SECS 7/400 G.H. CHANGE 0 IN 0 HRS.

METER TYPE _____
SPIN BEFORE MEAS. _____ AFTER _____

SPIN BEFORE MEAS. _____ AFTER _____
MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
WADING, UPSTR. ~~DOWNSTR.~~ SIDE BRIDGE 30 FEET, MILE, ABOVE, ~~BELOW~~ GAGE, AND

OVERALL
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW low, no, fern WEATHER clear, warm

OTHER _____ AIR 85 F@240

GAGE 120 WATER 18.3% @ 1230

RECORD REMOVED _____ INTAKE FLUSHED _____ L _____

OBSERVER _____

CONTROL Cement v-notch weir

REMARKS Gain/loss measurement - Fall

sampling - suspended sed. sample for TC

G.H. OF ZERO FLOW _____ FT _____

| GAGE READINGS | | | | | |
|-----------------|--|----------|--------|---------|--|
| TIME | | RECORDER | INSIDE | OUTSIDE | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| WEIGHTED M.G.H. | | | | | |
| G.H. CORRECTION | | | | | |
| CORRECT M.G.H. | | | | | |

DISCHARGE MEASUREMENT NOTES

CHECKED BY

METHOD Flame NO. SECS _____ G.H. CHANGE _____ IN _____ HRS.

FOLLOWING CONDITIONS: CROSS SECTION

FLOW low, uniform WEATHER clear, warm

OTHER _____ AIR & S F@ 1222

GAGE _____ WATER _____ °F @ _____

RECORD REMOVED | INTAKE FILISHED | 0

OBSERVER _____

CONTROL _____

fall sampling, sediment sample taken

G.H. OF ZERO FLOW

CORRECT M.G.H.

R. L. STOLLAR & ASSOCIATES

MEASUREMENT NO.:

COMBIL EN BY

COMPILED BY
CHECKED BY

STATION NAME PEORIA INTERCEPT (SW11001)

DATE 89116 4/26 1989 PARTY DK, LB, KH

WIDTH _____ AREA _____ VEL. _____ G.H. _____ DISCH. _____

| METHOD | LONG THROATED FLUME | NO. SECS | G.H. CHANGE | IN | HBS |
|--------|------------------------|----------|-------------|----|-----|
| | | N/A | | | |

METER TYPE N/A

SPIN BEFORE MEAS. NA AFTER NA
MEAS. PLOTS % DIFF. FROM RATING

WADING, UPSTR, DOWNSTR, SIDE BRIDGE 30 FEET, MILE, ABOVE, BELOW GAGE, AND

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW Low - Uniform WEATHER COOL CLOUDY

OTHER _____ AIR 50° CF@ 1010

GAGE STAFF 50° OF @ 1010 WATER

RECORD REMOVED
INTAKE FILISHED
U

OBSERVER

CONTROL

REMARKS

G.H. OF ZERO FLOW

[illegible]

FOPM31 / DEC 87

R. L. STOLLAR & ASSOCIATES

DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO.

COMPILED BY

CHECKED BY

STATION NAME Sullivan Prairie Interceptor

DATE 87270 9/27 19 87 PARTY GRP, JG, JEG

| WIDTH | AREA | VEL. | G.H. | DISCH. |
|-------|------|------|------|--------|
| | | | 70 | 0.982 |

METHOD Fluor NO. SECS 0.02 IN 1/2 HRS.

METER TYPE

SPIN BEFORE MEAS.

MEAS. PLOTS

WADING, UPSTR. DOWNSTR. SIDE BRIDGE

... I LEFT, MILL, ABOVE BELLOW GAGE; AND

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%) BASED ON

FOLLOWING CONDITIONS: CROSS SECTION

FLOW Low WEATHER Partly Cloudy 40-55

OTHER B

100

00000073

100

[illegible]

RECORD REMOVED

OBSERVER

RECORD REMOVED

INTAKE FLUSHED I

CONTROL Metal V-patch Wein

REMARKS Fall sampling

G.H. OF ZERO FLOW

5

[illegible]

| | |
|-----|------|
| LEW | 2.2' |
| REW | 7.0' |

SH: DDE RG

SW 11002

DISCH. : 346

IN _____ HRS.

OW GAGE AND

%), BASED ON

ND 0-5 mph

1324

1324

7 Q31

2

ET

| |
|---------|
| |
| |
| OUTSIDE |
| 0.25 |
| |
| |
| |
| |
| |
| |

[illegible]

R. L. STOLLAR & ASSOCIATES

COMPILER NO. 725

| | | | | | | | | | | | |
|--------------|---------|--|----------|--|------|-------------------|-------------|--|--------------|--|------------|
| STATION NAME | SW11002 | | | | | Hammock Intersect | | | | | |
| DATE | 8/27/01 | | 9/27 | | 1989 | | PARTY | | GPP, TG, SFG | | |
| WIDTH | | | AREA | | | | VEL. | | GH | | DISCH. 149 |
| METHOD | Flyline | | NO. SECS | | | | G.H. CHANGE | | IN | | HRS. |

METER TYPE _____
 SPIN BEFORE MEAS. _____ AFTER _____
 MEAS. PILOTS _____ % DIFF. FROM _____ RATING _____
 WADING, UPSTR. (DOWNSTR.) SIDE BRIDGE 50-50 FEET, MILE, ABOVE, BELOW GAGE, AND _____
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW low in stream WEATHER Partly cloudy
OTHER _____ AIR 75° @ 1034
GAGE Depth over bubble line WATER _____ @ _____
RECORD REMOVED No INTAKE FLUSHED Yes

OBSERVER _____

| | |
|---------|--|
| CONTROL | Concrete channel |
| REMARKS | Fall sampling, measurement made 100' below the end of concrete channel |

G.H. OF ZERO FLOW

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|--|--------------------------------|-------|-------------|-----------------|----------|-------|-----------|
| 300 mm length of broad flume | | | | | | | |
| | $h(1) = 1.33'$ | | | CFS | | Time | |
| #1 | 1.33 | | | 4900 | | 10.25 | |
| #2 | 1.33 | | | 4900 | | 10.25 | |
| #3 | 1.33 | | | 4900 | | 10.30 | |
| Total length of reference tube = 1.05' | | | | | | | |
| Top of tube to top of sill = .90' | | | | | | | |
| Total depth of H_2O = .47' (in tube) | | | | | | | |
| | | 1.05 | .47' = .58' | | | | |
| | | .90' | .58' = .33' | | | | |
| | $h = .33' = 14900 \text{ CFS}$ | | | | | | |
| Depth over bubble line = 0.249 | | | | | | | |
| CR10 | #6 | 1 | .25297 | | | | |
| | | 2 | .28547 | | | | |
| | | 3 | 15.128 | | | | |
| | | 4 | 1.0400 | | | | |
| | | 5 | 12.050 | | | | |
| | | 6 | 0.00 | | | | |

DISCHARGE MEASUREMENT NOTES

CHECKED BY

3

DATE APRIL 20 1989 PARTY JK, SG
WIDTH 500' AREA 1.92 VEL. 2.40 G.H. NA DISCH. 0.325

METHOD 60 NO. SECS 40 G.H. CHANGE NA IN 0 HRS.

METER TYPE PYGMY

SPIN BEFORE MEAS. 47 AFTER 45

| MEAS. PLOTS | % DIFF. FROM | RATING |
|-------------|--------------|--------|
| 1 | 10 | 1 |
| 2 | 10 | 1 |
| 3 | 10 | 1 |
| 4 | 10 | 1 |
| 5 | 10 | 1 |
| 6 | 10 | 1 |
| 7 | 10 | 1 |
| 8 | 10 | 1 |
| 9 | 10 | 1 |
| 10 | 10 | 1 |
| 11 | 10 | 1 |
| 12 | 10 | 1 |
| 13 | 10 | 1 |
| 14 | 10 | 1 |
| 15 | 10 | 1 |
| 16 | 10 | 1 |
| 17 | 10 | 1 |
| 18 | 10 | 1 |
| 19 | 10 | 1 |
| 20 | 10 | 1 |
| 21 | 10 | 1 |
| 22 | 10 | 1 |
| 23 | 10 | 1 |
| 24 | 10 | 1 |
| 25 | 10 | 1 |
| 26 | 10 | 1 |
| 27 | 10 | 1 |
| 28 | 10 | 1 |
| 29 | 10 | 1 |
| 30 | 10 | 1 |
| 31 | 10 | 1 |
| 32 | 10 | 1 |
| 33 | 10 | 1 |
| 34 | 10 | 1 |
| 35 | 10 | 1 |
| 36 | 10 | 1 |
| 37 | 10 | 1 |
| 38 | 10 | 1 |
| 39 | 10 | 1 |
| 40 | 10 | 1 |
| 41 | 10 | 1 |
| 42 | 10 | 1 |
| 43 | 10 | 1 |
| 44 | 10 | 1 |
| 45 | 10 | 1 |
| 46 | 10 | 1 |
| 47 | 10 | 1 |
| 48 | 10 | 1 |
| 49 | 10 | 1 |
| 50 | 10 | 1 |
| 51 | 10 | 1 |
| 52 | 10 | 1 |
| 53 | 10 | 1 |
| 54 | 10 | 1 |
| 55 | 10 | 1 |
| 56 | 10 | 1 |
| 57 | 10 | 1 |
| 58 | 10 | 1 |
| 59 | 10 | 1 |
| 60 | 10 | 1 |
| 61 | 10 | 1 |
| 62 | 10 | 1 |
| 63 | 10 | 1 |
| 64 | 10 | 1 |
| 65 | 10 | 1 |
| 66 | 10 | 1 |
| 67 | 10 | 1 |
| 68 | 10 | 1 |
| 69 | 10 | 1 |
| 70 | 10 | 1 |
| 71 | 10 | 1 |
| 72 | 10 | 1 |
| 73 | 10 | 1 |
| 74 | 10 | 1 |
| 75 | 10 | 1 |
| 76 | 10 | 1 |
| 77 | 10 | 1 |
| 78 | 10 | 1 |
| 79 | 10 | 1 |
| 80 | 10 | 1 |
| 81 | 10 | 1 |
| 82 | 10 | 1 |
| 83 | 10 | 1 |
| 84 | 10 | 1 |
| 85 | 10 | 1 |
| 86 | 10 | 1 |
| 87 | 10 | 1 |
| 88 | 10 | 1 |
| 89 | 10 | 1 |
| 90 | 10 | 1 |
| 91 | 10 | 1 |
| 92 | 10 | 1 |
| 93 | 10 | 1 |
| 94 | 10 | 1 |
| 95 | 10 | 1 |
| 96 | 10 | 1 |
| 97 | 10 | 1 |
| 98 | 10 | 1 |
| 99 | 10 | 1 |
| 100 | 10 | 1 |

WADING, UPSTR., DOWNSTR., SIDE BRIDGE

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW, UNIFORM WEATHER SUNNY 56°F NO WIND IN CLOUDY

OTHER _____ A/B .65 ♀@ 1030

GAGE _____ WATER 55 of @ 1030

RECORD REMOVED NONE INTAKE FLUSHED NONE

OBSERVER _____

CONTROL NONE INSTALLED

REMARKS BOTTOM VERY SOFT SLUDG, BANK OF VARIABLE WIDTH - DISCHARGED

TAKEN AS WARRIOR PARTY- DIE CHARMEE

G.H. OF ZERO FLOW

| GAGE READINGS | | | | |
|-----------------|--|----------|--------|---------|
| TIME | | RECORDER | INSIDE | OUTSIDE |
| 1030 JK | | | | |
| 84110 | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| WEIGHTED M.G.H. | | | | |
| G.H. CORRECTION | | | | |
| CORRECT M.G.H. | | | | |

[illegible]

START = 1520 2.20
END = 1547 6.20

COMPILED BY
CHECKED BY

12005

DISCH. 2/20

IN, S. HBS.

y No. 625

AFTER 15

IFF. FROM _____ RATING _____

SIDE BRIDGE 50 FEE

...%), BASED ON

m/sunny

1600

1600

①②③④⑤⑥⑦⑧⑨⑩⑪⑫⑬⑭⑮⑯⑰⑱⑲⑳㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿

OBSERVER

YEAS PT.

NG

BANL

13

[illegible]

NEW 6.20
LEW 2.20

START [REDACTED] 1554
FINISH 1613

| | | | | |
|-----------------|-------------------|----------|----------|----------------------|
| MEASUREMENT NO. | W489 #2- | | | |
| COMPILED BY | ULB | | | |
| CHECKED BY | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | |
| DATE | 89080 | 3/21 | 89 PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. 0.310 G.H. 3.85 |
| FLOW | 6 | NO. SECS | 0.15 | DISCH. 0.299 |
| METHOD | METER | | | G.H. CHANGE 0 |
| | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | W. 1980 | |
| METHOD | METER | | | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | | 0.163 | AC | 0.1980 |
| METHOD | METER | NO. SECS | 175 | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|------|-------|--------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | | 0.163 | AC | 0.1980 |
| METER | NO. SECS | 175 | G.H. | CHANGE | Ø |
| METHOD | DISCH. 0.299 | | | | |
| | IN 1.0 HRS. | | | | |

| | | | | |
|-----------------|-------------------|----------|----------|----------------------|
| MEASUREMENT NO. | W489 #2- | | | |
| COMPILED BY | ULB | | | |
| CHECKED BY | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | |
| DATE | 89080 | 3/21 | 89 PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. 0.310 G.H. 3.85 |
| FLOW | 6 | NO. SECS | 0.15 | DISCH. 0.299 |
| METHOD | METER | | | G.H. CHANGE 0 |
| | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | | 0.163 | AC | 0.1980 |
| METHOD | METER | NO. SECS | 175 | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | W. 1980 | |
| METHOD | METER | | | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | |
|-----------------|-------------------|----------|------------------|-------------|
| MEASUREMENT NO. | W489 #2- | | | |
| COMPILED BY | ULB | | | |
| CHECKED BY | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | |
| DATE | 89080 | 3/21 | 89 PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 VEL. 0.310 | G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | 0.1980 |
| METHOD | METER | | G.H. CHANGE | Ø |
| | | | | IN 1.0 HRS. |

| | | | | |
|-----------------|-------------------|----------|------------------|-------------|
| MEASUREMENT NO. | W489 #2- | | | |
| COMPILED BY | ULB | | | |
| CHECKED BY | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | |
| DATE | 89080 | 3/21 | 89 PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 VEL. 0.310 | G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | 0.1980 |
| METHOD | METER | | G.H. CHANGE | Ø |
| | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | W. 1980 | |
| METHOD | METER | | | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | W. 1980 | |
| METHOD | METER | | | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | | 0.163 | AC | 0.1980 |
| METHOD | METER | NO. SECS | 175 | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

| | | | | | |
|-----------------|-------------------|----------|-------|-------------|-----------------|
| MEASUREMENT NO. | W489 #2 | | | | |
| COMPILED BY | ULB | | | | |
| CHECKED BY | | | | | |
| STATION NAME | SOUTH VALDA 12005 | | | | |
| DATE | 89080 | 3/21 | 89 | PARTY | LB JK |
| WIDTH | 4.0 | AREA | 0.440 | VEL. | 0.310 G.H. \$85 |
| FLOW | 6 | NO. SECS | 0.15 | W. 1980 | |
| METHOD | METER | | | G.H. CHANGE | Ø |
| | | | | | IN 1.0 HRS. |

R. L. STOLLAR & ASSOCIATES DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. 20471187 3 KH
COMPILED BY
CHECKED BY

STATION NAME SOUTH UVALDA SW/2005
DATE 8/10/79 4/17 19 89 PARTY SG KH JK
WIDTH 4.1 AREA 16.47 VEL. 5.43 G.H. 2.81 DISCH. 0.352
METHOD Flow (0.6) NO. SECS G.H. CHANGE IN HRS.
METER TYPE PGMY CURRENT METER (GURLEY) #625 NO. NN6349
SPIN BEFORE MEAS. 60 SEC AFTER 52 SEC
MEAS. PLOTS % DIFF. FROM RATING
WADING, UPSTR., DOWNSTR., SIDE BRIDGE FEET, MILE, ABOVE, BELOW GAGE, AND

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
FOLLOWING CONDITIONS: CROSS SECTION
FLOW LOW-MODERATE WEATHER SUNNY; WIND < 5 mph
OTHER AIR 60 F @ 1248
GAGE WATER 55 OF @ 1248
RECORD REMOVED INTAKE FLUSHED L

OBSERVER PAUL WHITE, BRAD STEPHENSON
CONTROL
REMARKS

G.H. OF ZERO FLOW _____ FT

| GAGE READINGS | | | |
|-----------------|--------------------------------------|--------|-------------|
| TIME | RECORDER | INSIDE | OUTSIDE |
| <u>1203</u> | <u>RECORDED 3.82</u> <u>TO GH</u> | | <u>3.82</u> |
| <u>1254</u> | <u>3.81</u> | | <u>3.81</u> |
| <u>1321</u> | <u>* 3.81</u> | | <u>3.81</u> |
| <u>1331</u> | <u>3.81</u> | | <u>3.81</u> |
| WEIGHTED M.G.H. | | | |
| G.H. CORRECTION | | | |
| CORRECT M.G.H. | | | |

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|-------------|-------------|-------------|-----------------|--------------|--------------|----------------|
| <u>1.8</u> | <u>3.75</u> | <u>0.17</u> | <u>20</u> | <u>40</u> | <u>.000</u> | <u>.000</u> | <u>0.00</u> |
| <u>2.1</u> | <u>2.4</u> | <u>0.18</u> | <u>19</u> | <u>40</u> | <u>.475</u> | <u>.036</u> | <u>.0171</u> |
| <u>2.2</u> | <u>0.2</u> | <u>.18</u> | <u>21</u> | <u>40</u> | <u>.525</u> | <u>.036</u> | <u>.0189</u> |
| <u>2.4</u> | <u>0.2</u> | <u>.18</u> | <u>25</u> | <u>40</u> | <u>.625</u> | <u>.040</u> | <u>.025</u> |
| <u>2.6</u> | <u>0.2</u> | <u>0.20</u> | <u>27</u> | <u>40</u> | <u>.675</u> | <u>.044</u> | <u>.0297</u> |
| <u>2.8</u> | <u>0.2</u> | <u>0.22</u> | <u>20</u> | <u>40</u> | <u>.50</u> | <u>.036</u> | <u>.018</u> |
| <u>3.0</u> | <u>0.2</u> | <u>0.18</u> | <u>22</u> | <u>40</u> | <u>.55</u> | <u>.0425</u> | <u>.023375</u> |
| <u>3.2</u> | <u>0.25</u> | <u>0.17</u> | <u>16</u> | <u>40</u> | <u>.40</u> | <u>.051</u> | <u>.0204</u> |
| <u>3.5</u> | <u>0.3</u> | <u>0.17</u> | <u>23</u> | <u>40</u> | <u>.575</u> | <u>.054</u> | <u>.03105</u> |
| <u>3.8</u> | <u>0.3</u> | <u>0.18</u> | <u>24</u> | <u>40</u> | <u>.60</u> | <u>.048</u> | <u>.0288</u> |
| <u>* 4.1</u> | <u>0.3</u> | <u>0.16</u> | <u>23</u> | <u>40</u> | <u>.515</u> | <u>.054</u> | <u>.03105</u> |
| <u>4.4</u> | <u>0.3</u> | <u>0.18</u> | <u>22</u> | <u>40</u> | <u>.55</u> | <u>.054</u> | <u>.0297</u> |
| <u>4.7</u> | <u>0.3</u> | <u>0.18</u> | <u>24</u> | <u>40</u> | <u>.60</u> | <u>.054</u> | <u>.0324</u> |
| <u>5.0</u> | <u>0.3</u> | <u>0.18</u> | <u>23</u> | <u>40</u> | <u>.575</u> | <u>.042</u> | <u>.02415</u> |
| <u>5.3</u> | <u>0.3</u> | <u>0.14</u> | <u>16</u> | <u>40</u> | <u>.40</u> | <u>.057</u> | <u>.0228</u> |
| <u>5.6</u> | <u>0.3</u> | <u>0.19</u> | <u>0</u> | <u>40</u> | <u>.000</u> | <u>.000</u> | <u>.000</u> |
| <u>5.9</u> | <u>0.15</u> | <u>0.00</u> | | | | | |
| | | | | | <u>0.543</u> | <u>0.049</u> | <u>0.352</u> |

DISCHARGE MEASUREMENT NOTES

JK

METHOD 200 MM FLUME NO. SECS _____ G.H. CHANGE 0 IN 5 HRS. _____

MEAS. PLOTS _____
WADING, UPSTR. DOWNSTR. SIDE BRIDGE _____
% DIFF. FROM _____
RATING 4.0
FEET, MILE, ABOVE, BELOW GAGE, AND
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW-UNIFORM WEATHER COOL, SUNNY

OTHER _____
CAGE 1440-1440-1

RECORD REMOVED NO INTAKE FLUSHED L NO

OBSERVER _____

| CONTROL | REMARKS |
|---------|---------------------------------|
| ✓ | -NOTCH WEIR APPROX 30' UPSTREAM |

REMARKS _____

G.H. OF ZERO FLOW _____

[illegible][illegible]

R. L. STOLLAR & ASSOCIATES

COMPILED BY _____
CHECKED BY TLG

STATION NAME SW/2005 S. Uva/da

DATE 85272 9/29 1985 PARTY TG GPP

METHOD F/147c NO. SECS G.H. CHANGE 0

METER TYPE _____

MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____

FLOW, medium, clay, fern WEATHER clear, warm

OTHER _____ AIR GS #@ 1541

GAGE .50 WATER

RECORD REMOVED No INTAKE FLUSHED No

OBSERVER _____

CONTROL Cement V-notch weir

REMARKS Gain/dess measurement

G.H. OF ZERO FLOW _____

[illegible]

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|---|-------|-------|-------------|-----------------|----------|------|-----------|
| 200 mm Flume | | | | | | | |
| #1 | | .18' | (fs) | .1727 | Time | 1515 | |
| #2: | | .18' | | .1727 | | 1515 | |
| #3 | | .18' | | .1727 | | 1515 | |
| Total length of reference tube = 105' | | | | | | | |
| Top of tube to top of sill = .961' | | | | | | | |
| Total depth of H ₂ O in tube = .133' | | | | | | | |
| 1.05' - .133' = .72' | | | | | | | |
| Top 72% = .961' - .72' = .18'(h) | | | | | | | |
| h = .18 = .1727 cfs | | | | | | | |
| CARIO- | | | | | | | |

R. L. STOLLAR & ASSOCIATES

COMPILED BY
CHECKED BY

STATION NAME SW 1200 78 PT 90024

DATE 89272 9/29 1989 PARTY GDP, IG
 WIDTH _____ AREA _____ VEL. _____ G.H. None DISCH. 11

METHOD Flume NO. SECS _____ G.H. CHANGE _____ IN _____ HRS. _____

METER TYPE _____

SPIN BEFORE MEAS. _____ AFTER _____

MEAS. PLOTS

MEASUREMENT RATED EXCELLENT (2%) GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
WADING, UPSHIFT, DOWNSHIFT, SIDE BRIDGE

FLOW _____ WEATHER clear, warm

OTHER _____ AIR 80 4@ 1643

GAGE _____ WATER _____ °F @ _____

RECORD REMOVED _____ INTAKE FLUSHED L _____

OBSERVER

| Control | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
|---------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| Control | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |

| | |
|---------|----------------------|
| REMARKS | Chassis disconnected |
| | 11 - 1. |

5/21 sampling

| GAGE READINGS | |
|-------------------|----|
| g.n. OF ZERO FLOW | ET |
| | |

[illegible]

R. L. STOLLAR & ASSOCIATES

COMPILED BY
CHECKED BY

STATION NAME SW12006 SW120089 BA 90024

DATE 8-22-22 8/22/1989 PARTY TG GSP

WIDTH 200 m AREA _____ VEL. _____ G.H. 1100 DISCH. 10

METHOD F/6mm NO. SECS _____ G.H. CHANGE _____ IN _____ HRS. _____

METER TYPE _____
 SPIN BEFORE MEAS. _____ AFTER _____
 MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
 WADING, UP-STR. DOWN-STR. SIDE BRIDGE, 2 FEET, 1 MILE, ABOVE, BELOW GAGE, AND
Station 2205
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION

FLOW low, uniform WEATHER clear, warm
OTHER _____ AIR 80 °@ 1608

GAGE _____ WATER _____ °F @ _____ U
RECORD REMOVED _____ INTAKE FLUSHED L

OBSERVER _____

CONTROL _____

REMARKS Green/less on descent
Fall sampling

G.H. OF ZERO FLOW

| GAGE READINGS | | | | | |
|-----------------|--|----------|--------|---------|--|
| TIME | | RECORDER | INSIDE | OUTSIDE | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| WEIGHTED M.G.H. | | | | | |
| G.H. CORRECTION | | | | | |
| CORRECT M.G.H. | | | | | |

[illegible]

MEASUREMENT NO.
COMPILED BY
CHECKED BY

STATION NAME SEWAGE TREATMENT PLANT SW 24001

DATE 8-13-68 PARTY LB RT RT

WIDTH NA AREA _____ VEL. NA G.H. NA DISCH. 0.005

METHOD BUCKET NO SECS NA G.H. CHANGE NA IN _____ HRS. _____

METER TYPE NA
 SPIN BEFORE MEAS. NA AFTER NA
 MEAS. PLOTS NA % DIFF. FROM NA RATING
 WADING, UPSTR., DOWNSTR., SIDE BRIDGE NA FEET, MILE, ABOVE, BELOW GAGE, AND
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW-VNIFORM WEATHER COOL, PT CLOUDY
OTHER _____ AIR 70° F@ 1100
GAGE NONE WATER _____ W@ 1100
RECORD REMOVED _____ INTAKE FLUSHED U N0

OBSERVER _____

CONTROL _____

REMARKS USED TUCKET METHOD TO FIBURE
CFS

G.H. OF ZERO FLOW NA ET

[illegible]

FOPM31 / DEC 87

R. L. STOLLAR & ASSOCIATES

COMPILED BY
CHECKED BY

COMPILED BY
CHECKED BY SP

STATION NAME SW24001 Sewage Treatment Plant

| DATE | WIDTH | AREA | 1959 | PARTY | SEG |
|---------|---------|------|------|-------|---------|
| 9/27/89 | 9/27/89 | | | GPP | TG, SEG |

WIDTH NA AREA NA VEL. NA G.H. NA DISCH. NA
 Volumetric
 METHOD NA NO. SECS NA C.U. CHANGE

METER TYPE GP NO. SECS 111 G.H. CHANGE IN HRS

SPIN BEFORE MEAS. NA AFTER NA
MEAS. PLOTS NA % DIFF. FROM NA RATING

WADING, UPSTR., DOWNSTR., SIDE BRIDGE DATA DATA FEET, MILE, ABOVE, BELOW GAGE, A

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION *✓*

FLOW MED. - NON UNIFORM WEATHER partly cloudy

OTHER NA AIR: 85 40 1420

GAGE UA-NONE INSTALLED WATER 22.3 °C 1430

RECORD REMOVED N/A INTAKE FLUSHED L NO

OBSERVER SPG

[illegible]

| CONTROL | WINE - RETENTION BASIN |
|---------|---------------------------------|
| REMARKS | DEKADATE TRT ACCLIMATED 10-1-00 |

| DATE | TIME | LOCATION | REMARKS |
|----------|-------|------------------|-------------------------------|
| 12/10/71 | 11:00 | 100' N of 100' E | SEWAGE TREAT EFFLUENT - WATER |

G.H. OF ZERO FLOW

[illegible]

FOPM31 / DEC 87

R. L. STOLLAR & ASSOCIATES
DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. WY 84#3
COMPILED BY JK
CHECKED BY

STATION NAME NORTH FIRST CREEK (SW 7777) 24002
DATE 8/9/86 4-6 89 PARTY LB, JK
WIDTH 6.00' AREA 3.53 VEL. 0.091 G.H. 0.47 DISCH. 0.323
METHOD 1.6 METER NO. SECS 30 21 G.H. CHANGE 0 IN 1.5 HRS.

METER TYPE PIGMY #625
SPIN BEFORE MEAS. 48 AFTER 45
MEAS. PLOTS % DIFF. FROM RATING
WADING, UPSTR., DOWNSTR., SIDE BRIDGE 40 REEF MILE, ABOVE, BELOW GAGE, AND

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW - MODERATE WEATHER WARM, SUNNY, WINDY
OTHER WIND RIPPLING SURFACE AIR 65 °F @ 1530
GAGE STAFF / 40' UPSTREAM WATER 50 °F @ 1530
RECORD REMOVED NO INTAKE FLUSHED L NO

OBSERVER

CONTROL ✓ - NOTCH WEIR ≈ 35' UPSTREAM
REMARKS APPROX 40' DOWNSTREAM, AREA FULL OF VEGETATION, VEG REMOVED - NO EFFECTS

G.H. OF ZERO FLOW _____ FT

| GAGE READINGS | | | |
|-----------------|----------|--------|---------|
| TIME | RECORDER | INSIDE | OUTSIDE |
| 1510 | 0.47' | | 0.47' |
| 1522 | 0.47' | | 0.47' |
| 1530 | 0.47' | | 0.47' |
| WEIGHTED M.G.H. | | | |
| G.H. CORRECTION | | | |
| CORRECT M.G.H. | | | |
| | 0.47 | | 0.47 |

LEW = 3.15'
REW = 9.15'

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|-------|-------|-------------|-----------------|----------|-------|-----------|
| 3.15 | .15 | .28 | 0 | 0 | 0.000 | 0.042 | 0.000 |
| 3.45 | .30 | .33 | 0 | 30 | 0.000 | 0.094 | 0.000 |
| 3.75 | .30 | .42 | 0 | 30 | 0.000 | 0.126 | 0.000 |
| 4.05 | .30 | .51 | 0 | 30 | 0.000 | 0.153 | 0.000 |
| 4.35 | .30 | .60 | 0 | 30 | 0.000 | 0.180 | 0.000 |
| 4.65 | .30 | .70 | 0 | 30 | 0.000 | 0.210 | 0.000 |
| 4.95 | .30 | .77 | 0 | 30 | 0.000 | 0.231 | 0.000 |
| 5.25 | .30 | .80 | 0 | 30 | 0.000 | 0.240 | 0.000 |
| 5.55 | .30 | .84 | 2 | 30 | 0.067 | 0.252 | 0.017 |
| 5.85 | .30 | .83 | 11 | 30 | 0.367 | 0.249 | 0.091 |
| 6.15 | .30 | .78 | 11 | 30 | 0.367 | 0.234 | 0.086 |
| 6.45 | .30 | .75 | 7 | 30 | 0.233 | 0.225 | 0.052 |
| 6.75 | .30 | .74 | 6 | 30 | 0.200 | 0.222 | 0.044 |
| 7.05 | .30 | .70 | 2 | 30 | 0.067 | 0.210 | 0.014 |
| 7.35 | .30 | .63 | 2 | 30 | 0.067 | 0.189 | 0.013 |
| 7.65 | .30 | .57 | 1 | 30 | 0.033 | 0.171 | 0.006 |
| 7.95 | .30 | .50 | 0 | 30 | 0.000 | 0.150 | 0.000 |
| 8.25 | .30 | .49 | 0 | 30 | 0.000 | 0.147 | 0.000 |
| 8.55 | .30 | .40 | 0 | 30 | 0.000 | 0.120 | 0.000 |
| 8.85 | .30 | .29 | 0 | 30 | 0.000 | 0.087 | 0.000 |
| 9.15 | .15 | .00 | 0 | 0 | 0.000 | 0.000 | 0.000 |
| | | | | | 0.091 | 3.537 | 0.323 |

Q(6)N

R. L. STOLLAR & ASSOCIATES DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO.
COMPILED BY
CHECKED BY

REH

STATION NAME 24002 NORTH FIRST CREEK
DATE 8/11/89 4/21/89 PARTY L. BRONVILLE
WIDTH 6.3 AREA 2.705 VEL. 1.35 G.H. 0.47 DISCH. 3.13
METHOD 16 NO. SECS 40 each G.H. CHANGE +0.01 IN 1/2 HRS.

METER TYPE Surveyor's current Meter #625 No.
SPIN BEFORE MEAS. 31 AFTER 46
MEAS. PLOTS % DIFF. FROM RATING
WADING, UPSTR. (DOWNSTR.) SIDE BRIDGE NO. 44 (FEET) MILE, ABOVE, (BELOW) GAGE AND
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
FOLLOWING CONDITIONS: CROSS SECTION

FLOW non uniform, low WEATHER SUNNY 75°F SLIGHT BREEZE

OTHER AIR 75 °F@ 1045
GAGE STEVENS TYPE F, GAGE WATER HO OF@ 1045
NO RECORD REMOVED NO INTAKE FLUSHED L

OBSERVER PAUL WHITE, JULIE STEPHENS

CONTROL WEIR (CEMENT CONTROL STRUCTURE)
REMARKS Higher flow on right edge; measurement suspect as low flow will not turn meter consistently

G.H. OF ZERO FLOW FT

| GAGE READINGS | | | | |
|-----------------|----------|--------|---------|--|
| TIME | RECORDER | INSIDE | OUTSIDE | |
| 1037 | | 0.46 | 0.47 | |
| 1050 | START | 0.46 | 0.46 | |
| 1119 | | 0.47 | 0.47 | |
| 1128 | FINISH | 0.47 | 0.47 | |
| WEIGHTED M.G.H. | | | | |
| G.H. CORRECTION | | | | |
| CORRECT M.G.H. | | | | |

REW 7-6-89
222 4/21/89
1050
START
FINISH -
1128

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|-------|-------|-------------|-----------------|----------|--------|-----------|
| 7.8 | 0.5 | 0.05 | 0 | 40 | 0 | 0.025 | 0 |
| 6.8 | 1.0 | 0.20 | 0 | 40 | 0 | 0.200 | 0 |
| 5.8 | 0.8 | 0.42 | 0 | 40 | 0 | 0.336 | 0 |
| 5.4 | 0.4 | 0.62 | 0 | 40 | 0 | 0.248 | 0 |
| 5.0 | 0.4 | 0.60 | 0 | 40 | 0 | 0.240 | 0 |
| 4.8 | 0.5 | 0.60 | 7 | 40 | 1.75 | 0.300 | 0.525 |
| 4.4 | 0.4 | 0.61 | 7 | 40 | 1.75 | 0.244 | 0.427 |
| 4.0 | 0.4 | 0.62 | 7 | 40 | 1.75 | 0.248 | 0.434 |
| 3.6 | 0.4 | 0.65 | 7 | 40 | 1.75 | 0.260 | 0.455 |
| 3.2 | 0.4 | 0.63 | 7 | 40 | 1.75 | 0.252 | 0.441 |
| 2.8 | 0.4 | 0.55 | 8 | 40 | 2.00 | 0.220 | 0.440 |
| 2.4 | 0.35 | 0.42 | 11 | 40 | 2.75 | 0.147 | 0.40425 |
| 2.1 | 0.3 | 0.41 | 0 | 40 | 0 | 0.123 | 0 |
| 1.8 | 0.3 | 0.28 | 0 | 40 | 0 | 0.074 | 0 |
| 1.5 | 0.15 | 0.05 | 0 | 40 | 0 | 0.0075 | 0 |
| | | | | | 1.35 | 2.705 | 3.13 |

R. L. STOLLAR & ASSOCIATES

DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. 88
 COMPILED BY 88
 CHECKED BY 88
 STATION NAME NORTH 1ST CROSS (SW 24002)
 DATE 29/23 MAY 3 1989 PARTY PA JIC
 WIDTH 200MM FLOWING SECS NA AREA 0.52 DISCH. 0.79
 METHOD 200MM FLOWING VEL. 0 G.H. CHANGE 0 IN. 5 HRS.
 METER TYPE NA
 SPIN BEFORE MEAS. NA AFTER NA
 MEAS. PLOTS NA % DIFF. FROM NA RATING 30
 WADING, UPSTR. DOWNSTR. SIDE BRIDGE 30 FEET, MILE, ABOVE (BELOW) GAGE, AND
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION
 FLOW UNIFORM WEATHER SUNNY
 OTHER CLEAR AIR 60°F
 GAGE CLEAR WATER 50°F
 RECORD REMOVED NO INTAKE FLUSHED NO

CONTROL CLEAR
 REMARKS MEASURING Q w/TIME

G.H. OF ZERO FLOW _____ FT

| GAGE READINGS | | | |
|-----------------|---------|--------|---------|
| TIME | REORDER | INSIDE | OUTSIDE |
| 1005 | BEFORE | 0.52 | 0.52 |
| 1020 | DURING | 0.52 | 0.52 |
| 1025 | " | 0.52 | 0.52 |
| 1030 | " | 0.52 | 0.52 |
| WEIGHTED M.G.H. | | | |
| G.H. CORRECTION | | | |
| CORRECT M.G.H. | | | |
| | 0.52 | | 0.52 |

R. L. STOLLAR & ASSOCIATES DISCHARGE MEASUREMENT NOTES

MEASUREMENT NO. 10

COMPILED BY JK
CHECKED BY

STATION NAME NORTH FIRST CREEK B.S.
DATE 8/13/89 19 89 PARTY OK
WIDTH 3.9 AREA 1.986 VEL. 1.345 G.H. 0.92 DISCH. 3.3545

METHOD .6 NO. SECS 11 G.H. CHANGE IN HRS 34

METER TYPE GURLEY #625 PV6MW
SPIN BEFORE MEAS. 44 AFTER 43
MEAS. PLOTS 3 DIFF. FROM 1 RATING 57

WADING, UPSTR. DOWNSTR. SIDE BRIDGE FEET, MILE, ABOVE BELOW GAGE AND
MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%) BASED ON 11
FOLLOWING CONDITIONS: ROUGH SECTION

FLOW MOD - UNIFORM WEATHER COOL, CLOUDY

OTHER AIR 45° F @ 0950

GAGE STAFF - GOOD COND. WATER 45° F @ 0950

RECORD REMOVED NO INTAKE FLUSHED NO

OBSERVER

CONTROL CLEAR

REMARKS 20 HRS AFTER STORM

G.H. OF ZERO FLOW FT

| GAGE READINGS | | | | |
|-----------------|----------|--------|---------|--|
| TIME | RECORDED | INSIDE | OUTSIDE | |
| 0930 | BEFORE | 0.93 | 0.93 | |
| 1015 | " | 0.93 | 0.93 | |
| 1021 | START | 0.92 | 0.92 | |
| 1032 | MID | 0.92 | 0.92 | |
| 1041 | END | 0.92 | 0.92 | |
| WEIGHTED M.G.H. | | | | |
| G.H. CORRECTION | | | | |
| CORRECT M.G.H. | | | | |

| Distance from Initial Point | Width | Depth | Revolutions | Time in Seconds | Velocity | Area | Discharge |
|-----------------------------|-------|-------|-------------|-----------------|----------|-------|-----------|
| 3.0 | .15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3.3 | .30 | .33 | 70 | 40 | 1.75 | .099 | .173 |
| 3.6 | .30 | .52 | 66 | 40 | 1.65 | .156 | .257 |
| 3.9 | .30 | .63 | 67 | 40 | 1.675 | .189 | .317 |
| 4.2 | .30 | .63 | 50 | 40 | 1.25 | .189 | .236 |
| 4.5 | .30 | .63 | 52 | 40 | 1.30 | .189 | .246 |
| 4.8 | .30 | .61 | 49 | 40 | 1.225 | .183 | .224 |
| 5.1 | .30 | .60 | 83 | 40 | 2.075 | .180 | .374 |
| 5.4 | .30 | .67 | 154 | 40 | 3.35 | .201 | .673 |
| 5.7 | .30 | .73 | 99 | 40 | 2.475 | .219 | .542 |
| 6.0 | .30 | .60 | 50 | 40 | 1.25 | .180 | .225 |
| 6.3 | .30 | .42 | 14 | 40 | 0.35 | .126 | .044 |
| 6.6 | .30 | .25 | 19 | 40 | 0.475 | .1075 | .036 |
| 6.9 | .15 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | 1.345 | 1.986 | 3.397 |

MEASUREMENT NO.
COMPILED BY
CHECKED BY

STATION NAME FIRST CREEK - NORTH BOUNDARY - SW13404

DATE 89/14 4/24 1989 PARTY JK LB

WIDTH ~6.0 AREA _____ VEL. _____ G.H. NA DISCH. 1742

METHOD FLUME NO. SECS NA G.H. CHANGE NA IN 0 HRS.

METER TYPE N/A
 SPIN BEFORE MEAS. N/A AFTER N/A
 MEAS. PLOTS _____ % DIFF. FROM _____ RATING _____
 WADING, UPSTR., DOWNSTR., SIDE BRIDGE _____ FEET, MILE, ABOVE, BELOW GAGE, AND _____
 MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON
 FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW LOW / UNIFORM WEATHER COOL, CLOUDY
OTHER _____ AIR 65 °@ 1020
GAGE NONE INSTALLED WATER 55 °@ 1020
RECORD REMOVED _____ U
INTAKE FLUSHED L

OBSERVER

CONTROL

REMARKS FLOW NOT STEADY, BACKING UP DUE TO
SHALLOW BANKING STRUCTURE

G.H. OF ZERO FLOW _____ FT

[illegible]

R. L. STOLLAR & ASSOCIATES

COMPILED BY

CHECKED BY

STATION NAME 751 CREEK @ NORTH PLANTS (SW30002)

| DATE | WIDTH | AREA | VEI | PARTY | CHK, LB |
|---------|-------|------|-----|-------|---------|
| 59114 | 7/34 | | | 19 89 | |
| ~ 13 14 | | | | | |

| | | | | | | | |
|--------|---------------|---------|----|-----------|----|----|--------|
| 200 mm | FLYING | NO SECS | NA | GH CHANGE | NA | IN | DISCH. |
| width | LONG THROATED | | | | | | |
| area | 180 V 1 | | | | | | |
| VEL. | | | | | | | |
| U.H. | | | | | | | |

METER TYPE NA

SPIN BEFORE MEAS. NA AFTER NA RATING _____
MEAS. PLOTS _____ % DIFF. FROM _____

WADING, UPSTR., DOWNSTR., SIDE BRIDGE _____ FEET, MILE, ABOVE, BELOW GA. _____

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BAS
FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW-- UNIFORM WEATHER COOL, CLEAR, LT W.

OTHER _____ AIR . 60 1142 40

GAGE NONE INSTALLED WATER 50 OF @ 114 11

RECORD REMOVED NA INTAKE FLUSHED LA

OBSERVER

| CONTROL | REMARKS |
|---------|----------------------------------|
| | OFFENSIVE VEGETATION 10-15' HIGH |

| REMARKS | ACCU | ANY | LOCATION | 10-13 | VF | 13-14 |
|---------|------|-----|----------|-------|----|-------|
| | | | | | | |

G.H. OF ZERO FLOW

[illegible]

DISCHARGE MEASURED WITH BUCKET & TIMER. MEASURED JUST BEFORE WEIR.

COMPILED BY
CHECKED BY

36001

6499 DISCH.

G.H. CHANGE

NA

1

TING

3

CC

A

WATE

no

2

751:2011

1

CAGE READING

INIS 4 =

JK

FIRST CREEK OFF-POST (37001)

METER TYPE NA
SPIN BEFORE MEAS. NA AFTER NA RATING
MEAS. PLOTS _____ % DIFF. FROM _____
WADING, UPST., DOWNSTR., SIDE BRIDGE 40 FEET

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION

FLOW LOW- UNIFORM WEATHER COOL SL RAINY, LT WIND

OTHER _____

GAGE STAFF - 600 STAFF WATER 55° OF @ 1055

RECORD REMOVED _____ INTAKE FLUSHED L _____

OBSERVER _____

CONTROL

REMARKS

G.H. OF ZERO FLOW
FT

| GAGE READINGS | | | | |
|-----------------|--|----------|--------|---------|
| TIME | | RECORDER | INSIDE | OUTSIDE |
| 1045 | | 005 | | 0.61 |
| 1054 | | 005 | | 0.51 |
| 1059 | | 005 | | 0.55 |
| 1104 | | 005 | | 0.56 |
| 1109 | | 005 | | 0.57 |
| 1114 | | 005 | | 0.58 |
| WEIGHTED M.G.H. | | | | |
| G.H. CORRECTION | | | | |
| CORRECT M.G.H. | | | | |

FOPM31 / DEC 87

MEASUREMENT NO.
COMPILED BY
CHECKED BY

DATE 89/94 7/13 AREA 19 PARTY JK DISCH. 0.0753
WIDTH _____ VEL. _____ G.H. 6.58 IN 1/8 HRS.
METHOD 100 MM LT NO. SECS. MA G.H. CHANGE 0 (15)

METER TYPE NA
SPIN BEFORE MEAS. NA AFTER NA RATING _____
MEAS. PLOTS _____
WADING UPSTR. (DOWNSTR.) SIDE BRIDGE 10 FEET _____
_____ MILE, ABOVE, BELOW GAGE, AND _____

MEASUREMENT RATED EXCELLENT (2%), GOOD (5%), FAIR (8%), POOR (OVER 8%), BASED ON FOLLOWING CONDITIONS: CROSS SECTION _____

FLOW VERY LOW-UNIFORM WEATHER WARM, MOSTLY SUNNY
OTHER AIR 85 F@ 1545

GAGE INSIDE STAFF - GOOD COND WATER 65 °F @ 1545

RECORD REMOVED EARLIER INTAKE FLUSHED NO
10 DAY

| CONTROL | CEMENT FLUME |
|---------|--------------|
| 1 | 1 |
| 2 | 2 |
| 3 | 3 |
| 4 | 4 |
| 5 | 5 |
| 6 | 6 |
| 7 | 7 |
| 8 | 8 |
| 9 | 9 |
| 10 | 10 |
| 11 | 11 |
| 12 | 12 |
| 13 | 13 |
| 14 | 14 |
| 15 | 15 |
| 16 | 16 |
| 17 | 17 |
| 18 | 18 |
| 19 | 19 |
| 20 | 20 |
| 21 | 21 |
| 22 | 22 |
| 23 | 23 |
| 24 | 24 |
| 25 | 25 |
| 26 | 26 |
| 27 | 27 |
| 28 | 28 |
| 29 | 29 |
| 30 | 30 |
| 31 | 31 |
| 32 | 32 |
| 33 | 33 |
| 34 | 34 |
| 35 | 35 |
| 36 | 36 |
| 37 | 37 |
| 38 | 38 |
| 39 | 39 |
| 40 | 40 |
| 41 | 41 |
| 42 | 42 |
| 43 | 43 |
| 44 | 44 |
| 45 | 45 |
| 46 | 46 |
| 47 | 47 |
| 48 | 48 |
| 49 | 49 |
| 50 | 50 |
| 51 | 51 |
| 52 | 52 |
| 53 | 53 |
| 54 | 54 |
| 55 | 55 |
| 56 | 56 |
| 57 | 57 |
| 58 | 58 |
| 59 | 59 |
| 60 | 60 |
| 61 | 61 |
| 62 | 62 |
| 63 | 63 |
| 64 | 64 |
| 65 | 65 |
| 66 | 66 |
| 67 | 67 |
| 68 | 68 |
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| 70 | 70 |
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| 72 | 72 |
| 73 | 73 |
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| 76 | 76 |
| 77 | 77 |
| 78 | 78 |
| 79 | 79 |
| 80 | 80 |
| 81 | 81 |
| 82 | 82 |
| 83 | 83 |
| 84 | 84 |
| 85 | 85 |
| 86 | 86 |
| 87 | 87 |
| 88 | 88 |
| 89 | 89 |
| 90 | 90 |
| 91 | 91 |
| 92 | 92 |
| 93 | 93 |
| 94 | 94 |
| 95 | 95 |
| 96 | 96 |
| 97 | 97 |
| 98 | 98 |
| 99 | 99 |
| 100 | 100 |

REMARKS STRUCTURE IN GOOD COND

G.H. OF ZERO FLOW 0.50 FT

[illegible][illegible]

APPENDIX A-3

Rating Curves

APPENDIX A-3.1

Rating Curve Development Procedures

Appendix A-3.1 Rating Curve Development Procedures

Channel Control Rating Development. - The development of the rating curve for a channel control station would normally use a graphical analysis of discharge measurements plotted on logarithmic graph paper. Upon review of the discharge measurements, made prior to the 1989 water year, for the only channel control station, Havana Interceptor, all were rejected as unreliable for rating curve development. Therefore, the following analysis was performed to derive a rating curve for Havana Interceptor:

- A normal depth hydraulic analysis was performed using HEC-2 to predict gage height and corresponding discharges from channel geometry.
- The predicted discharges and gage heights were plotted on logarithmic paper. The discharge was on the ordinate and the gage height was on the abscissa.
- A curve of connected straight-line segments was visually fitted through the plotted points.
- Endpoint coordinates of each straight-line segment were determined from the rating curve plot. A rating equation was derived in the form of a power curve (Rantz 1982).

The rating equation was of the form

$$Q = pG^N$$

where

Q = discharge in cubic feet per second (cfs);

G = the gage height of the water surface in feet;

p = regression coefficient (dimensionless); and

N = regression coefficient (dimensionless), generally not equal to p.

Two different criteria were used to confirm the permanence and/or follow shifts in the rating curve for Havana Interceptor. These criteria are as follows:

- Instantaneous discharge measurements made during the 1989 water year must be within ± 5 percent of the rating curve discharge corresponding to the same gage height in order to confirm the permanence of the rating curve.
- For low-flow measurements, the ± 5 percent criteria may be too stringent because of station control insensitivity; therefore, departures greater than ± 5 percent are

acceptable and confirm the permanence of the rating curve if the indicated shift in stage does not exceed 0.02 feet.

A detailed analysis of each instantaneous discharge measurement made during the 1989 water year at this station is presented in Appendix A-5.

Section Control Rating Development. - Laboratory-rated discharge-measurement structures have been installed at seven RMA stations (Highline Lateral, Ladora Weir, Basin A, South First Creek, North First Creek, First Creek Off-post, and South Plants Ditch). These structures provide section control for the complete range of stages falling within the capacity of each structure. Each artificial control stabilizes and constricts the channel at a section, and thereby simplifies the procedure for obtaining accurate records of discharge. Although these structures have been built in conformance with the dimensions of laboratory-rated weirs or flumes (the relationship of stage to discharge has been carefully measured under controlled conditions) differences between the model and prototype invariably exist, if only in approach-channel conditions (Rantz 1982). Therefore, instantaneous discharge measurements were made at artificial section control stations to verify the rating curves prepared for the respective model structures.

It should be emphasized that the primary purpose of the weir structures, and the triangular-throated flume at the First Creek Off-post station, was to measure flows within the capacity of the structures. Therefore, no attempt was made to determine the relationship of stage to discharge for stages and flows exceeding the capacity of the artificial section controls.

The laboratory rating for each structure was plotted along with the discharge measurements to discharge if a correlation existed. These laboratory ratings are based on depth of water above the zero-reference of the structure. Since the field-measured staff gage heights do not generally equal the water depths above the zero-reference of the structures, an offset was subtracted from each staff gage height to obtain the plotted depth value. This offset (e) is the gage height (in feet) corresponding to zero flow for the existing control. If the discharge measurements consistently plotted on the empirical rating curve, the empirical curve was used. For stations at RMA requiring modification of the empirical ratings, the verified stage-discharge measurements were plotted, and connected straight-line segments were fit to the plotted points. Regression analysis to fit a power curve was performed as previously described (Channel Control Rating Development) to obtain a calibrated rating curve and rating equations for the existing condition of each structure. For the stations where zero on the staff gage does not correspond to zero flow, the rating equation will be of the form

$$Q = p(G-e)^N$$

where

$$Q = \text{discharge in cubic feet per second (cfs);}$$

- (G-e) = head or depth of water on the control in feet;
G = the gage height of the water surface in feet;
e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
p = regression coefficient (dimensionless); and
N = regression coefficient (dimensionless), generally not equal to p.

Confirmation of the permanence of these rating curves followed the same criteria as previously described in Section 3.1.2.6, Rating Curve Development Procedures; and in this Appendix, Channel Control Rating Development.

The development of the rating curve for South First Creek followed the normal graphical analysis of instantaneous discharge measurements. The reliable instantaneous discharge measurements were plotted on logarithmic graph paper with the discharge on the ordinate and the corresponding gage height on the abscissa. A curve of connected straight-line segments was visually fitted through the plotted points. Endpoint coordinates of each straight-line segment were determined from the rating curve plot. Regression analysis to fit a power curve was performed, as previously described (channel control rating development), to obtain a calibrated rating curve and equations for the existing condition of the structures. The rating curve required extrapolation beyond the range defined by discharge measurements for low flows. A table of gage height and discharge was generated by using the rating equation in the defined region for the lowest flows. These points were plotted on rectangular-coordinate graph paper along with the gage height of zero flow, and a smooth curve was drawn to merge the point of zero flow with the defined range of points (Rantz 1982). Several points from this extrapolated curve below the defined segment were transferred onto the logarithmic paper. Straight-line segments were connected between selected extrapolated points and equations were derived for the segments as previously described.

Upon review of the four instantaneous discharge measurements made at the North First Creek gaging station, only one was accepted as reliable for rating curve development. Therefore, the following analysis was performed to derive a rating curve for this station:

- A normal depth hydraulic analysis was performed using HEC-2 to predict gage height and corresponding discharges from channel geometry.
- The predicted discharges and gage heights were plotted on logarithmic graph paper, along with the one reliable discharge measurement.

- A curve of connected straight-line segments was visually fit through the plotted points.
- Endpoint coordinates of each straight-line segment were determined from the rating curve plot and regression analysis to fit a power curve, as previously described (channel control rating development).

A detailed analysis of each instantaneous discharge measurement made during the 1989 water year at each of these stations is presented in Appendix A-5.

Compound Control Rating Development. - The development of rating curves for the compound control stations (South Uvalda, North Uvalda, and Peoria Interceptor) utilized a procedure that was a combination of the procedures delineated in the previous two station control sections (section control and channel control). Additional considerations included the following:

- Discharge measurements were evaluated to determine if the measured discharges and corresponding staff readings could occur theoretically. This evaluation was conducted using HEC-2 to simulate the channel hydraulics. Discharge measurements that appeared invalid based upon the HEC-2 analysis were not used in the rating curve development.
- The rating curves required extrapolation beyond the range defined by discharge measurements for high flows. An analysis was performed using HEC-2 to determine if the transition from section control to channel control had occurred at the highest recorded stage. In all cases, this transition had not occurred. Further analysis demonstrated that it was inappropriate to use HEC-2 for the high flow extrapolation.

A hydraulic analysis using HEC-2 was attempted to predict the higher flows. (Note however, that these higher flows are section controlled.) This was done by assuming critical depth at the control section and that normal depth would then occur at the gage section. The present stations were constructed such that there is insufficient distance between the gage section and the control section. The result is that normal depth occurs upstream of the gage section, therefore, yielding an unrealistic result.

- The high flow extrapolation was done using the Manning equation:

$$Q = \frac{1.486}{n} AR^{2/3} S^{1/2}$$

where

Q = discharge (cfs);
n = Manning's channel roughness coefficient (dimensionless);
A = cross-sectional area (ft²);
R = hydraulic radius = $\frac{A}{P}$;
P = wetted perimeter (ft); and
S = slope (ft/ft).

The cross-section geometry corresponding to the maximum recorded gage height was plotted from reach survey data to determine the cross-sectional area and wetted perimeter at the location of the staff gage. The slope of the corresponding stream surface energy gradient was not available. Since average streambed slope typically approaches the energy gradient at the higher stages (Rantz 1982), the average streambed slope was computed from contour maps or reach survey data for input to Manning's equation. The channel roughness coefficient, n, was determined from stage-discharge measurements and field observations of streambed and bank cover conditions. The calculated discharge was plotted on logarithmic paper and regression analysis was performed on this line segment as previously described.

Confirmation of the permanence of these rating curves followed the same criteria as previously described. A detailed analysis of each instantaneous discharge measurement made during the 1989 water year at each of these stations is presented in Appendix A-5.

APPENDIX A-3.2

Gage Height vs. Discharge

APPENDIX A-3.3

Head vs. Discharge

APPENDIX A-4

Rating Equations

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW01001, NORTH UVALDA

DESCRIPTION: BROAD CRESTED CONCRETE WEIR

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| -0.104 to -0.060 | 0.882177764 | 1.444590283 | -0.105 | 10-01-88 | 09-30-89 |
| -0.059 to 0.000 | 1.597817538 | 1.636135791 | -0.105 | 10-01-88 | 09-30-89 |
| 0.001 - 0.015 | 0.118589583 | 0.205644337 | 0.00 | 10-01-88 | 09-30-89 |
| 0.016 - 0.03 | 0.184078048 | 0.310340083 | 0.00 | 10-01-88 | 09-30-89 |
| 0.04 - 0.05 | 0.356680281 | 0.498980945 | 0.00 | 10-01-88 | 09-30-89 |
| 0.06 - 0.09 | 0.631774902 | 0.689816811 | 0.00 | 10-01-88 | 09-30-89 |
| 0.10 - 0.15 | 2.323074133 | 1.230573848 | 0.00 | 10-01-88 | 09-30-89 |
| 0.16 - 0.20 | 5.667685192 | 1.700702010 | 0.00 | 10-01-88 | 09-30-89 |
| 0.21 - 0.515 | 12.65759878 | 2.199930256 | 0.00 | 10-01-88 | 09-30-89 |
| 0.516 - 0.975 | 14.63974813 | 2.419166422 | 0.00 | 10-01-88 | 09-30-89 |
| 0.976 - 2.00 | 14.95376940 | 3.257434047 | 0.00 | 10-01-88 | 09-30-89 |
| 2.01 - 2.54 | 45.64969387 | 1.647337806 | 0.00 | 10-01-88 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW01003, SOUTH PLANTS DITCH

DESCRIPTION: 90 DEGREE V-NOTCH WEIR PLATE

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 $(G-e)$ = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p .

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 3.43 - 3.62 | (1) | (1) | 3.43 | 10-01-88 | 09-30-89 |
| 3.63 - 3.80 | 2.488803337 | 2.481549685 | 3.43 | 10-01-88 | 09-30-89 |
| 3.80 - 5.43 (2) | 33.30000000 | 1.500000000 | 3.80 | 10-01-88 | 09-30-89 |

- (1) For gage heights between 3.43 ft and 3.62 ft which corresponds to heads of 0.00 ft and 0.19 ft, use the given coefficients for the gage height range of 3.63 ft - 3.80 ft. Note that the flow can only be estimated in the low-flow range due to the fact that the nappe may not spring free of the crest when the head is less than 0.2 ft.
- (2) For gage heights above 3.80 ft use the coefficients given to compute a flow. To this add 0.21 cfs, the maximum flow through the V-notch. Note that the flow can only be estimated in this range above 3.80 ft.

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW02001, LADORA WEIR

DESCRIPTION: 2-INCH-WIDE PLANKS FITTED ON TOP OF A CONCRETE WALL

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 $(G-e)$ = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p .

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 4.13 - 4.32 | (1) | (1) | 4.13 | 10-01-88 | 09-30-89 |
| 4.13 - 6.13 | 19.98000000 | 1.500000000 | 4.13 | 10-01-88 | 09-30-89 |

(1) For gage heights between 4.13 ft and 4.32 ft, which corresponds to heads of 0.0 ft and 0.19 ft, use the given coefficients for the gage height range of 4.33 ft - 6.13 ft. Note that the flow can only be estimated in the low-flow range due to the fact that the nappe may not spring free of the crest when the head is less than 0.2 ft.

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW08003, SOUTH FIRST CREEK

DESCRIPTION: CONCRETE COMPOUND WEIR

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.03 - 0.12 | 0.274865251 | 1.562869813 | 0.00 | 10-01-88 | 09-30-89 |
| 0.13 - 0.20 | 30.32336677 | 3.781175623 | 0.00 | 10-01-88 | 09-30-89 |
| 0.21 - 1.38 | 4.970971764 | 2.657613623 | 0.00 | 10-01-88 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW11001, PEORIA INTERCEPTOR

DESCRIPTION: FLAT CRESTED WEIR WHICH CONSISTS OF A NARROW PLANK POSITIONED PERPENDICULAR TO FLOW. CHANGED TO A 90 DEGREE V-NOTCH WEIR ON APRIL 14, 1989.

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|--------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 1.04 - 1.06 | 3.640718E-12 | 436.7207643 | 0.00 | 10-01-88 | 04-07-89 |
| 1.07 - 1.12 | 0.051158789 | 35.71755364 | 0.00 | 10-01-88 | 04-07-89 |
| 1.13 - 1.29 | 1.202206920 | 7.860705838 | 0.00 | 10-01-88 | 04-07-89 |
| 1.30 - 4.32 | 5.407527455 | 1.955820912 | 0.00 | 10-01-88 | 04-07-89 |
| 0.404 - 0.50 | 0.236237085 | 1.280211429 | 0.39 | 04-14-89 | 09-30-89 |
| 0.51 - 0.59 | 1.131299766 | 1.989813381 | 0.39 | 04-14-89 | 09-30-89 |
| 0.60 - 1.05 | 2.488803337 | 2.481549685 | 0.39 | 04-14-89 | 09-30-89 |
| 1.051 - 1.06 | 0.123984198 | 40.32966282 | 0.00 | 04-14-89 | 09-30-89 |
| 1.07 - 1.12 | 0.415469558 | 19.57665310 | 0.00 | 04-14-89 | 09-30-89 |
| 1.13 - 1.29 | 1.795908698 | 6.659737538 | 0.00 | 04-14-89 | 09-30-89 |
| 1.30 - 4.32 | 6.058487140 | 1.884610242 | 0.00 | 04-14-89 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW11002, HAVANA INTERCEPTOR

DESCRIPTION: CONCRETE LINED TRAPEZOIDAL CHANNEL

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.01 - 0.025 | 2.000000126 | 1.000000012 | 0.00 | 10-01-88 | 09-30-89 |
| 0.026 - 0.10 | 2.364864829 | 1.045426716 | 0.00 | 10-01-88 | 09-30-89 |
| 0.11 - 0.175 | 2.305695547 | 1.034422377 | 0.00 | 10-01-88 | 09-30-89 |
| 0.176 - 0.24 | 4.725356666 | 1.446111016 | 0.00 | 04-25-89 | 09-30-89 |
| 0.25 - 0.32 | 23.80114393 | 2.579018353 | 0.00 | 04-25-89 | 09-30-89 |
| 0.33 - 1.39 | 20.86833977 | 2.463609783 | 0.00 | 04-25-89 | 09-30-89 |
| 1.40 - 1.91 | 21.46649374 | 2.377791962 | 0.00 | 04-25-89 | 09-30-89 |
| 1.92 - 4.14 | 8.454697601 | 3.817702957 | 0.00 | 04-25-89 | 09-30-89 |
| 0.176 - 4.14 | 3.276612758 | 1.236048284 | 0.00 | 10-01-88 | 04-25-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW12005, SOUTH UVALDA

DESCRIPTION: V-NOTCH IN A 12 INCH WIDE CONCRETE WEIR

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|--------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 3.428 - 3.57 | 4.315263E-29 | 48.79427888 | 0.00 | 10-01-88 | 09-30-89 |
| 3.58 - 3.84 | 1.627457E-16 | 26.03831775 | 0.00 | 10-01-88 | 05-08-89 |
| 3.85 - 4.31 | 7.204057E-14 | 21.50994769 | 0.00 | 10-01-88 | 05-08-89 |
| 4.32 - 4.82 | 0.000700004 | 5.768606020 | 0.00 | 10-01-88 | 05-08-89 |
| 4.83 - 4.92 | 1.199150E-29 | 43.49109493 | 0.00 | 10-01-88 | 09-30-89 |
| 4.93 - 5.10 | 6.693750E-10 | 14.95383007 | 0.00 | 10-01-88 | 09-30-89 |
| 5.11 - 8.00 | 0.014836562 | 4.572277074 | 0.00 | 10-01-88 | 09-30-89 |
| 3.58 - 4.06 | 1.931987E-19 | 31.33173826 | 0.00 | 05-09-89 | 09-30-89 |
| 4.07 - 4.82 | 0.000653393 | 5.812418902 | 0.00 | 05-09-89 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW12007, HIGHLINE LATERAL

DESCRIPTION: CIPPOLETTI WEIR

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.01 - 0.04 | 5.999999825 | 0.999999995 | 0.00 | 10-01-88 | 09-30-89 |
| 0.05 - 0.09 | 11.77702045 | 1.209511252 | 0.00 | 10-01-88 | 09-30-89 |
| 0.10 - 0.20 | 15.97301939 | 1.336071751 | 0.00 | 10-01-88 | 09-30-89 |
| 0.21 - 0.33 | 26.14011331 | 1.642122716 | 0.00 | 10-01-88 | 09-30-89 |
| 0.34 - 1.00 | 54.66181761 | 2.307513945 | 0.00 | 10-01-88 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW24002, NORTH FIRST CREEK

DESCRIPTION: CONCRETE COMPOUND WEIR

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.084 - 0.25 | 4.547328047 | 2.470675002 | 0.00 | 10-01-88 | 09-30-89 |
| 0.26 - 1.24 | 3.522261553 | 2.286416481 | 0.00 | 10-01-88 | 09-30-89 |
| 1.25 - 1.70 | 3.174816454 | 2.769205688 | 0.00 | 10-01-88 | 09-30-89 |

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW36001, BASIN A

DESCRIPTION: 90 DEGREE V-NOTCH WEIR PLATE

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.07 - 0.26 | (1) | (1) | 0.07 | 10-01-88 | 09-30-89 |
| 0.27 - 1.32 | 2.488803337 | 2.481549685 | 0.07 | 10-01-88 | 09-30-89 |

(1) For gage heights between 0.07 ft and 0.26 ft which corresponds to heads of 0.0 ft and 0.19 ft use the given coefficients for the gage height range of 0.27 ft - 1.32 ft. Note that the flow can only be estimated in the low-flow range due to the fact that the nappe may not spring free of the crest when the head is less than 0.2 ft.

STAGE-DISCHARGE RATING EQUATIONS

STATION: SW37001, FIRST CREEK OFF POST

DESCRIPTION: CONCRETE TRIANGULAR-THROATED FLUME

EQUATION FORM: $Q = p(G-e)^N$

where: Q = Discharge in cubic feet per second;
 (G-e) = head or depth of water on the control in feet;
 G = the gage height of the water surface in feet;
 e = gage height in feet of zero flow for a section control of regular shape, or the gage height of effective zero flow for a channel control or a section control of irregular shape;
 p = regression coefficient (dimensionless); and
 N = regression coefficient (dimensionless), generally not equal to p.

| Gage Height, G, Range (ft) | p | N | e (ft) | Valid Period | |
|----------------------------------|-------------|-------------|-----------|--------------|----------|
| | | | | Begin Date | End Date |
| 0.50 - 0.54 | 0.124999989 | 0.999999979 | 0.50 | 06-15-89 | 09-30-89 |
| 0.55 - 0.59 | 1.226773025 | 1.709511275 | 0.50 | 06-15-89 | 09-30-89 |
| 0.60 - 0.75 | 4.306533142 | 2.231012279 | 0.50 | 06-15-89 | 09-30-89 |
| 0.76 - 2.50 | 6.853180828 | 2.566146561 | 0.50 | 06-15-89 | 09-30-89 |

APPENDIX A-5

Comparison of Instantaneous Discharge
Versus Computed Discharge

[illegible][illegible]

[illegible][illegible]

[illegible][illegible]

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
SOUTH FIRST CREEK (SW08003)

| (1) Meas- urement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Start, Stop Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instan- taneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8) = 100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10) = (4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|-----------------------------------|-------------|-------------------------------------|---|---|---|---------------------------------------|---|--------------------------------------|---|--|--|
| 1 | 04/07/89 | 1130,1205 | 0.49 | --- | 0.59 | 0.75 | -21.3 | 0.45 | 0.04 | | RLSA, Pygmy #625, downstream 25' |
| 2 | 04/12/89 | 1536,1647 | 0.58 | --- | 1.1 | 1.1 | 0.0 | 0.57 | 0.01 | X | RLSA, Pygmy #625, downstream 45' below gage |
| 3 | 04/25/89 | 1000,1042 | 0.47 | --- | 0.72 | 0.67 | 7.5 | 0.48 | -0.01 | X | RLSA, 200mm flume, downstream 40' below gage |
| 4 | 05/03/89 | 0915,0935 | 0.50 | --- | 0.86 | 0.79 | 8.9 | 0.52 | -0.02 | X | RLSA, 200mm flume, downstream 40' below gage |
| 5 | 05/05/89 | 1020,1110 | 1.23 | --- | 9.2 | 8.6 | 7.0 | 1.26 | -0.03 | X | RLSA, Pygmy #625, downstream 40' below gage |
| 6 | 06/20/89 | 1228,1245 | 0.48 | --- | 0.69 | 0.71 | -2.8 | 0.48 | 0.00 | X | RLSA, 200mm flume, downstream 30' below gage |
| 7 | 07/20/89 | 1335,1343 | 0.13 | --- | 0.01 | 0.01 | 0.0 | 0.12 | 0.01 | X | RLSA, 100mm flume, downstream 30' below gage |
| 8 | 09/26/89 | 1440,1450 | 0.22 | --- | 0.10 | 0.09 | 11.1 | 0.23 | -0.01 | X | RLSA, 100mm flume, downstream 30' below weir |
| 9 | 09/29/89 | 1235,1246 | 0.20 | --- | 0.06 | 0.07 | -14.3 | 0.19 | 0.01 | X | RLSA, 100mm flume, downstream 30' below weir |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
PEORIA INTERCEPTOR (SW11001)

| (1) Meas- urement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instan- taneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8)=100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10)=(4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|-----------------------------------|-------------|-------------------------------------|--|---|---|---------------------------------------|---|--------------------------------------|---|--|--|
| 1 | 04/26/89 | 1116,1125 | 0.72 | --- | 0.13 | 0.16 | -18.8 | 0.30 | 0.03 | | RLSA, Long throated flume, downstream 30' below gage |
| 2 | 07/20/89 | 1710,1727 | 0.69 | --- | 0.16 | 0.13 | 23.1 | 0.33 | -0.03 | | RLSA, 200mm flume, downstream 30' below gage |
| 3 | 09/27/89 | 0845,0900 | 0.70 | --- | 0.05 | 0.14 | -64.3 | 0.21 | 0.10 | | RLSA, 100mm flume, downstream 100' below gage |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
HAVANA INTERCEPTOR (SW11002)

| (1) Meas- urement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Start, Stop Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instan- taneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8) = 100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10) = (4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|-----------------------------------|-------------|-------------------------------------|---|---|---|---------------------------------------|---|--------------------------------------|---|--|---|
| 1 | 04/11/89 | 1515,1545 | 0.52 | N/A | 1.5 | N/A | N/A | N/A | N/A | | RLSA, Pygmy #625, downstream 8' below bubble line |
| 2 | 04/26/89 | 1330 | 0.24** | 0.29 | 0.37 | 0.60 | -38.3 | 0.17 | 0.07 | | RLSA, Pygmy #625, 10' above gage |
| 3 | 07/20/89 | 1630,1655 | 0.18** | 0.23 | 0.37 | 0.40 | -7.5 | 0.17 | 0.01 | X | RLSA, 200mm flume, downstream 350' below gage |
| 4 | 09/27/89 | 1020,1030 | 0.19** | 0.24 | 0.49 | 0.43 | 14.0 | 0.21 | -0.02 | X | RLSA, 200mm flume, downstream 500' below gage |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

** Computed by (New Gage - 0.05 offset)

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
SOUTH UVALDA (SW12005)

| (1) Meas- urement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Start, Stop Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instan- taneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8) = 100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10) = (4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|-----------------------------------|-------------|-------------------------------------|---|---|---|---------------------------------------|---|--------------------------------------|---|--|--|
| 1 | 03/21/89 | 1520,1547 | 3.85,3.85 | --- | 0.26 | 0.28 | -7.1 | 3.84 | 0.01 | X | RLSA, Pygmy #625, downstream 50' below gage |
| 2 | 03/21/89 | 1544,1613 | 3.85,3.85 | --- | 0.30 | 0.28 | 7.1 | 3.85 | 0.00 | X | RLSA, Pygmy #625, downstream 50' below gage |
| 3 | 04/17/89 | 1203,1331 | 3.82,3.81 | --- | 0.35 | 0.22 | 59.1 | 3.88 | -0.06 | | RLSA, Pygmy #625, downstream 50' below gage |
| 4 | 04/21/89 | 1525,1535 | 3.84,3.84 | --- | 0.26 | 0.27 | -3.7 | 3.84 | 0.00 | X | RLSA, Long throated flume, downstream 30' below gage |
| 5 | 06/20/89 | 1330,1349 | 3.88,3.88 | --- | 0.54 | 0.54 | 0.0 | 3.88 | 0.00 | X | RLSA, 200mm flume, downstream 40' below gage |
| 6 | 09/26/89 | 0910,0920 | 3.83** | 0.51 | 0.30 | 0.36 | -16.7 | 3.81 | 0.02 | X | RLSA, 200mm flume, downstream 30' below gage |
| 7 | 09/29/89 | 1515,1515 | 3.82** | 0.50 | 0.17 | 0.33 | -48.5 | 3.74 | 0.08 | | RLSA, 200mm flume, downstream 50' below gage |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

** Computed by (New Gage + 3.32 offset)

[illegible][illegible]

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
NORTH FIRST CREEK (SW24002)

| (1) Meas- urement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Start, Stop Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instan- taneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8) = 100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10)=(4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|-----------------------------------|-------------|-------------------------------------|---|---|---|---------------------------------------|---|--------------------------------------|---|--|--|
| 1 | 04/06/89 | 1510,1530 | 0.47,0.47 | --- | 0.32 | 0.63 | -49.2 | 0.35 | 0.12 | | RLSA, Pygmy #625, downstream 40' below gage |
| 2 | 04/21/89 | 1056,1128 | 0.46,0.47 | --- | 0.31 | 0.60 | -48.3 | 0.35 | 0.11 | | RLSA, Pygmy #625, downstream 35' below gage |
| 3 | 05/03/89 | 1005,1030 | 0.52,0.52 | --- | 0.79 | 0.79 | 0.00 | 0.52 | 0.00 | X | RLSA, 200mm flume, downstream 30' below gage |
| 4 | 05/15/89 | 0930,1041 | 0.93,0.92 | --- | 3.4 | 3.0 | 13.3 | 0.98 | -0.05 | | RLSA, Pygmy #625, downstream 30' below gage |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

[illegible][illegible]

COMPARISON OF INSTANTANEOUS DISCHARGE VERSUS COMPUTED DISCHARGE *
FIRST CREEK OFF-POST (SW37001)

| (1) Measurement Number | (2) Date | (3) Start, Stop Time (hrs) | (4) Old Start, Stop Gage Height (feet) | (5) New Start, Stop Gage Height (feet) | (6) Instantaneous Discharge (cfs) | (7) Computed Discharge (cfs) | (8) = 100* [(6)-(7)]/(7) Difference in Discharge (%) | (9) Computed Gage ht. (ft.) | (10) = (4)-(9) Difference in Gage ht. (ft.) | (11) Measurements used for Rating Curve Development | (12) Comments |
|------------------------------|-------------|-------------------------------------|---|---|--|---------------------------------------|---|--------------------------------------|---|--|--|
| 1 | 04/07/89 | 1435,1453 | 0.51 | -- | 0.29 | N/A | N/A | N/A | N/A | | RSLA, Pygmy #625, upstream 40' above gage |
| 2 | 04/20/89 | 1648,1714 | 0.52 | -- | 0.31 | N/A | N/A | N/A | N/A | | RSLA, Pygmy #625, upstream 30' above gage |
| 3 | 05/03/89 | 1045,1114 | 0.61,0.58 | -- | 0.54 | N/A | N/A | N/A | N/A | | RLSA, 200mm flume, upstream 40' above gage |
| 4 ** | 07/13/89 | 1546,1550 | -- | 0.58 | 0.02 | 0.02 | 0.0 | 0.09 | -- | X | RLSA, 100mm flume, downstream 10' below gage |

* Computed discharge and computed gage height were obtained from rating curves and do not necessarily represent gage height output produced from strip charts.

** New control structure installed June 1989.

APPENDIX A-6

Continuous Gage Height Recorders
Equipment and Procedures

APPENDIX A-6.1

Stevens Type F Equipment Specifications
and Procedures

A-6.1 Stevens Type F Recorder Procedures

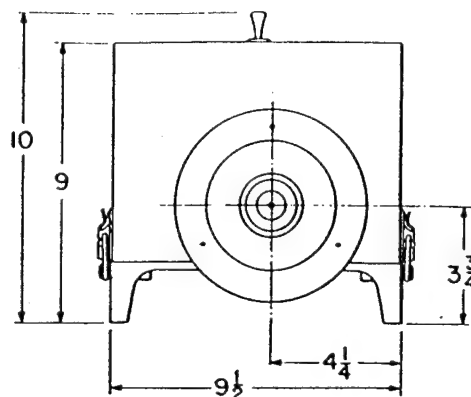
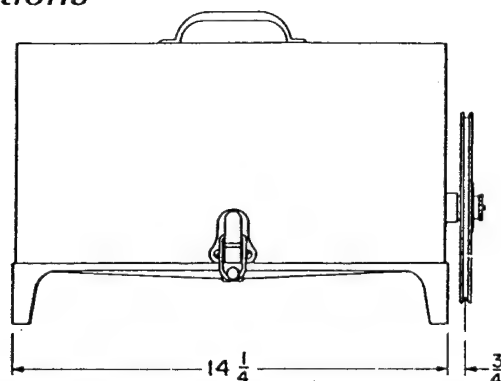
During Water Year 1989 there were eleven surface water stations equipped with Stevens Type F water level recorders. The Stevens Type F recorders currently in use are Model 68's equipped with quartz multispeed timers and either multiple D-cell batteries or a single mercury battery power source. The Stevens Type F recorder is attached to a float, beaded wire, and pulley. Changing water levels in the stilling well cause the float to rise and fall which turns the recorder's drum proportionally. The quartz multispeed timer moves a pen across the strip chart at a uniform speed. The resulting record produced is a graph of water level versus time.

Weekly activities at the continuous monitoring stations included collecting and replacing strip charts, checking recorder operation, calibrating strip charts to the outside observed stage and initial time, and removing obstructions from stilling wells, channel sections and control structures. Freezing conditions prohibited the use of the recorders from late November 1988 through February 1989. Stage data is invalid during periods of freezing because the frozen water in the stilling well incapacitates the recorder's float and pulley system.

The strip chart analog stage data were reduced to a digitized format using the computer program CPSPC (Radian Corp., October 1987, Version 3.1) in conjunction with a digitizer. After a strip chart has been digitized, the software program transforms the digital file into units used by the analog record. In this case, the scale was correlated to Julian date and scientific hours for time and to 0.01 ft for gage height. The minimal digitized strip chart points chosen were 0.00, 12.00, and 24.00 for each record day. Other significant stage points selected for digitization were high flow events, when gage heights were digitized at a minimum of 15 minute intervals, and any stage points that exhibited 0.1+ ft of deflection within any 2 hour period. Finally, the digitized stage output was compared to the strip chart analog record and corrected to the observed staff gage settings.

STEVENS TYPE F Water-level Recorder

Specifications



GAGE SCALES ADAPT RECORDER TO WATER-LEVEL RANGE

The relationship between the rotation of the float pulley and the chart drum is set by gearing. Changes in the gearing, or the pulley circumference, thus affect the ratio between the chart record and water-level changes. This ratio is known as *gage scale*.

To make a field change from any scale listed in the Table, below, (except 1:20 and 1:24) to another, requires only the substitution of a pair of gears. The 1:20 and 1:24 scales are obtained by installing the 750 mm. or 36 in. circumference ring on the float pulley of a Recorder geared for the 1:10 or 1:12 scales, respectively.

Table 3
GAGE SCALES FOR STEVENS TYPE F RECORDER
(obtained by gearing)

| Gage Scale | Water Level Change for 1 Rev. of Drum | Value of Smallest Chart Division | Float Pulley Required |
|------------------------------------|---|--|--------------------------|
| English Decimal System— | | | |
| | | F1/F2 F3 Chart | |
| 1:1 | 1.0 ft. | .01 ft. .1 in. | 18 in. circ. |
| 1:2 | 2.0 ft. | .02 ft. .2 in. | 18 in. circ. |
| 1:5 | 5.0 ft. | .05 ft. .5 in. | 18 in. circ. |
| 1:10 | 10.0 ft. | .10 ft. 1.0 in. | 18 in. circ. |
| 1:20 | 20.0 ft. | .20 ft. 2.0 in. | 36 in. circ. |
| English Duo-Decimal System— | | | |
| | | F3 Chart | |
| 10:12 | 1.2 ft. | .01 ft. | 18 in. circ. |
| 5:12 | 2.4 ft. | .02 ft. | 18 in. circ. |
| 1:6 | 6.0 ft. | .05 ft. | 18 in. circ. |
| 1:12 | 12.0 ft. | .10 ft. | 18 in. circ. |
| 1:24 | 24.0 ft. | .20 ft. | 36 in. circ. |
| Metric System— | | | |
| | | F4 Chart | |
| 1:1 | 0.3 m. | 2 mm. | 375 mm. circ. |
| 1:2 | 0.6 m. | 4 mm. | 375 mm. circ. |
| 1:5 | 1.5 m. | 10 mm. | 375 mm. circ. |
| 1:10 | 3.0 m. | 20 mm. | 375 mm. circ. |
| 1:20 | 6.0 m. | 40 mm. | 750 mm. circ. |

NOTE: Range is unlimited since the chart drum may make any number of revolutions.

Leupold & Stevens, Inc.

P.O. Box 688

Tel. 503 646-9171

Beaverton, Oregon 97005 U.S.A. • Cable LEUSTEV, Beaverton.

Basic Type F Recorder Specifications

Float operated water level recorder with horizontal ball bearing chart drum; rectangular chart 12 inches (or 30 cm) x 9.6 inches; capillary pen with Lucite reservoir; 1 oz. black ink; 4 legged cast aluminum base for shelf or table mounting; metal cover without port.

APPLICATION OPTIONS:

Type of pen drive:

- ☐ 8 day spring driven clock
- ☐ 30 day weight driven clock
- ☐ synchronous motor for ___V, ___Hz
- ☐ battery driven clock, 1.5 VDC

Time scale:

_____ (refer to Table 1 for availability)

Gage scale:

_____ (refer to Table 3 for availability)

Chart:

- ☐ F1 ☐ F3 ☐ F7
- ☐ F2 ☐ F4 ☐ F8

Float Pulley:

- ☐ 18 in. or 375 mm circumference for
- ☐ beaded float line ☐ perforated tape
- ☐ 36 in. or 750 mm pulley ring for 1:20 and 1:24 gage scales

Float line/ tape:

- ☐ _____ feet stainless steel float line with set end hooks
- ☐ _____ feet stainless steel perforated and graduated float tape with set end hooks and index bracket

Float with counterweight:

- ☐ 2 1/2 in. ☐ 5 in.
- ☐ 3 in. ☐ 6 in.
- ☐ 3 1/2 in. ☐ 7 in.
- ☐ 4 in. ☐ 8 in.

Accessories:

- ☐ Scow float with adjustable anchor rod and counterweight
- ☐ Automatic clock starter (for 8 day clock only)
- ☐ Cover with viewing port
- ☐ Pencil stylus (in place of pen)

Note: See Price List for options available. Manufacturer reserves the right to make changes in design or materials for product improvement, without notice.

APPENDIX A-6.2

Datapod Equipment Specifications and Procedures

The Omnidata International, Inc. model DP115 datapod, equipped with a 10-turn potentiometer, operates in conjunction with the Stevens Type F recorder. Data collected by the DP115 is used to obtain digital stage measurements in conjunction with the Stevens recorder.

Proper setup of the DP115 datapod requires that two recording functions are set:

- Resolution (stage change required to record a data point); and
- Sampling time interval.

The recording functions are set on the datapod using the control switches located on the inside panel. Switches 1 and 2 control resolution, and switches 3 and 4 control sampling interval. A resolution of 0.01 ft and a sampling interval of 30 minutes is set on the data pod. The datapod will record a change in stage of 0.01 ft or greater at 30 minute intervals; however, if the stage change is less than 0.01 ft the datapod does not record a data point. This function allows the datapod to conserve space on the data storage module (DSM). A stage data point is also recorded when the unit is powered up and will record a data point at 24 hour intervals regardless of any change in stage.

The datapod's DSM is changed monthly along with the units batteries. Data "short dumps" are acquired weekly and recorded in the log book. The following procedures are used to acquire the "short dump" and to change the DSM and batteries on the datapod.

Procedure:

Note: ** indicates that a display has to be recorded in the log book.

[] indicates a display that will appear on the DP115.

1. **RECORD station number in the log book.
2. **RECORD the DP115 serial number on the log book.
3. **RECORD the display message [RUN] in the log book: Display.
4. Loosen the four screws on the face plate and separate the face plate from the case. (do not remove screws if only a short dump is being acquired.)

SHORT DUMP

Note: The DP115 will advance through the following sequence fairly quickly. If a display is missed, the sequence can be reinitiated by pressing the button on the outer case after the last display [RUN] is shown.

5. Push the button on the outer case -
 - [DLY] will be displayed, then -
 - [CHN1] will be displayed, then -
 - a number will be displayed indicating the current stream stage.
 - **RECORD** the number with the label: CHN1
 - [ERR] will be displayed, then -
 - a number indicating the number of errors will be displayed.
 - **RECORD** this number with the label: ERR
 - [TIME] will be displayed, then -
 - a number indicating the time (relative to startup) will be displayed.
 - **RECORD** this number with the label: TIME
 - [DSM USED] will be displayed, then -
 - a number will be displayed indicating the amount of data storage modules space so far.
 - **RECORD** this number with the label: DSM USED
 - [RUN] will be displayed indicating the DP115 is finished with the short dump.

Note: continue procedures only if DSM and batteries are to removed.

Caution: There is a 24- hour clock in the DP115 that displays time to the nearest tenth hour.

Example: When the [TIME] display reads XXX.1, the DP115 has advanced 6 minutes into the hour.

The DP115 clock begins as soon as the last battery is inserted.

The DP115 is set to make a stream gage recording every 30 minutes. A 30 minute interval will be denoted on the [TIME] display as XXX.0 or XXX.5. If it is getting close to a recording interval such as XXX.4 or XXX.9, wait until after the reading has been make and then continue. (The LED will flash when a reading is being taken.)

6. Remove a battery from the battery pack to power down the DP115.
7. ****RECORD** the time of day with the label: Stop Time.
8. ****RECORD** the staff gage reading with the label: Staff Gage (ft).

Caution: Be sure your fingers are clean and dry before touching the DSM. Care should be taken no to touch any of the pins on the DSM.

9. Remove the DSM from the back of the face plate by gently pulling it straight up and place it in the protective container with the pins on the DSM inserted into the anti-static foam in the plastic storage container.

POWER UP

10. Replace the battery removed (or replace all batteries) to power up the DP115.
11. [DATA POD 115] will appear in the display window, then -
12. [SAM] will appear in the display window, then -
a number indicating the sample interval.
****RECORD** this number with the label: SAM.
13. [RES] will appear in the display window, then -
a number indicating the deviation from straight-line resolution.
****RECORD** this number with the label: RES
14. [DLY] will appear in the display window, then -
15. [CHN1] will appear in the display window, then -
a number indicating the sensor test for Channel 1.
****RECORD** this number with the label: CHN1.
16. Push in and hold the external button until [PLUG IN DSM PUSH] appears in the display window, then -
17. Insert a new DSM in the DP115.
****RECORD** the DSM number with the label: DSM#IN
Note: If either test fails, remove a battery, replace the DSM with another one and start the procedure again from "Power Up".
23. If both tests pass:
****RECORD** the time of day with the label: Start Time.
****RECORD** the staff gage height with the label: Staff Gage (ft).
24. [RUN] should then be displayed in the display window.
****RECORD** RUN with the label: DISPLAY
25. Replace the face plate on the case and tighten the 4 screws.

The DSM containing data is read with an Omnidata Model 217 Reader. The DSM Reader transmits the data from the DSM to a computer file where it can be further reduced to a stream stage record.

DPI15 DATAPOD SPECIFICATIONS

FUNCTION:

Single channel stream stage recorder.

TYPE OF SENSORS:

10-turn potentiometer. 5,000 to 100,000 Ohm resistance.

RESOLUTION:

0.01 foot in 10 feet of water.

RECORDING FUNCTIONS:

Records time of change and amount of change in water level.

SAMPLING INTERVALS:

User sets the time of day.

INPUT CONNECTOR:

3-pin environmentally sealed.

DATA STORAGE:

Medium: Non-volatile, interchangeable memory module.

Retrieval: Via built-in display or Model 217 Reader.

OPERATING CONTROLS AND DISPLAY:

Display: 4 1/2 digit LCD with low battery indicator.

Push Button: control data display and retrieval.

CLOCK ACCURACY:

+/- 3 minutes per month (-10C to + 60C).

SELF TEST:

Performs self test functions on power-up.

OPERATING ENVIRONMENT:

-35 deg C to + 60 deg C, 0 to 100% RH, dust and water tight.

POWER:

8 alkaline AA penlight cells.

SIZE AND WEIGHT:

6.3" x 3.3" x 2.3", 1.2 lb.

APPENDIX A-6.3

Data Logger Equipment
Specifications and Procedures

Data Logger/Bubbler System Procedures

Four Campbell Scientific CR-10 data logger/bubbler systems were put into operation at RMA during WY89. The CR-10 data logger/bubbler system provides stream stage data throughout the year including periods of freezing conditions.

Customized software was developed to operate the data logger and associated bubbler system. The data logger/bubbler system software controls several functions:

- operating the system on a specified uniform time interval;
- performing the calibration calculations; and
- storing the data in the RAM pack storage module.

This software can be loaded either by the use of the hand-held display or by transferring the program from a PC compatible computer to the unit's RAM pack storage module, then down loading the program from the RAM pack into the data logger. The time interval between the start of each measurement cycle is user-selectable and may range from 20 seconds to 6554 seconds. The measurement cycle interval used during WY89 was 900 seconds (15 minutes). Calibration of the data logger/bubbler system is based on two different pressure measurements made at a known distance apart in a reference cylinder located in each station's gage house. The software residing in the data logger performs the calibration calculation prior to each measurement cycle. During the routine monthly maintenance, the calibration is checked using the station's staff gage reading as a reference point, so that the accuracy of each measurement can be verified.

Data are retrieved from the from the RAM pack storage module using either SMCOM or PC208 software. Both SMCOM and PC208 are available from Campbell Scientific, Inc. These communication software programs run on PC compatible computers, additionally, the PC208 software also serves as a simple data formatting and programming tool for the data logger.

Various field operating procedures were used during WY89 for proper and continual operation of CR-10 data logger/bubbler system stations. They are as follows:

1. Reading and Recording the Current Datalogger Output

This procedure is performed during each weekly station visit. Each CR-10 is equipped with a hand help keypad and display. The following key entries denote specific display readouts. Output from the keypad's display is recorded in the field log book and a data sheet that is kept in the gage house. Additionally, nitrogen tank pressure, staff gage reading, and flow condition are recorded in the log book and data sheet.

- *5 - (Real Time)
 - A - The Current Year
 - A - The Julian Day
 - A - The Time - Mountain Standard
- *6 - (Field Data)
 - A
 - #1 - Head above tube in stream.
 - A
 - #2 - Depth in reference tube above top line.
 - A
 - #3 - Ambient Temp. - °C
 - A
 - #4 - Reference differential - distance between lines in reference tube - (approx. 1 ft - 1.0).
 - A
 - #5 - Battery voltage - should be above 12 v.
 - A
 - #6 (with Isco sampler), 0.01 = sample taken, 0.00 = no sample.
 - #20 and #21 - Time sample(s) taken.
 - #20 - XXXX divide by 24 and add 1 = (day sample taken).
 - #21 - minutes + #20 = (actual time sample taken).

2. Changing Batteries

The CR-10 data logger/bubbler system is powered by an industrial 12-volt, 15 amp-hour, sealed lead-acid battery. When the voltage falls below 12 volts, the battery is changed. The battery could be damaged if it is left in the field when the voltage drops below 12 volts. This is especially critical in the cold winter months.

The CR-10 has an internal battery pack consisting of eight alkaline D-cell batteries, that can be used as a back-up for the primary power supply. The following procedure is used to keep power applied to the unit while the external battery is being changed:

1. Insert the one D-cell battery back into the internal battery pack.
2. Disconnect the leads from the discharged external battery.
3. Connect a charged external battery.
4. Remove the D-cell battery from the internal battery pack.

3. Changing Nitrogen Tanks

Industrial nitrogen is supplied to the bubbler from a standard 2,200 psi nitrogen tank. The tank is equipped with a low pressure regulator to maintain a constant flow of 9 psi to the bubbler. The pressure to the bubbler can be changed by using the T-handle on the regulator. The regulator also has a gauge that indicates the pressure of nitrogen in the tank. When the tank pressure drops to approximately 500 psi, it is replaced with a full one. The following procedure is used to change the nitrogen tank:

1. With hand-held display, check *5 mode time to be sure that the instrument is not about to sample.
2. Close the valve on the top of the nitrogen tank.
3. With a 7/8" wrench, unscrew the flare nut on the regulator from the nitrogen tank orifice.
4. Unhook the safety chain and remove the empty tank from the shelter.
5. Place a full tank in the shelter and fasten the safety chain around it.
6. Place the regulator on the full tank and tighten the flare nut.
Note: Slightly wiggling the regulator while tightening the flare nut will help ensure a tight fit to the mating fitting on tank.
7. Open the valve at the top of the bottle. The pressure to the bubbler should read 9 psi.
8. Check for leaks around the regulator flare nut and tank orifice. After the regulator is attached to the new tank, open the T-handle until 0 psi is read on low pressure gage. Observe the tank pressure gauge to determine if any pressure is lost (15 minutes should be adequate). If the pressure drops, there is a leak in the connection. If a leak is detected, close the valve on top of the tank and remove the regulator. Place the regulator in a different position on the orifice and retighten the flare nut. Repeat the procedure to check for leaks.

SPECIFICATIONS

The following electrical specifications are valid for an ambient temperature range of -25°C to $+50^{\circ}\text{C}$ unless otherwise specified.

ANALOG INPUTS

NUMBER OF CHANNELS: 12 single ended or 6 differential with any combination, software selectable.

CHANNEL EXPANSION: Increments of 32 channels multiplexed through a single CR10 channel with the Model AM32 Relay Scanner. Maximum of 6 AM32's possible.

ACCURACY OF VOLTAGE MEASUREMENTS AND ANALOG OUTPUT VOLTAGES:
0.2% of FSR, 0.1% of FSR (0 to 40°C).

RANGE AND RESOLUTION: Ranges are software selectable for any channel. Resolution for single ended measurements is twice the value shown.

| Full Scale Range | Resolution |
|-----------------------|-----------------|
| ± 2.50 volts | 333. microvolts |
| ± 0.25 volts | 33.3 microvolts |
| ± 25.0 millivolts | 3.33 microvolts |
| ± 7.5 millivolts | 1.00 microvolts |
| ± 2.5 millivolts | 0.33 microvolts |

INPUT SAMPLE RATES: The fast or slow A/D conversion on the four lowest input ranges uses a 250 μs or 2.72 ms signal integration time, respectively. Two integrations, separated in time by $\frac{1}{2}$ of an AC line cycle, are used with the 60 Hz or 50 Hz noise rejection option. Differential measurements include a second sampling with reversed input polarity to reduce thermal offset and common mode errors. Input sample rates are the time required to measure and convert the result to engineering units.

| | |
|----------------------------|---------|
| Fast single ended voltage: | 2.6 ms |
| Fast differential voltage: | 4.2 ms |
| Slow single ended voltage: | 5.1 ms |
| Slow differential voltage: | 9.2 ms |
| Diff. w/60 Hz rejection: | 25.9 ms |
| Fast diff. thermocouple: | 8.6 ms |

INPUT NOISE VOLTAGE:

| | |
|-------------------------|-----------------------|
| Fast differential | — 0.82 microvolts RMS |
| Slow differential | — 0.25 microvolts RMS |
| Diff. w/60 Hz rejection | — 0.18 microvolts RMS |

COMMON MODE RANGE: ± 2.5 volts.

DC COMMON MODE REJECTION: >140 dB.

NORMAL MODE REJECTION: 70 dB (60 Hz with slow differential measurement).

INPUT CURRENT: 3 nanoamps max.

INPUT RESISTANCE: 200 gigohms.

EXCITATION OUTPUTS

DESCRIPTION: The CR10 has 3 switched excitations, active only during measurement, with only one output active at any time. The off state is high impedance.

RANGE: ± 2.5 volts.

RESOLUTION: 0.67 millivolts.

ACCURACY: Same as voltage input.

OUTPUT CURRENT: 20 mA @ ± 2.5 V, 35 mA @ ± 2.0 V, 50 mA @ ± 1.5 V.

FREQUENCY SWEEP FUNCTION: A swept frequency square wave output between 0 and 2.5 volts is provided for vibrating wire transducers. Timing and frequency range are specified by the instruction.

PERIOD AVERAGING MEASUREMENTS

DEFINITION: The time period for a specified number of cycles of an input frequency is measured, then divided by the number of cycles to obtain the average period of a single cycle.

INPUTS: Any single ended analog channel; signal dividing or AC coupling is normally required.

INPUT FREQUENCY RANGE:

| Range Code | Preamp Gain | Input Hysteresis | Maximum Frequency |
|------------|-------------|-------------------|-------------------|
| 4 | 1 | 10 mV | 200 kHz |
| 3 | 10 | 1 mV | 50 kHz |
| 2 | 33 | 300 μV | 20 kHz |
| 1 | 100 | 100 μV | 8 kHz |

REFERENCE ACCURACY: ± 40 ppm.

RESOLUTION: ± 100 nanoseconds divided by the number of cycles measured. Resolution is reduced by signal noise and for signals with a slow transition through the zero voltage threshold.

TIME REQUIRED FOR MEASUREMENT: Signal period times the number of cycles measured plus 1.5 cycles; minimum measurement time is 2 ms.

RESISTANCE AND CONDUCTIVITY MEASUREMENTS

ACCURACY: 0.015% of full scale bridge output, limited by the matching bridge resistors. The excitation voltage should be programmed so the bridge output matches the full scale input voltage range.

MEASUREMENT TYPES: 6 wire and 4 wire full bridge; 4 wire, 3 wire, and 2 wire half bridge. Bridge measurements are ratio-metric and dual polarity to eliminate thermal emf's. AC resistance measurements use a dual polarity 750 μs excitation pulse for ionic depolarization, with the signal integration occurring over the last 250 μs .

PULSE COUNTERS

NUMBER OF PULSE COUNTER CHANNELS: 2 eight bit or 1 sixteen bit selectable.

MAXIMUM COUNT RATE: 2000 Hz, eight bit counters; 250 kHz, sixteen bit counters. Pulse counter channels scanned at 8 Hz.

MODES: Switch closure, high frequency pulse, and low level AC.

SWITCH CLOSURE MODE

Minimum Switch Closed Time: 5 ms.
Minimum Switch Open Time: 6 ms.
Maximum Bounce Time: 1 ms open without count.

HIGH FREQUENCY PULSE MODE

Minimum Pulse Width: 2 μs .
Maximum Input Frequency: 250 kHz.
Voltage Thresholds: Count upon transition from below 1.5 V to above 3.5 V.
Maximum Input Voltage: ± 20 V.

LOW LEVEL AC MODE

(Typical of magnetic pulse flow sensors, selected anemometers, etc.)

Min AC Input Voltage: 6 mV RMS
Input Hysteresis: 11 mV
Max. AC Input Voltage: 20 V RMS

Frequency Range:

| AC Input (RMS) | Range |
|------------------------|-------------------|
| 20 millivolts | 1 Hz to 100 Hz |
| 50 millivolts | 0.5 Hz to 400 Hz |
| 150 millivolts to 20 V | 0.3 Hz to 1000 Hz |

(Consult factory if higher frequencies are desired.)

DIGITAL I/O PORTS

8 ports, software selectable as binary inputs or control outputs.

OUTPUT VOLTAGES (no load):

high — 5 V ± 0.1 V; low — < 0.1 V.

OUTPUT RESISTANCE: 500 ohms.

INPUT STATE: high — > 3 V; low — < 0.8 V.

INPUT RESISTANCE: 100 kohms.

TRANSIENT PROTECTION

All input and output connections to the CR10 module are protected using RC filters or transzorbis connected to a heavy copper bar between the circuit card and the case. The CR10WP Wiring Panel includes additional spark gap and transzorb protection.

CPU AND INTERFACE

PROCESSOR: Hitachi 6303.

MEMORY: 32k ROM, 16k RAM expandable to 64k.

DISPLAY: 8 digit LCD (0.5" digits).

PERIPHERAL INTERFACE: 9 pin D-type connector for keyboard/display, storage module, cassette, modem, printer, and RS232 adapter. Baud rates selectable at 300, 1200, 9600, and 76,800.

CLOCK ACCURACY: ± 1 minute per month.

MAXIMUM PROGRAM EXECUTION RATE: System tasks initiated in sync with real-time up to 64 Hz. One measurement with tape transfer is possible at this rate without interruption.

SYSTEM POWER REQUIREMENTS

VOLTAGE: 9.6 to 16 volts.

TYPICAL CURRENT DRAIN: 0.5 mA quiescent, 13 mA during processing, and 35 mA during analog measurement.

BATTERIES: 7.5 Ahr alkaline D-cells or 5 Ahr rechargeable lead acid batteries, standard.

PHYSICAL SPECIFICATIONS

SIZE: 7.8" x 3.5" x 1.5"; 9" x 3.5" x 2.9" with CR10WP Wiring Panel. Input connectors extend length 0.15".

WEIGHT: 2 lbs.

WARRANTY

Two years against defects in materials and workmanship.



CAMPBELL SCIENTIFIC

P.O. Box 551
Logan, UT 84321
Phone (801) 753-2342
TLX 453058

9699 45th Avenue
Edmonton, Alberta T6E 5Z8
CANADA
Phone (403) 434-9421
TLX 037-2966 (EDM)

College Road/Sutton Bonington
Loughborough, LE12 5RA
ENGLAND
Phone 05097 2516
TLX 94016393 (CAMP G)